

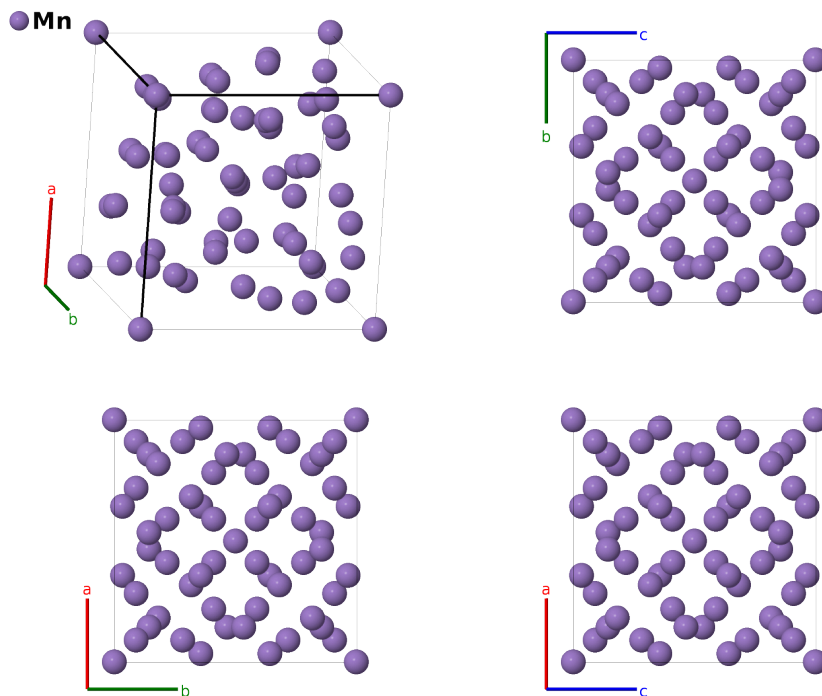
# $\alpha$ -Mn (A12) Structure: A\_cI58\_217\_ac2g-001

This structure originally had the label A\_cI58\_217\_ac2g. Calls to that address will be redirected here.

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<https://aflow.org/p/SV19>

[https://aflow.org/p/A\\_cI58\\_217\\_ac2g-001](https://aflow.org/p/A_cI58_217_ac2g-001)

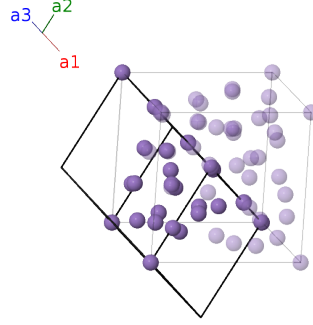


<b>Prototype</b>	Mn
<b>AFLOW prototype label</b>	A_cI58_217_ac2g-001
<b><i>Strukturbericht</i> designation</b>	A12
<b>ICSD</b>	42743
<b>Pearson symbol</b>	cI58
<b>Space group number</b>	217
<b>Space group symbol</b>	$I\bar{4}3m$
<b>AFLOW prototype command</b>	<code>aflow --proto=A_cI58_217_ac2g-001 --params=a, x2, x3, z3, x4, z4</code>

- This is the ground state structure of manganese. The high temperature structure,  $\beta$ -Mn (A13), is stable from 727-1095°C and metastable at room temperature (Donohue, 1982).
- $Mg_{17}Al_{12}$  is a binary form of this structure.

## Body-centered Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a\hat{x} + \frac{1}{2}a\hat{y} + \frac{1}{2}a\hat{z} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{x} - \frac{1}{2}a\hat{y} + \frac{1}{2}a\hat{z} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{x} + \frac{1}{2}a\hat{y} - \frac{1}{2}a\hat{z}\end{aligned}$$



## Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$0$	$=$	$0$	(2a)	Mn I
$\mathbf{B}_2$	$2x_2 \mathbf{a}_1 + 2x_2 \mathbf{a}_2 + 2x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{x} + ax_2 \hat{y} + ax_2 \hat{z}$	(8c)	Mn II
$\mathbf{B}_3$	$-2x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{x} - ax_2 \hat{y} + ax_2 \hat{z}$	(8c)	Mn II
$\mathbf{B}_4$	$-2x_2 \mathbf{a}_2$	$=$	$-ax_2 \hat{x} + ax_2 \hat{y} - ax_2 \hat{z}$	(8c)	Mn II
$\mathbf{B}_5$	$-2x_2 \mathbf{a}_1$	$=$	$ax_2 \hat{x} - ax_2 \hat{y} - ax_2 \hat{z}$	(8c)	Mn II
$\mathbf{B}_6$	$(x_3 + z_3) \mathbf{a}_1 + (x_3 + z_3) \mathbf{a}_2 + 2x_3 \mathbf{a}_3$	$=$	$ax_3 \hat{x} + ax_3 \hat{y} + az_3 \hat{z}$	(24g)	Mn III
$\mathbf{B}_7$	$-(x_3 - z_3) \mathbf{a}_1 - (x_3 - z_3) \mathbf{a}_2 - 2x_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{x} - ax_3 \hat{y} + az_3 \hat{z}$	(24g)	Mn III
$\mathbf{B}_8$	$(x_3 - z_3) \mathbf{a}_1 - (x_3 + z_3) \mathbf{a}_2$	$=$	$-ax_3 \hat{x} + ax_3 \hat{y} - az_3 \hat{z}$	(24g)	Mn III
$\mathbf{B}_9$	$-(x_3 + z_3) \mathbf{a}_1 + (x_3 - z_3) \mathbf{a}_2$	$=$	$ax_3 \hat{x} - ax_3 \hat{y} - az_3 \hat{z}$	(24g)	Mn III
$\mathbf{B}_{10}$	$2x_3 \mathbf{a}_1 + (x_3 + z_3) \mathbf{a}_2 + (x_3 + z_3) \mathbf{a}_3$	$=$	$az_3 \hat{x} + ax_3 \hat{y} + ax_3 \hat{z}$	(24g)	Mn III
$\mathbf{B}_{11}$	$-2x_3 \mathbf{a}_1 - (x_3 - z_3) \mathbf{a}_2 - (x_3 - z_3) \mathbf{a}_3$	$=$	$az_3 \hat{x} - ax_3 \hat{y} - ax_3 \hat{z}$	(24g)	Mn III
$\mathbf{B}_{12}$	$(x_3 - z_3) \mathbf{a}_2 - (x_3 + z_3) \mathbf{a}_3$	$=$	$-az_3 \hat{x} - ax_3 \hat{y} + ax_3 \hat{z}$	(24g)	Mn III
$\mathbf{B}_{13}$	$-(x_3 + z_3) \mathbf{a}_2 + (x_3 - z_3) \mathbf{a}_3$	$=$	$-az_3 \hat{x} + ax_3 \hat{y} - ax_3 \hat{z}$	(24g)	Mn III
$\mathbf{B}_{14}$	$(x_3 + z_3) \mathbf{a}_1 + 2x_3 \mathbf{a}_2 + (x_3 + z_3) \mathbf{a}_3$	$=$	$ax_3 \hat{x} + az_3 \hat{y} + ax_3 \hat{z}$	(24g)	Mn III
$\mathbf{B}_{15}$	$-(x_3 - z_3) \mathbf{a}_1 - 2x_3 \mathbf{a}_2 - (x_3 - z_3) \mathbf{a}_3$	$=$	$-ax_3 \hat{x} + az_3 \hat{y} - ax_3 \hat{z}$	(24g)	Mn III
$\mathbf{B}_{16}$	$-(x_3 + z_3) \mathbf{a}_1 + (x_3 - z_3) \mathbf{a}_3$	$=$	$ax_3 \hat{x} - az_3 \hat{y} - ax_3 \hat{z}$	(24g)	Mn III
$\mathbf{B}_{17}$	$(x_3 - z_3) \mathbf{a}_1 - (x_3 + z_3) \mathbf{a}_3$	$=$	$-ax_3 \hat{x} - az_3 \hat{y} + ax_3 \hat{z}$	(24g)	Mn III
$\mathbf{B}_{18}$	$(x_4 + z_4) \mathbf{a}_1 + (x_4 + z_4) \mathbf{a}_2 + 2x_4 \mathbf{a}_3$	$=$	$ax_4 \hat{x} + ax_4 \hat{y} + az_4 \hat{z}$	(24g)	Mn IV
$\mathbf{B}_{19}$	$-(x_4 - z_4) \mathbf{a}_1 - (x_4 - z_4) \mathbf{a}_2 - 2x_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{x} - ax_4 \hat{y} + az_4 \hat{z}$	(24g)	Mn IV
$\mathbf{B}_{20}$	$(x_4 - z_4) \mathbf{a}_1 - (x_4 + z_4) \mathbf{a}_2$	$=$	$-ax_4 \hat{x} + ax_4 \hat{y} - az_4 \hat{z}$	(24g)	Mn IV
$\mathbf{B}_{21}$	$-(x_4 + z_4) \mathbf{a}_1 + (x_4 - z_4) \mathbf{a}_2$	$=$	$ax_4 \hat{x} - ax_4 \hat{y} - az_4 \hat{z}$	(24g)	Mn IV
$\mathbf{B}_{22}$	$2x_4 \mathbf{a}_1 + (x_4 + z_4) \mathbf{a}_2 + (x_4 + z_4) \mathbf{a}_3$	$=$	$az_4 \hat{x} + ax_4 \hat{y} + ax_4 \hat{z}$	(24g)	Mn IV

$$\begin{aligned}
\mathbf{B}_{23} &= \begin{matrix} -2x_4 \mathbf{a}_1 - (x_4 - z_4) \mathbf{a}_2 - \\ (x_4 - z_4) \mathbf{a}_3 \end{matrix} = az_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}} & (24g) & \text{Mn IV} \\
\mathbf{B}_{24} &= (x_4 - z_4) \mathbf{a}_2 - (x_4 + z_4) \mathbf{a}_3 = -az_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}} & (24g) & \text{Mn IV} \\
\mathbf{B}_{25} &= -(x_4 + z_4) \mathbf{a}_2 + (x_4 - z_4) \mathbf{a}_3 = -az_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}} & (24g) & \text{Mn IV} \\
\mathbf{B}_{26} &= \begin{matrix} (x_4 + z_4) \mathbf{a}_1 + 2x_4 \mathbf{a}_2 + \\ (x_4 + z_4) \mathbf{a}_3 \end{matrix} = ax_4 \hat{\mathbf{x}} + az_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}} & (24g) & \text{Mn IV} \\
\mathbf{B}_{27} &= \begin{matrix} -(x_4 - z_4) \mathbf{a}_1 - 2x_4 \mathbf{a}_2 - \\ (x_4 - z_4) \mathbf{a}_3 \end{matrix} = -ax_4 \hat{\mathbf{x}} + az_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}} & (24g) & \text{Mn IV} \\
\mathbf{B}_{28} &= -(x_4 + z_4) \mathbf{a}_1 + (x_4 - z_4) \mathbf{a}_3 = ax_4 \hat{\mathbf{x}} - az_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}} & (24g) & \text{Mn IV} \\
\mathbf{B}_{29} &= (x_4 - z_4) \mathbf{a}_1 - (x_4 + z_4) \mathbf{a}_3 = -ax_4 \hat{\mathbf{x}} - az_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}} & (24g) & \text{Mn IV}
\end{aligned}$$

## References

- [1] J. A. Oberteuffer and J. A. Ibers, *A refinement of the atomic and thermal parameters of  $\alpha$ -manganese from a single crystal*, Acta Crystallogr. Sect. B **26**, 1499–1504 (1970), doi:10.1107/S0567740870004399.
- [2] J. Donohue, *The Structures of the Elements* (Robert E. Krieger Publishing Company, Malabar, Florida, 1982). Reprint of the 1974 John Wiley & Sons edition.