

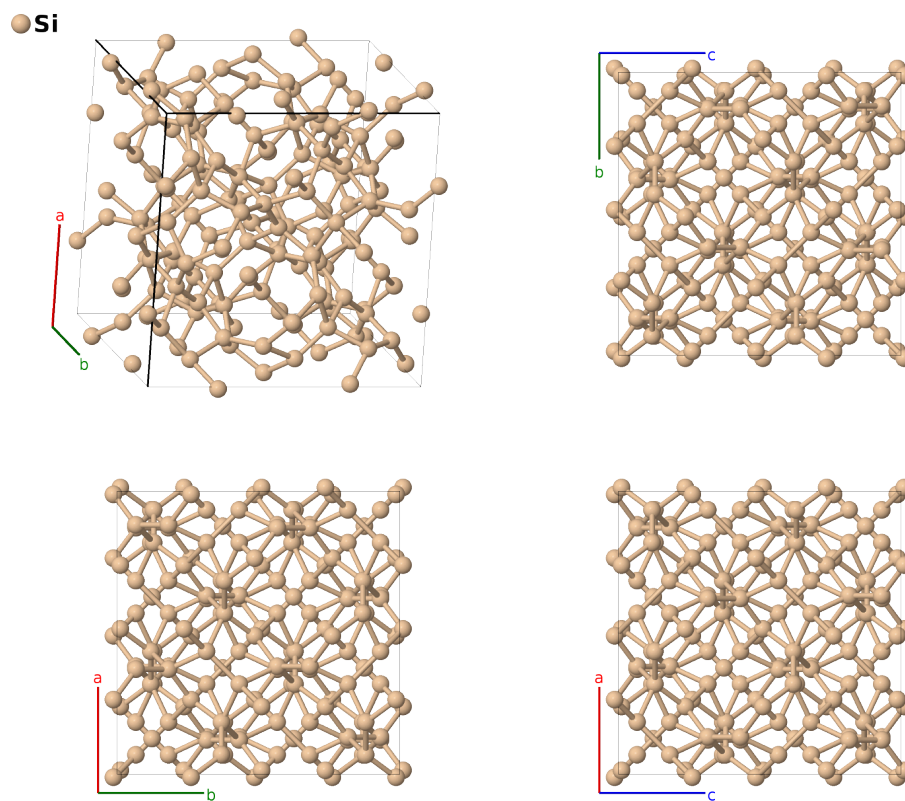
Si₃₄ Clathrate Structure: A_cF136_227_aeg-001

This structure originally had the label A_cF136_227_aeg. Calls to that address will be redirected here.

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<https://aflow.org/p/U115>

https://aflow.org/p/A_cF136_227_aeg-001



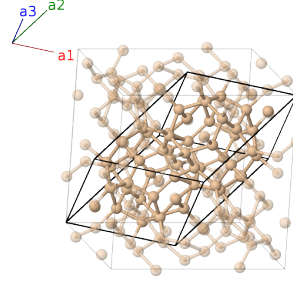
Prototype	Si
AFLOW prototype label	A_cF136_227_aeg-001
ICSD	none
Pearson symbol	cF136
Space group number	227
Space group symbol	$Fd\bar{3}m$
AFLOW prototype command	<code>aflow --proto=A_cF136_227_aeg-001 --params=a, x₂, x₃, z₃</code>

Other compounds with this structure
Ge (high pressure)

- Silicon clathrates are open structures of pentagonal dodecahedra connected so that all of the silicon atoms have sp³ bonding. In nature these structures are stabilized by alkali impurity atoms.
- This structure and the Si₄₆ structure are proposed “pure” silicon clathrate structures.
- For more information about these structures and their possible stability, see (Adams, 1994).
- See (Gryko, 2000) for a possible experimental realization of this structure (Si₃₄Na_x, where x is very small).
- We have used the fact that all vectors of the form (0, ±a/2, ±a/2), (±a/2, 0, ±a/2), and (±a/2, ±a/2, 0) are primitive vectors of the face-centered cubic lattice to simplify the positions of some atoms in both lattice and Cartesian coordinates.
- (Dong, 1999) study a similar, but not identical structure (ICSD 56271), and (Schwarz, 2008) find a similar high-pressure phase of germanium (ICSD 245948).

Face-centered Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}a \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= \frac{1}{8} \mathbf{a}_1 + \frac{1}{8} \mathbf{a}_2 + \frac{1}{8} \mathbf{a}_3$	$=$	$\frac{1}{8} a \hat{\mathbf{x}} + \frac{1}{8} a \hat{\mathbf{y}} + \frac{1}{8} a \hat{\mathbf{z}}$	(8a)	Si I
\mathbf{B}_2	$= \frac{7}{8} \mathbf{a}_1 + \frac{7}{8} \mathbf{a}_2 + \frac{7}{8} \mathbf{a}_3$	$=$	$\frac{7}{8} a \hat{\mathbf{x}} + \frac{7}{8} a \hat{\mathbf{y}} + \frac{7}{8} a \hat{\mathbf{z}}$	(8a)	Si I
\mathbf{B}_3	$= x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$	(32e)	Si II
\mathbf{B}_4	$= x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 - (3x_2 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-a(x_2 - \frac{1}{4}) \hat{\mathbf{x}} - a(x_2 - \frac{1}{4}) \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$	(32e)	Si II
\mathbf{B}_5	$= x_2 \mathbf{a}_1 - (3x_2 - \frac{1}{2}) \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$-a(x_2 - \frac{1}{4}) \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} - a(x_2 - \frac{1}{4}) \hat{\mathbf{z}}$	(32e)	Si II
\mathbf{B}_6	$= -(3x_2 - \frac{1}{2}) \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} - a(x_2 - \frac{1}{4}) \hat{\mathbf{y}} - a(x_2 - \frac{1}{4}) \hat{\mathbf{z}}$	(32e)	Si II
\mathbf{B}_7	$= -x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 + (3x_2 + \frac{1}{2}) \mathbf{a}_3$	$=$	$a(x_2 + \frac{1}{4}) \hat{\mathbf{x}} + a(x_2 + \frac{1}{4}) \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$	(32e)	Si II
\mathbf{B}_8	$= -x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$	(32e)	Si II
\mathbf{B}_9	$= -x_2 \mathbf{a}_1 + (3x_2 + \frac{1}{2}) \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$a(x_2 + \frac{1}{4}) \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} + a(x_2 + \frac{1}{4}) \hat{\mathbf{z}}$	(32e)	Si II
\mathbf{B}_{10}	$= (3x_2 + \frac{1}{2}) \mathbf{a}_1 - x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + a(x_2 + \frac{1}{4}) \hat{\mathbf{y}} + a(x_2 + \frac{1}{4}) \hat{\mathbf{z}}$	(32e)	Si II
\mathbf{B}_{11}	$= z_3 \mathbf{a}_1 + z_3 \mathbf{a}_2 + (2x_3 - z_3) \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + az_3 \hat{\mathbf{z}}$	(96g)	Si III
\mathbf{B}_{12}	$= z_3 \mathbf{a}_1 + z_3 \mathbf{a}_2 - (2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-a(x_3 - \frac{1}{4}) \hat{\mathbf{x}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{y}} + az_3 \hat{\mathbf{z}}$	(96g)	Si III
\mathbf{B}_{13}	$= (2x_3 - z_3) \mathbf{a}_1 - (2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$-a(x_3 - \frac{1}{4}) \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} - a(z_3 - \frac{1}{4}) \hat{\mathbf{z}}$	(96g)	Si III
\mathbf{B}_{14}	$= -(2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_1 + (2x_3 - z_3) \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{y}} - a(z_3 - \frac{1}{4}) \hat{\mathbf{z}}$	(96g)	Si III
\mathbf{B}_{15}	$= (2x_3 - z_3) \mathbf{a}_1 + z_3 \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$az_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(96g)	Si III
\mathbf{B}_{16}	$= -(2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_1 + z_3 \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$az_3 \hat{\mathbf{x}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{y}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{z}}$	(96g)	Si III

$$\begin{aligned}
\mathbf{B}_{17} &= z_3 \mathbf{a}_1 + (2x_3 - z_3) \mathbf{a}_2 - (2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_3 &= -a(z_3 - \frac{1}{4}) \hat{\mathbf{x}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{18} &= z_3 \mathbf{a}_1 - (2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_2 + (2x_3 - z_3) \mathbf{a}_3 &= -a(z_3 - \frac{1}{4}) \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{19} &= z_3 \mathbf{a}_1 + (2x_3 - z_3) \mathbf{a}_2 + z_3 \mathbf{a}_3 &= ax_3 \hat{\mathbf{x}} + az_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{20} &= z_3 \mathbf{a}_1 - (2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_2 + z_3 \mathbf{a}_3 &= -a(x_3 - \frac{1}{4}) \hat{\mathbf{x}} + az_3 \hat{\mathbf{y}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{21} &= -(2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_1 + z_3 \mathbf{a}_2 + (2x_3 - z_3) \mathbf{a}_3 &= ax_3 \hat{\mathbf{x}} - a(z_3 - \frac{1}{4}) \hat{\mathbf{y}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{22} &= (2x_3 - z_3) \mathbf{a}_1 + z_3 \mathbf{a}_2 - (2x_3 + z_3 - \frac{1}{2}) \mathbf{a}_3 &= -a(x_3 - \frac{1}{4}) \hat{\mathbf{x}} - a(z_3 - \frac{1}{4}) \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{23} &= -z_3 \mathbf{a}_1 - z_3 \mathbf{a}_2 + (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_3 &= a(x_3 + \frac{1}{4}) \hat{\mathbf{x}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{y}} - az_3 \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{24} &= -z_3 \mathbf{a}_1 - z_3 \mathbf{a}_2 - (2x_3 - z_3) \mathbf{a}_3 &= -ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - az_3 \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{25} &= -(2x_3 - z_3) \mathbf{a}_1 + (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_2 - z_3 \mathbf{a}_3 &= a(x_3 + \frac{1}{4}) \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + a(z_3 + \frac{1}{4}) \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{26} &= (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_1 - (2x_3 - z_3) \mathbf{a}_2 - z_3 \mathbf{a}_3 &= -ax_3 \hat{\mathbf{x}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{y}} + a(z_3 + \frac{1}{4}) \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{27} &= -(2x_3 - z_3) \mathbf{a}_1 - z_3 \mathbf{a}_2 + (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_3 &= a(x_3 + \frac{1}{4}) \hat{\mathbf{x}} + a(z_3 + \frac{1}{4}) \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{28} &= (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_1 - z_3 \mathbf{a}_2 - (2x_3 - z_3) \mathbf{a}_3 &= -ax_3 \hat{\mathbf{x}} + a(z_3 + \frac{1}{4}) \hat{\mathbf{y}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{29} &= -z_3 \mathbf{a}_1 - (2x_3 - z_3) \mathbf{a}_2 - z_3 \mathbf{a}_3 &= -ax_3 \hat{\mathbf{x}} - az_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{30} &= -z_3 \mathbf{a}_1 + (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_2 - z_3 \mathbf{a}_3 &= a(x_3 + \frac{1}{4}) \hat{\mathbf{x}} - az_3 \hat{\mathbf{y}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{31} &= -z_3 \mathbf{a}_1 - (2x_3 - z_3) \mathbf{a}_2 + (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_3 &= a(z_3 + \frac{1}{4}) \hat{\mathbf{x}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{32} &= -z_3 \mathbf{a}_1 + (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_2 - (2x_3 - z_3) \mathbf{a}_3 &= a(z_3 + \frac{1}{4}) \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{33} &= (2x_3 + z_3 + \frac{1}{2}) \mathbf{a}_1 - z_3 \mathbf{a}_2 - z_3 \mathbf{a}_3 &= -az_3 \hat{\mathbf{x}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{y}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{z}} &(96g) &\text{Si III} \\
\mathbf{B}_{34} &= -(2x_3 - z_3) \mathbf{a}_1 - z_3 \mathbf{a}_2 - z_3 \mathbf{a}_3 &= -az_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}} &(96g) &\text{Si III}
\end{aligned}$$

References

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