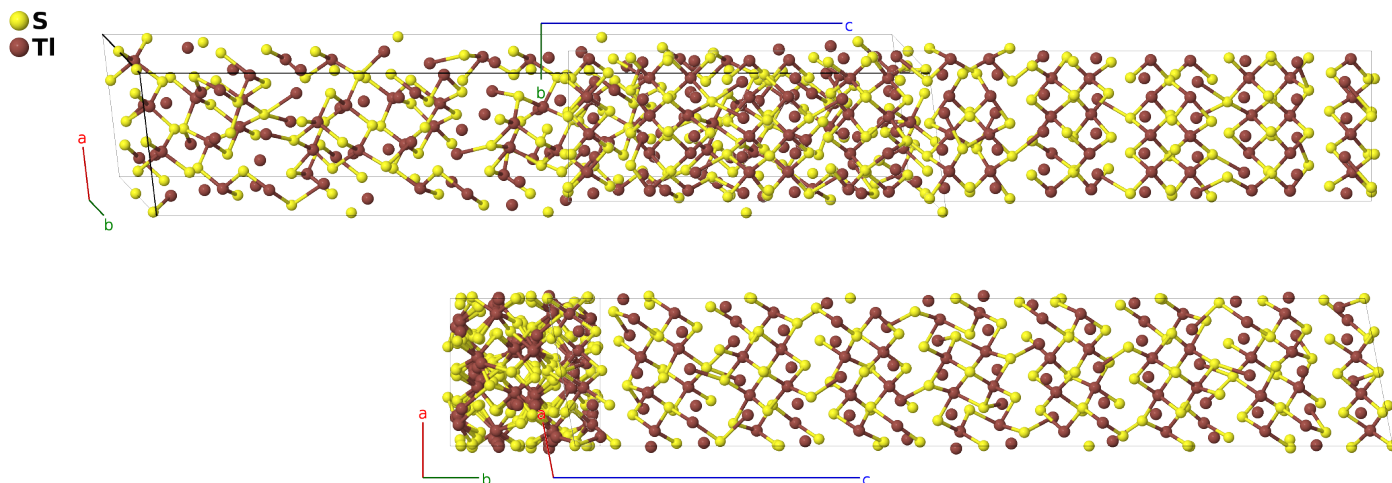


# High Temperature Monoclinic TlS Structure: AB\_mC256\_5\_2a2b30c\_32c-001

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<https://aflow.org/p/J6WY>

[https://aflow.org/p/AB\\_mC256\\_5\\_2a2b30c\\_32c-001](https://aflow.org/p/AB_mC256_5_2a2b30c_32c-001)



Prototype	STl
AFLOW prototype label	AB_mC256_5_2a2b30c_32c-001
ICSD	74446
Pearson symbol	mC256
Space group number	5
Space group symbol	$C2$
AFLOW prototype command	<pre>aflow --proto=AB_mC256_5_2a2b30c_32c-001       --params=a, b/a, c/a, <math>\beta</math>, y1, y2, y3, y4, x5, y5, z5, x6, y6, z6, x7, y7, z7, x8, y8, z8, x9, y9, z9, x10, y10, z10, x11, y11, z11, x12, y12, z12, x13, y13, z13, x14, y14, z14, x15, y15, z15, x16, y16, z16, x17, y17, z17, x18, y18, z18, x19, y19, z19, x20, y20, z20, x21, y21, z21, x22, y22, z22, x23, y23, z23, x24, y24, z24, x25, y25, z25, x26, y26, z26, x27, y27, z27, x28, y28, z28, x29, y29, z29, x30, y30, z30, x31, y31, z31, x32, y32, z32, x33, y33, z33, x34, y34, z34, x35, y35, z35, x36, y36, z36, x37, y37, z37, x38, y38, z38, x39, y39, z39, x40, y40, z40, x41, y41, z41, x42, y42, z42, x43, y43, z43, x44, y44, z44, x45, y45, z45, x46, y46, z46, x47, y47, z47, x48, y48, z48, x49, y49, z49, x50, y50, z50, x51, y51, z51, x52, y52, z52, x53, y53, z53, x54, y54, z54, x55, y55, z55, x56, y56, z56, x57, y57, z57, x58, y58, z58, x59, y59, z59, x60, y60, z60, x61, y61, z61, x62, y62, z62, x63, y63, z63, x64, y64, z64, x65, y65, z65, x66, y66, z66</pre>

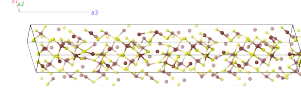
- TlS occurs naturally in three forms (Villars, 2018):
  - The ground state is tetragonal in the TlSe ( $B37$ ) structure which (Villars, 2018) calls “Tet-I” and (Kishida, 1994) calls “Type I.”
  - An intermediate tetragonal structure, which (Villars, 2018) calls “Tetragonal II,” and (Kashida, 1994) calls Type III.
  - A high temperature monoclinic structure, called “Mon” by (Villars, 2018) and “Type II” by (Kishida, 1994). (this structure)

- If we replaced the conventional cell primitive vector  $\mathbf{a}_3$  used by (Nakamura, 1993) with  $\mathbf{a}'_3 = \mathbf{a}_1 + \mathbf{a}_3$  both the conventional and primitive cells would be very close to tetragonal cells.

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### Base-centered Monoclinic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}b \hat{\mathbf{y}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \cos \beta \hat{\mathbf{x}} + c \sin \beta \hat{\mathbf{z}}\end{aligned}$$




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### Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= -y_1 \mathbf{a}_1 + y_1 \mathbf{a}_2$	$=$	$by_1 \hat{\mathbf{y}}$	(2a)	S I
$\mathbf{B}_2$	$= -y_2 \mathbf{a}_1 + y_2 \mathbf{a}_2$	$=$	$by_2 \hat{\mathbf{y}}$	(2a)	S II
$\mathbf{B}_3$	$= -y_3 \mathbf{a}_1 + y_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}c \cos \beta \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} + \frac{1}{2}c \sin \beta \hat{\mathbf{z}}$	(2b)	S III
$\mathbf{B}_4$	$= -y_4 \mathbf{a}_1 + y_4 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}c \cos \beta \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} + \frac{1}{2}c \sin \beta \hat{\mathbf{z}}$	(2b)	S IV
$\mathbf{B}_5$	$= (x_5 - y_5) \mathbf{a}_1 + (x_5 + y_5) \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$(ax_5 + cz_5 \cos \beta) \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} + cz_5 \sin \beta \hat{\mathbf{z}}$	(4c)	S V
$\mathbf{B}_6$	$= -(x_5 + y_5) \mathbf{a}_1 - (x_5 - y_5) \mathbf{a}_2 - z_5 \mathbf{a}_3$	$=$	$-(ax_5 + cz_5 \cos \beta) \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} - cz_5 \sin \beta \hat{\mathbf{z}}$	(4c)	S V
$\mathbf{B}_7$	$= (x_6 - y_6) \mathbf{a}_1 + (x_6 + y_6) \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$(ax_6 + cz_6 \cos \beta) \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \sin \beta \hat{\mathbf{z}}$	(4c)	S VI
$\mathbf{B}_8$	$= -(x_6 + y_6) \mathbf{a}_1 - (x_6 - y_6) \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$-(ax_6 + cz_6 \cos \beta) \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} - cz_6 \sin \beta \hat{\mathbf{z}}$	(4c)	S VI
$\mathbf{B}_9$	$= (x_7 - y_7) \mathbf{a}_1 + (x_7 + y_7) \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$(ax_7 + cz_7 \cos \beta) \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} + cz_7 \sin \beta \hat{\mathbf{z}}$	(4c)	S VII
$\mathbf{B}_{10}$	$= -(x_7 + y_7) \mathbf{a}_1 - (x_7 - y_7) \mathbf{a}_2 - z_7 \mathbf{a}_3$	$=$	$-(ax_7 + cz_7 \cos \beta) \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} - cz_7 \sin \beta \hat{\mathbf{z}}$	(4c)	S VII
$\mathbf{B}_{11}$	$= (x_8 - y_8) \mathbf{a}_1 + (x_8 + y_8) \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$(ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} + cz_8 \sin \beta \hat{\mathbf{z}}$	(4c)	S VIII
$\mathbf{B}_{12}$	$= -(x_8 + y_8) \mathbf{a}_1 - (x_8 - y_8) \mathbf{a}_2 - z_8 \mathbf{a}_3$	$=$	$-(ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} - cz_8 \sin \beta \hat{\mathbf{z}}$	(4c)	S VIII
$\mathbf{B}_{13}$	$= (x_9 - y_9) \mathbf{a}_1 + (x_9 + y_9) \mathbf{a}_2 + z_9 \mathbf{a}_3$	$=$	$(ax_9 + cz_9 \cos \beta) \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} + cz_9 \sin \beta \hat{\mathbf{z}}$	(4c)	S IX
$\mathbf{B}_{14}$	$= -(x_9 + y_9) \mathbf{a}_1 - (x_9 - y_9) \mathbf{a}_2 - z_9 \mathbf{a}_3$	$=$	$-(ax_9 + cz_9 \cos \beta) \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} - cz_9 \sin \beta \hat{\mathbf{z}}$	(4c)	S IX
$\mathbf{B}_{15}$	$= (x_{10} - y_{10}) \mathbf{a}_1 + (x_{10} + y_{10}) \mathbf{a}_2 + z_{10} \mathbf{a}_3$	$=$	$(ax_{10} + cz_{10} \cos \beta) \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} + cz_{10} \sin \beta \hat{\mathbf{z}}$	(4c)	S X
$\mathbf{B}_{16}$	$= -(x_{10} + y_{10}) \mathbf{a}_1 - (x_{10} - y_{10}) \mathbf{a}_2 - z_{10} \mathbf{a}_3$	$=$	$-(ax_{10} + cz_{10} \cos \beta) \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} - cz_{10} \sin \beta \hat{\mathbf{z}}$	(4c)	S X
$\mathbf{B}_{17}$	$= (x_{11} - y_{11}) \mathbf{a}_1 + (x_{11} + y_{11}) \mathbf{a}_2 + z_{11} \mathbf{a}_3$	$=$	$(ax_{11} + cz_{11} \cos \beta) \hat{\mathbf{x}} + by_{11} \hat{\mathbf{y}} + cz_{11} \sin \beta \hat{\mathbf{z}}$	(4c)	S XI
$\mathbf{B}_{18}$	$= -(x_{11} + y_{11}) \mathbf{a}_1 - (x_{11} - y_{11}) \mathbf{a}_2 - z_{11} \mathbf{a}_3$	$=$	$-(ax_{11} + cz_{11} \cos \beta) \hat{\mathbf{x}} + by_{11} \hat{\mathbf{y}} - cz_{11} \sin \beta \hat{\mathbf{z}}$	(4c)	S XI
$\mathbf{B}_{19}$	$= (x_{12} - y_{12}) \mathbf{a}_1 + (x_{12} + y_{12}) \mathbf{a}_2 + z_{12} \mathbf{a}_3$	$=$	$(ax_{12} + cz_{12} \cos \beta) \hat{\mathbf{x}} + by_{12} \hat{\mathbf{y}} + cz_{12} \sin \beta \hat{\mathbf{z}}$	(4c)	S XII
$\mathbf{B}_{20}$	$= -(x_{12} + y_{12}) \mathbf{a}_1 - (x_{12} - y_{12}) \mathbf{a}_2 - z_{12} \mathbf{a}_3$	$=$	$-(ax_{12} + cz_{12} \cos \beta) \hat{\mathbf{x}} + by_{12} \hat{\mathbf{y}} - cz_{12} \sin \beta \hat{\mathbf{z}}$	(4c)	S XII







$$\begin{aligned}
\mathbf{B}_{93} &= (x_{49} - y_{49}) \mathbf{a}_1 + (x_{49} + y_{49}) \mathbf{a}_2 + z_{49} \mathbf{a}_3 &= (ax_{49} + cz_{49} \cos \beta) \hat{\mathbf{x}} + by_{49} \hat{\mathbf{y}} + cz_{49} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XV} \\
\mathbf{B}_{94} &= -(x_{49} + y_{49}) \mathbf{a}_1 - (x_{49} - y_{49}) \mathbf{a}_2 - z_{49} \mathbf{a}_3 &= -(ax_{49} + cz_{49} \cos \beta) \hat{\mathbf{x}} + by_{49} \hat{\mathbf{y}} - cz_{49} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XV} \\
\mathbf{B}_{95} &= (x_{50} - y_{50}) \mathbf{a}_1 + (x_{50} + y_{50}) \mathbf{a}_2 + z_{50} \mathbf{a}_3 &= (ax_{50} + cz_{50} \cos \beta) \hat{\mathbf{x}} + by_{50} \hat{\mathbf{y}} + cz_{50} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XVI} \\
\mathbf{B}_{96} &= -(x_{50} + y_{50}) \mathbf{a}_1 - (x_{50} - y_{50}) \mathbf{a}_2 - z_{50} \mathbf{a}_3 &= -(ax_{50} + cz_{50} \cos \beta) \hat{\mathbf{x}} + by_{50} \hat{\mathbf{y}} - cz_{50} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XVI} \\
\mathbf{B}_{97} &= (x_{51} - y_{51}) \mathbf{a}_1 + (x_{51} + y_{51}) \mathbf{a}_2 + z_{51} \mathbf{a}_3 &= (ax_{51} + cz_{51} \cos \beta) \hat{\mathbf{x}} + by_{51} \hat{\mathbf{y}} + cz_{51} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XVII} \\
\mathbf{B}_{98} &= -(x_{51} + y_{51}) \mathbf{a}_1 - (x_{51} - y_{51}) \mathbf{a}_2 - z_{51} \mathbf{a}_3 &= -(ax_{51} + cz_{51} \cos \beta) \hat{\mathbf{x}} + by_{51} \hat{\mathbf{y}} - cz_{51} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XVII} \\
\mathbf{B}_{99} &= (x_{52} - y_{52}) \mathbf{a}_1 + (x_{52} + y_{52}) \mathbf{a}_2 + z_{52} \mathbf{a}_3 &= (ax_{52} + cz_{52} \cos \beta) \hat{\mathbf{x}} + by_{52} \hat{\mathbf{y}} + cz_{52} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XVIII} \\
\mathbf{B}_{100} &= -(x_{52} + y_{52}) \mathbf{a}_1 - (x_{52} - y_{52}) \mathbf{a}_2 - z_{52} \mathbf{a}_3 &= -(ax_{52} + cz_{52} \cos \beta) \hat{\mathbf{x}} + by_{52} \hat{\mathbf{y}} - cz_{52} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XVIII} \\
\mathbf{B}_{101} &= (x_{53} - y_{53}) \mathbf{a}_1 + (x_{53} + y_{53}) \mathbf{a}_2 + z_{53} \mathbf{a}_3 &= (ax_{53} + cz_{53} \cos \beta) \hat{\mathbf{x}} + by_{53} \hat{\mathbf{y}} + cz_{53} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XIX} \\
\mathbf{B}_{102} &= -(x_{53} + y_{53}) \mathbf{a}_1 - (x_{53} - y_{53}) \mathbf{a}_2 - z_{53} \mathbf{a}_3 &= -(ax_{53} + cz_{53} \cos \beta) \hat{\mathbf{x}} + by_{53} \hat{\mathbf{y}} - cz_{53} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XIX} \\
\mathbf{B}_{103} &= (x_{54} - y_{54}) \mathbf{a}_1 + (x_{54} + y_{54}) \mathbf{a}_2 + z_{54} \mathbf{a}_3 &= (ax_{54} + cz_{54} \cos \beta) \hat{\mathbf{x}} + by_{54} \hat{\mathbf{y}} + cz_{54} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XX} \\
\mathbf{B}_{104} &= -(x_{54} + y_{54}) \mathbf{a}_1 - (x_{54} - y_{54}) \mathbf{a}_2 - z_{54} \mathbf{a}_3 &= -(ax_{54} + cz_{54} \cos \beta) \hat{\mathbf{x}} + by_{54} \hat{\mathbf{y}} - cz_{54} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XX} \\
\mathbf{B}_{105} &= (x_{55} - y_{55}) \mathbf{a}_1 + (x_{55} + y_{55}) \mathbf{a}_2 + z_{55} \mathbf{a}_3 &= (ax_{55} + cz_{55} \cos \beta) \hat{\mathbf{x}} + by_{55} \hat{\mathbf{y}} + cz_{55} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XXI} \\
\mathbf{B}_{106} &= -(x_{55} + y_{55}) \mathbf{a}_1 - (x_{55} - y_{55}) \mathbf{a}_2 - z_{55} \mathbf{a}_3 &= -(ax_{55} + cz_{55} \cos \beta) \hat{\mathbf{x}} + by_{55} \hat{\mathbf{y}} - cz_{55} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XXI} \\
\mathbf{B}_{107} &= (x_{56} - y_{56}) \mathbf{a}_1 + (x_{56} + y_{56}) \mathbf{a}_2 + z_{56} \mathbf{a}_3 &= (ax_{56} + cz_{56} \cos \beta) \hat{\mathbf{x}} + by_{56} \hat{\mathbf{y}} + cz_{56} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XXII} \\
\mathbf{B}_{108} &= -(x_{56} + y_{56}) \mathbf{a}_1 - (x_{56} - y_{56}) \mathbf{a}_2 - z_{56} \mathbf{a}_3 &= -(ax_{56} + cz_{56} \cos \beta) \hat{\mathbf{x}} + by_{56} \hat{\mathbf{y}} - cz_{56} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XXII} \\
\mathbf{B}_{109} &= (x_{57} - y_{57}) \mathbf{a}_1 + (x_{57} + y_{57}) \mathbf{a}_2 + z_{57} \mathbf{a}_3 &= (ax_{57} + cz_{57} \cos \beta) \hat{\mathbf{x}} + by_{57} \hat{\mathbf{y}} + cz_{57} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XXIII} \\
\mathbf{B}_{110} &= -(x_{57} + y_{57}) \mathbf{a}_1 - (x_{57} - y_{57}) \mathbf{a}_2 - z_{57} \mathbf{a}_3 &= -(ax_{57} + cz_{57} \cos \beta) \hat{\mathbf{x}} + by_{57} \hat{\mathbf{y}} - cz_{57} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XXIII} \\
\mathbf{B}_{111} &= (x_{58} - y_{58}) \mathbf{a}_1 + (x_{58} + y_{58}) \mathbf{a}_2 + z_{58} \mathbf{a}_3 &= (ax_{58} + cz_{58} \cos \beta) \hat{\mathbf{x}} + by_{58} \hat{\mathbf{y}} + cz_{58} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XXIV} \\
\mathbf{B}_{112} &= -(x_{58} + y_{58}) \mathbf{a}_1 - (x_{58} - y_{58}) \mathbf{a}_2 - z_{58} \mathbf{a}_3 &= -(ax_{58} + cz_{58} \cos \beta) \hat{\mathbf{x}} + by_{58} \hat{\mathbf{y}} - cz_{58} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XXIV} \\
\mathbf{B}_{113} &= (x_{59} - y_{59}) \mathbf{a}_1 + (x_{59} + y_{59}) \mathbf{a}_2 + z_{59} \mathbf{a}_3 &= (ax_{59} + cz_{59} \cos \beta) \hat{\mathbf{x}} + by_{59} \hat{\mathbf{y}} + cz_{59} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XXV} \\
\mathbf{B}_{114} &= -(x_{59} + y_{59}) \mathbf{a}_1 - (x_{59} - y_{59}) \mathbf{a}_2 - z_{59} \mathbf{a}_3 &= -(ax_{59} + cz_{59} \cos \beta) \hat{\mathbf{x}} + by_{59} \hat{\mathbf{y}} - cz_{59} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XXV} \\
\mathbf{B}_{115} &= (x_{60} - y_{60}) \mathbf{a}_1 + (x_{60} + y_{60}) \mathbf{a}_2 + z_{60} \mathbf{a}_3 &= (ax_{60} + cz_{60} \cos \beta) \hat{\mathbf{x}} + by_{60} \hat{\mathbf{y}} + cz_{60} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XXVI} \\
\mathbf{B}_{116} &= -(x_{60} + y_{60}) \mathbf{a}_1 - (x_{60} - y_{60}) \mathbf{a}_2 - z_{60} \mathbf{a}_3 &= -(ax_{60} + cz_{60} \cos \beta) \hat{\mathbf{x}} + by_{60} \hat{\mathbf{y}} - cz_{60} \sin \beta \hat{\mathbf{z}} &(4c) &\text{Tl XXVI}
\end{aligned}$$

$\mathbf{B}_{117} =$	$(x_{61} - y_{61}) \mathbf{a}_1 +$ $(x_{61} + y_{61}) \mathbf{a}_2 + z_{61} \mathbf{a}_3$	$=$	$(ax_{61} + cz_{61} \cos \beta) \hat{\mathbf{x}} + by_{61} \hat{\mathbf{y}} + cz_{61} \sin \beta \hat{\mathbf{z}}$	(4c)	Tl XXVII
$\mathbf{B}_{118} =$	$-(x_{61} + y_{61}) \mathbf{a}_1 -$ $(x_{61} - y_{61}) \mathbf{a}_2 - z_{61} \mathbf{a}_3$	$=$	$-(ax_{61} + cz_{61} \cos \beta) \hat{\mathbf{x}} + by_{61} \hat{\mathbf{y}} -$ $cz_{61} \sin \beta \hat{\mathbf{z}}$	(4c)	Tl XXVII
$\mathbf{B}_{119} =$	$(x_{62} - y_{62}) \mathbf{a}_1 +$ $(x_{62} + y_{62}) \mathbf{a}_2 + z_{62} \mathbf{a}_3$	$=$	$(ax_{62} + cz_{62} \cos \beta) \hat{\mathbf{x}} + by_{62} \hat{\mathbf{y}} + cz_{62} \sin \beta \hat{\mathbf{z}}$	(4c)	Tl XXVIII
$\mathbf{B}_{120} =$	$-(x_{62} + y_{62}) \mathbf{a}_1 -$ $(x_{62} - y_{62}) \mathbf{a}_2 - z_{62} \mathbf{a}_3$	$=$	$-(ax_{62} + cz_{62} \cos \beta) \hat{\mathbf{x}} + by_{62} \hat{\mathbf{y}} -$ $cz_{62} \sin \beta \hat{\mathbf{z}}$	(4c)	Tl XXVIII
$\mathbf{B}_{121} =$	$(x_{63} - y_{63}) \mathbf{a}_1 +$ $(x_{63} + y_{63}) \mathbf{a}_2 + z_{63} \mathbf{a}_3$	$=$	$(ax_{63} + cz_{63} \cos \beta) \hat{\mathbf{x}} + by_{63} \hat{\mathbf{y}} + cz_{63} \sin \beta \hat{\mathbf{z}}$	(4c)	Tl XXIX
$\mathbf{B}_{122} =$	$-(x_{63} + y_{63}) \mathbf{a}_1 -$ $(x_{63} - y_{63}) \mathbf{a}_2 - z_{63} \mathbf{a}_3$	$=$	$-(ax_{63} + cz_{63} \cos \beta) \hat{\mathbf{x}} + by_{63} \hat{\mathbf{y}} -$ $cz_{63} \sin \beta \hat{\mathbf{z}}$	(4c)	Tl XXIX
$\mathbf{B}_{123} =$	$(x_{64} - y_{64}) \mathbf{a}_1 +$ $(x_{64} + y_{64}) \mathbf{a}_2 + z_{64} \mathbf{a}_3$	$=$	$(ax_{64} + cz_{64} \cos \beta) \hat{\mathbf{x}} + by_{64} \hat{\mathbf{y}} + cz_{64} \sin \beta \hat{\mathbf{z}}$	(4c)	Tl XXX
$\mathbf{B}_{124} =$	$-(x_{64} + y_{64}) \mathbf{a}_1 -$ $(x_{64} - y_{64}) \mathbf{a}_2 - z_{64} \mathbf{a}_3$	$=$	$-(ax_{64} + cz_{64} \cos \beta) \hat{\mathbf{x}} + by_{64} \hat{\mathbf{y}} -$ $cz_{64} \sin \beta \hat{\mathbf{z}}$	(4c)	Tl XXX
$\mathbf{B}_{125} =$	$(x_{65} - y_{65}) \mathbf{a}_1 +$ $(x_{65} + y_{65}) \mathbf{a}_2 + z_{65} \mathbf{a}_3$	$=$	$(ax_{65} + cz_{65} \cos \beta) \hat{\mathbf{x}} + by_{65} \hat{\mathbf{y}} + cz_{65} \sin \beta \hat{\mathbf{z}}$	(4c)	Tl XXXI
$\mathbf{B}_{126} =$	$-(x_{65} + y_{65}) \mathbf{a}_1 -$ $(x_{65} - y_{65}) \mathbf{a}_2 - z_{65} \mathbf{a}_3$	$=$	$-(ax_{65} + cz_{65} \cos \beta) \hat{\mathbf{x}} + by_{65} \hat{\mathbf{y}} -$ $cz_{65} \sin \beta \hat{\mathbf{z}}$	(4c)	Tl XXXI
$\mathbf{B}_{127} =$	$(x_{66} - y_{66}) \mathbf{a}_1 +$ $(x_{66} + y_{66}) \mathbf{a}_2 + z_{66} \mathbf{a}_3$	$=$	$(ax_{66} + cz_{66} \cos \beta) \hat{\mathbf{x}} + by_{66} \hat{\mathbf{y}} + cz_{66} \sin \beta \hat{\mathbf{z}}$	(4c)	Tl XXXII
$\mathbf{B}_{128} =$	$-(x_{66} + y_{66}) \mathbf{a}_1 -$ $(x_{66} - y_{66}) \mathbf{a}_2 - z_{66} \mathbf{a}_3$	$=$	$-(ax_{66} + cz_{66} \cos \beta) \hat{\mathbf{x}} + by_{66} \hat{\mathbf{y}} -$ $cz_{66} \sin \beta \hat{\mathbf{z}}$	(4c)	Tl XXXII

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