

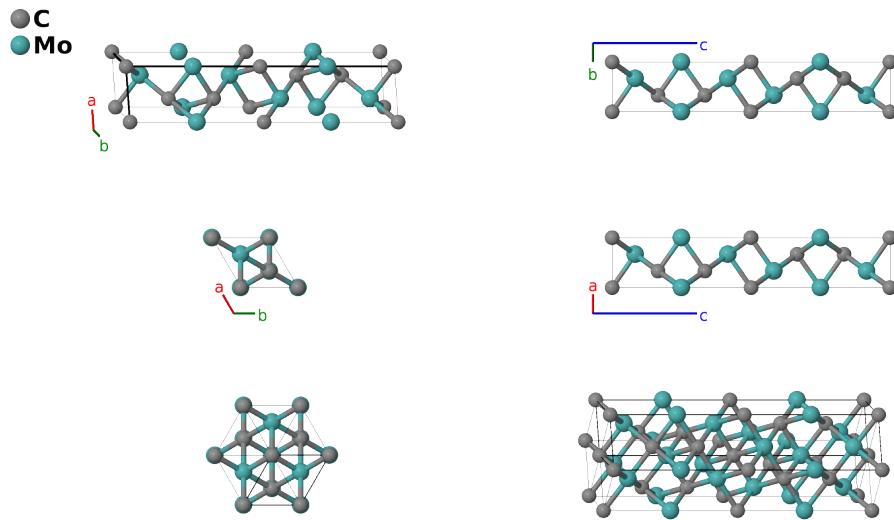
CMo Structure: AB_hP12_194_af_bf-001

This structure originally had the label `AB_hP12_194_af_bf`. Calls to that address will be redirected here.

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<https://aflow.org/p/Q5G8>

https://aflow.org/p/AB_hP12_194_af_bf-001



Prototype	CMo
AFLOW prototype label	<code>AB_hP12_194_af_bf-001</code>
ICSD	44987
Pearson symbol	hP12
Space group number	194
Space group symbol	$P6_3/mmc$
AFLOW prototype command	<code>aflow --proto=AB_hP12_194_af_bf-001 --params=a, c/a, z₃, z₄</code>

Other compounds with this structure

CRE, BaGaGe, CaGaGe, CaGaSn, CeNiP, DyNiP, GaGeSr, GdNiP, HoNiP, LiNiP, LuNiP, NdNiP, NiPPr, NiPTb, NiPTm, NiPY, C₂GeTi₃, C₂SiTi₃, C₂AlTi₃

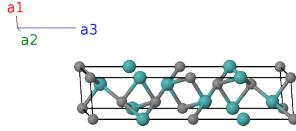
- Note that all of the atoms sit on close packed $\langle 0001 \rangle$ planes. The stacking sequence may be written:

Atom	Mo-II	C-II	C-I	C-II	Mo-II	Mo-I	Mo-II	C-II	C-I	C-II	Mo-II	Mo-I
Position	B	C	A	B	C	A	C	B	A	C	B	A

- Thus the Mo-II atoms and all of the C atoms are always in an fcc-like local environment, while the Mo-I atoms are in an hcp-like local environment. Like AlN₃Ti₄, this is a MAX phase. For more information, see (Radovic, 2013).

Hexagonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{2}a\hat{\mathbf{y}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{2}a\hat{\mathbf{y}} \\ \mathbf{a}_3 &= c\hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	= 0	=	0	(2a)	C I
\mathbf{B}_2	= $\frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{2}c\hat{\mathbf{z}}$	(2a)	C I
\mathbf{B}_3	= $\frac{1}{4}\mathbf{a}_3$	=	$\frac{1}{4}c\hat{\mathbf{z}}$	(2b)	Mo I
\mathbf{B}_4	= $\frac{3}{4}\mathbf{a}_3$	=	$\frac{3}{4}c\hat{\mathbf{z}}$	(2b)	Mo I
\mathbf{B}_5	= $\frac{1}{3}\mathbf{a}_1 + \frac{2}{3}\mathbf{a}_2 + z_3\mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} + cz_3\hat{\mathbf{z}}$	(4f)	C II
\mathbf{B}_6	= $\frac{2}{3}\mathbf{a}_1 + \frac{1}{3}\mathbf{a}_2 + (z_3 + \frac{1}{2})\mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} + c(z_3 + \frac{1}{2})\hat{\mathbf{z}}$	(4f)	C II
\mathbf{B}_7	= $\frac{2}{3}\mathbf{a}_1 + \frac{1}{3}\mathbf{a}_2 - z_3\mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} - cz_3\hat{\mathbf{z}}$	(4f)	C II
\mathbf{B}_8	= $\frac{1}{3}\mathbf{a}_1 + \frac{2}{3}\mathbf{a}_2 - (z_3 - \frac{1}{2})\mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} - c(z_3 - \frac{1}{2})\hat{\mathbf{z}}$	(4f)	C II
\mathbf{B}_9	= $\frac{1}{3}\mathbf{a}_1 + \frac{2}{3}\mathbf{a}_2 + z_4\mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(4f)	Mo II
\mathbf{B}_{10}	= $\frac{2}{3}\mathbf{a}_1 + \frac{1}{3}\mathbf{a}_2 + (z_4 + \frac{1}{2})\mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} + c(z_4 + \frac{1}{2})\hat{\mathbf{z}}$	(4f)	Mo II
\mathbf{B}_{11}	= $\frac{2}{3}\mathbf{a}_1 + \frac{1}{3}\mathbf{a}_2 - z_4\mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} - cz_4\hat{\mathbf{z}}$	(4f)	Mo II
\mathbf{B}_{12}	= $\frac{1}{3}\mathbf{a}_1 + \frac{2}{3}\mathbf{a}_2 - (z_4 - \frac{1}{2})\mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} - c(z_4 - \frac{1}{2})\hat{\mathbf{z}}$	(4f)	Mo II

References

- [1] H. Nowotny, R. Parthé, and F. Benesovsky, *Das Dreistotfsystem: Molybdän–Silizium–Kohlenstoff*, Monatsh. Chem. Verw. Tl. **85**, 255–272 (1954).
- [2] M. Radovic and M. W. Barsoum, *MAX phases: Bridging the gap between metals and ceramics*, American Ceramic Society Bulletin **92**, 20–27 (2013).