

# Diopside [CaMg(SiO<sub>3</sub>)<sub>2</sub>, *S*4<sub>1</sub>] Structure:

ABC6D2\_mC40\_15\_e\_e\_3f\_f-002

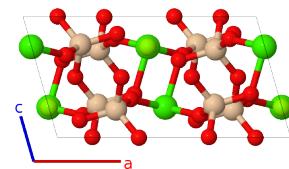
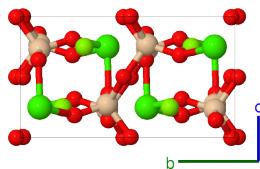
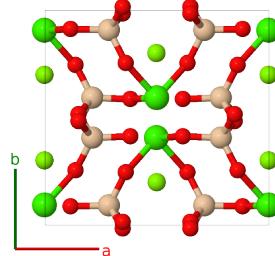
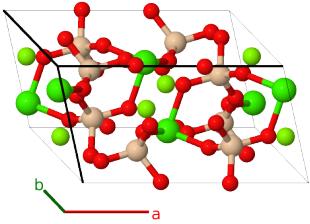
This structure originally had the label ABC6D2\_mC40\_15\_e\_e\_3f\_f.S4\_1. Calls to that address will be redirected here.

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<https://aflow.org/p/J45L>

[https://aflow.org/p/ABC6D2\\_mC40\\_15\\_e\\_e\\_3f\\_f-002](https://aflow.org/p/ABC6D2_mC40_15_e_e_3f_f-002)

● Ca  
● Mg  
● O  
● Si



**Prototype** CaMgO<sub>6</sub>Si<sub>2</sub>

**AFLOW prototype label** ABC6D2\_mC40\_15\_e\_e\_3f\_f-002

**Strukturbericht designation** *S*4<sub>1</sub>

**Mineral name** diopside

**ICSD** 12128

**Pearson symbol** mC40

**Space group number** 15

**Space group symbol** *C*2/*c*

**AFLOW prototype command**

```
aflow --proto=ABC6D2_mC40_15_e_e_3f_f-002
--params=a, b/a, c/a, β, y1, y2, x3, y3, z3, x4, y4, z4, x5, y5, z5, x6, y6, z6
```

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## Other compounds with this structure

(Ca, Na)(Mg, Fe, Al, Ti)(Si, Al)<sub>2</sub>O<sub>6</sub> (augite), NaAlSi<sub>2</sub>O<sub>6</sub>, NaFeSi<sub>2</sub>O<sub>6</sub>, NaInSi<sub>2</sub>O<sub>6</sub>, NaScSi<sub>2</sub>O<sub>6</sub>

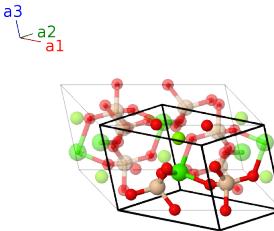
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- (Finger, 1976) list the two (4e) positions as 'M1' and 'M2', and both are mixtures of calcium and magnesium. For visual clarity we designated the first (4e) position as calcium and the second as magnesium.
- This structure has the same AFLOW label, ABC6D2\_mC40\_15\_e\_e\_3f\_f, as esseneite. The structures are generated by the same symmetry operations with different sets of parameters (`--params`) specified in their corresponding CIF files.

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### Base-centered Monoclinic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}b\hat{\mathbf{y}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}} \\ \mathbf{a}_3 &= c\cos\beta\hat{\mathbf{x}} + c\sin\beta\hat{\mathbf{z}}\end{aligned}$$




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### Basis vectors

	Lattice coordinates	=	Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$-y_1 \mathbf{a}_1 + y_1 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	=	$\frac{1}{4}c\cos\beta\hat{\mathbf{x}} + by_1\hat{\mathbf{y}} + \frac{1}{4}c\sin\beta\hat{\mathbf{z}}$	(4e)	Ca I
$\mathbf{B}_2$	$y_1 \mathbf{a}_1 - y_1 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	=	$\frac{3}{4}c\cos\beta\hat{\mathbf{x}} - by_1\hat{\mathbf{y}} + \frac{3}{4}c\sin\beta\hat{\mathbf{z}}$	(4e)	Ca I
$\mathbf{B}_3$	$-y_2 \mathbf{a}_1 + y_2 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	=	$\frac{1}{4}c\cos\beta\hat{\mathbf{x}} + by_2\hat{\mathbf{y}} + \frac{1}{4}c\sin\beta\hat{\mathbf{z}}$	(4e)	Mg I
$\mathbf{B}_4$	$y_2 \mathbf{a}_1 - y_2 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	=	$\frac{3}{4}c\cos\beta\hat{\mathbf{x}} - by_2\hat{\mathbf{y}} + \frac{3}{4}c\sin\beta\hat{\mathbf{z}}$	(4e)	Mg I
$\mathbf{B}_5$	$(x_3 - y_3) \mathbf{a}_1 + (x_3 + y_3) \mathbf{a}_2 + z_3 \mathbf{a}_3$	=	$(ax_3 + cz_3 \cos\beta)\hat{\mathbf{x}} + by_3\hat{\mathbf{y}} + cz_3 \sin\beta\hat{\mathbf{z}}$	(8f)	O I
$\mathbf{B}_6$	$-(x_3 + y_3) \mathbf{a}_1 - (x_3 - y_3) \mathbf{a}_2 - (z_3 - \frac{1}{2}) \mathbf{a}_3$	=	$-(ax_3 + c(z_3 - \frac{1}{2}) \cos\beta)\hat{\mathbf{x}} + by_3\hat{\mathbf{y}} - c(z_3 - \frac{1}{2}) \sin\beta\hat{\mathbf{z}}$	(8f)	O I
$\mathbf{B}_7$	$-(x_3 - y_3) \mathbf{a}_1 - (x_3 + y_3) \mathbf{a}_2 - z_3 \mathbf{a}_3$	=	$-(ax_3 + cz_3 \cos\beta)\hat{\mathbf{x}} - by_3\hat{\mathbf{y}} - cz_3 \sin\beta\hat{\mathbf{z}}$	(8f)	O I
$\mathbf{B}_8$	$(x_3 + y_3) \mathbf{a}_1 + (x_3 - y_3) \mathbf{a}_2 + (z_3 + \frac{1}{2}) \mathbf{a}_3$	=	$(ax_3 + c(z_3 + \frac{1}{2}) \cos\beta)\hat{\mathbf{x}} - by_3\hat{\mathbf{y}} + c(z_3 + \frac{1}{2}) \sin\beta\hat{\mathbf{z}}$	(8f)	O I
$\mathbf{B}_9$	$(x_4 - y_4) \mathbf{a}_1 + (x_4 + y_4) \mathbf{a}_2 + z_4 \mathbf{a}_3$	=	$(ax_4 + cz_4 \cos\beta)\hat{\mathbf{x}} + by_4\hat{\mathbf{y}} + cz_4 \sin\beta\hat{\mathbf{z}}$	(8f)	O II
$\mathbf{B}_{10}$	$-(x_4 + y_4) \mathbf{a}_1 - (x_4 - y_4) \mathbf{a}_2 - (z_4 - \frac{1}{2}) \mathbf{a}_3$	=	$-(ax_4 + c(z_4 - \frac{1}{2}) \cos\beta)\hat{\mathbf{x}} + by_4\hat{\mathbf{y}} - c(z_4 - \frac{1}{2}) \sin\beta\hat{\mathbf{z}}$	(8f)	O II
$\mathbf{B}_{11}$	$-(x_4 - y_4) \mathbf{a}_1 - (x_4 + y_4) \mathbf{a}_2 - z_4 \mathbf{a}_3$	=	$-(ax_4 + cz_4 \cos\beta)\hat{\mathbf{x}} - by_4\hat{\mathbf{y}} - cz_4 \sin\beta\hat{\mathbf{z}}$	(8f)	O II
$\mathbf{B}_{12}$	$(x_4 + y_4) \mathbf{a}_1 + (x_4 - y_4) \mathbf{a}_2 + (z_4 + \frac{1}{2}) \mathbf{a}_3$	=	$(ax_4 + c(z_4 + \frac{1}{2}) \cos\beta)\hat{\mathbf{x}} - by_4\hat{\mathbf{y}} + c(z_4 + \frac{1}{2}) \sin\beta\hat{\mathbf{z}}$	(8f)	O II
$\mathbf{B}_{13}$	$(x_5 - y_5) \mathbf{a}_1 + (x_5 + y_5) \mathbf{a}_2 + z_5 \mathbf{a}_3$	=	$(ax_5 + cz_5 \cos\beta)\hat{\mathbf{x}} + by_5\hat{\mathbf{y}} + cz_5 \sin\beta\hat{\mathbf{z}}$	(8f)	O III
$\mathbf{B}_{14}$	$-(x_5 + y_5) \mathbf{a}_1 - (x_5 - y_5) \mathbf{a}_2 - (z_5 - \frac{1}{2}) \mathbf{a}_3$	=	$-(ax_5 + c(z_5 - \frac{1}{2}) \cos\beta)\hat{\mathbf{x}} + by_5\hat{\mathbf{y}} - c(z_5 - \frac{1}{2}) \sin\beta\hat{\mathbf{z}}$	(8f)	O III
$\mathbf{B}_{15}$	$-(x_5 - y_5) \mathbf{a}_1 - (x_5 + y_5) \mathbf{a}_2 - z_5 \mathbf{a}_3$	=	$-(ax_5 + cz_5 \cos\beta)\hat{\mathbf{x}} - by_5\hat{\mathbf{y}} - cz_5 \sin\beta\hat{\mathbf{z}}$	(8f)	O III
$\mathbf{B}_{16}$	$(x_5 + y_5) \mathbf{a}_1 + (x_5 - y_5) \mathbf{a}_2 + (z_5 + \frac{1}{2}) \mathbf{a}_3$	=	$(ax_5 + c(z_5 + \frac{1}{2}) \cos\beta)\hat{\mathbf{x}} - by_5\hat{\mathbf{y}} + c(z_5 + \frac{1}{2}) \sin\beta\hat{\mathbf{z}}$	(8f)	O III

$$\begin{aligned}
\mathbf{B}_{17} &= (x_6 - y_6) \mathbf{a}_1 + (x_6 + y_6) \mathbf{a}_2 + z_6 \mathbf{a}_3 & = & (ax_6 + cz_6 \cos \beta) \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \sin \beta \hat{\mathbf{z}} & (8f) & \text{Si I} \\
\mathbf{B}_{18} &= -(x_6 + y_6) \mathbf{a}_1 - (x_6 - y_6) \mathbf{a}_2 - (z_6 - \frac{1}{2}) \mathbf{a}_3 & = & - (ax_6 + c(z_6 - \frac{1}{2}) \cos \beta) \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} - c(z_6 - \frac{1}{2}) \sin \beta \hat{\mathbf{z}} & (8f) & \text{Si I} \\
\mathbf{B}_{19} &= -(x_6 - y_6) \mathbf{a}_1 - (x_6 + y_6) \mathbf{a}_2 - z_6 \mathbf{a}_3 & = & - (ax_6 + cz_6 \cos \beta) \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} - cz_6 \sin \beta \hat{\mathbf{z}} & (8f) & \text{Si I} \\
\mathbf{B}_{20} &= (x_6 + y_6) \mathbf{a}_1 + (x_6 - y_6) \mathbf{a}_2 + (z_6 + \frac{1}{2}) \mathbf{a}_3 & = & (ax_6 + c(z_6 + \frac{1}{2}) \cos \beta) \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + c(z_6 + \frac{1}{2}) \sin \beta \hat{\mathbf{z}} & (8f) & \text{Si I}
\end{aligned}$$

## References

- [1] L. W. Finger and Y. Ohashi, *The thermal expansion of diopside to 800° C and a refinement of the crystal structure at 700° C*, Am. Mineral. **61**, 303–310 (1976).