

NbIrTe₄ Structure:

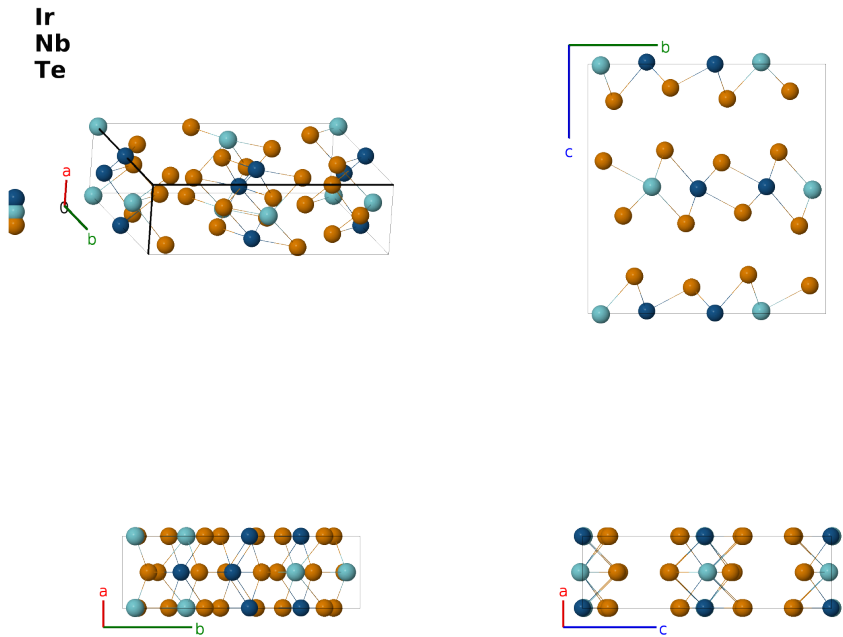
ABC4_oP24_31_2a_2a_8a-001

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<https://aflow.org/prototype-encyclopedia/H22P>

https://aflow.org/prototype-encyclopedia/ABC4_oP24_31_2a_2a_8a-001



Prototype	IrNbTe ₄
AFLOW prototype label	ABC4_oP24_31_2a_2a_8a-001
ICSD	73690
CCDC	1634457
Pearson symbol	oP24
Space group number	31
Space group symbol	$Pmn2_1$
AFLOW prototype command	<pre>aflow --proto=ABC4_oP24_31_2a_2a_8a-001 --params=a, b/a, c/a, y₁, z₁, y₂, z₂, y₃, z₃, y₄, z₄, y₅, z₅, y₆, z₆, y₇, z₇, y₈, z₈, y₉, z₉, y₁₀, z₁₀, y₁₁, z₁₁, y₁₂, z₁₂</pre>

Other compounds with this structure

NbOsTe₄, TaIrTe₄, TaOsTe₄, TaRhTe₄, TaRuTe₄

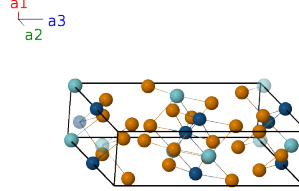
- Space group $Pmn2_1$ #31 allows an arbitrary placement of the origin of the z -axis. Here we set $z_1 = 0$ for the first iridium Wyckoff position.

Simple Orthorhombic primitive vectors

$$\mathbf{a}_1 = a \hat{\mathbf{x}}$$

$$\mathbf{a}_2 = b \hat{\mathbf{y}}$$

$$\mathbf{a}_3 = c \hat{\mathbf{z}}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= y_1 \mathbf{a}_2 + z_1 \mathbf{a}_3$	$=$	$by_1 \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(2a)	Ir I
$\mathbf{B}_2$	$= \frac{1}{2} \mathbf{a}_1 - y_1 \mathbf{a}_2 + (z_1 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - by_1 \hat{\mathbf{y}} + c(z_1 + \frac{1}{2}) \hat{\mathbf{z}}$	(2a)	Ir I
$\mathbf{B}_3$	$= y_2 \mathbf{a}_2 + z_2 \mathbf{a}_3$	$=$	$by_2 \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(2a)	Ir II
$\mathbf{B}_4$	$= \frac{1}{2} \mathbf{a}_1 - y_2 \mathbf{a}_2 + (z_2 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - by_2 \hat{\mathbf{y}} + c(z_2 + \frac{1}{2}) \hat{\mathbf{z}}$	(2a)	Ir II
$\mathbf{B}_5$	$= y_3 \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$by_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(2a)	Nb I
$\mathbf{B}_6$	$= \frac{1}{2} \mathbf{a}_1 - y_3 \mathbf{a}_2 + (z_3 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} + c(z_3 + \frac{1}{2}) \hat{\mathbf{z}}$	(2a)	Nb I
$\mathbf{B}_7$	$= y_4 \mathbf{a}_2 + z_4 \mathbf{a}_3$	$=$	$by_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(2a)	Nb II
$\mathbf{B}_8$	$= \frac{1}{2} \mathbf{a}_1 - y_4 \mathbf{a}_2 + (z_4 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} + c(z_4 + \frac{1}{2}) \hat{\mathbf{z}}$	(2a)	Nb II
$\mathbf{B}_9$	$= y_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(2a)	Te I
$\mathbf{B}_{10}$	$= \frac{1}{2} \mathbf{a}_1 - y_5 \mathbf{a}_2 + (z_5 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} + c(z_5 + \frac{1}{2}) \hat{\mathbf{z}}$	(2a)	Te I
$\mathbf{B}_{11}$	$= y_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(2a)	Te II
$\mathbf{B}_{12}$	$= \frac{1}{2} \mathbf{a}_1 - y_6 \mathbf{a}_2 + (z_6 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + c(z_6 + \frac{1}{2}) \hat{\mathbf{z}}$	(2a)	Te II
$\mathbf{B}_{13}$	$= y_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(2a)	Te III
$\mathbf{B}_{14}$	$= \frac{1}{2} \mathbf{a}_1 - y_7 \mathbf{a}_2 + (z_7 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} + c(z_7 + \frac{1}{2}) \hat{\mathbf{z}}$	(2a)	Te III
$\mathbf{B}_{15}$	$= y_8 \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(2a)	Te IV
$\mathbf{B}_{16}$	$= \frac{1}{2} \mathbf{a}_1 - y_8 \mathbf{a}_2 + (z_8 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} + c(z_8 + \frac{1}{2}) \hat{\mathbf{z}}$	(2a)	Te IV
$\mathbf{B}_{17}$	$= y_9 \mathbf{a}_2 + z_9 \mathbf{a}_3$	$=$	$by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(2a)	Te V
$\mathbf{B}_{18}$	$= \frac{1}{2} \mathbf{a}_1 - y_9 \mathbf{a}_2 + (z_9 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - by_9 \hat{\mathbf{y}} + c(z_9 + \frac{1}{2}) \hat{\mathbf{z}}$	(2a)	Te V
$\mathbf{B}_{19}$	$= y_{10} \mathbf{a}_2 + z_{10} \mathbf{a}_3$	$=$	$by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}}$	(2a)	Te VI
$\mathbf{B}_{20}$	$= \frac{1}{2} \mathbf{a}_1 - y_{10} \mathbf{a}_2 + (z_{10} + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - by_{10} \hat{\mathbf{y}} + c(z_{10} + \frac{1}{2}) \hat{\mathbf{z}}$	(2a)	Te VI
$\mathbf{B}_{21}$	$= y_{11} \mathbf{a}_2 + z_{11} \mathbf{a}_3$	$=$	$by_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}}$	(2a)	Te VII
$\mathbf{B}_{22}$	$= \frac{1}{2} \mathbf{a}_1 - y_{11} \mathbf{a}_2 + (z_{11} + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - by_{11} \hat{\mathbf{y}} + c(z_{11} + \frac{1}{2}) \hat{\mathbf{z}}$	(2a)	Te VII
$\mathbf{B}_{23}$	$= y_{12} \mathbf{a}_2 + z_{12} \mathbf{a}_3$	$=$	$by_{12} \hat{\mathbf{y}} + cz_{12} \hat{\mathbf{z}}$	(2a)	Te VIII

$$\mathbf{B}_{24} = \frac{1}{2} \mathbf{a}_1 - y_{12} \mathbf{a}_2 + \left(z_{12} + \frac{1}{2}\right) \mathbf{a}_3 = \frac{1}{2} a \hat{\mathbf{x}} - by_{12} \hat{\mathbf{y}} + c \left(z_{12} + \frac{1}{2}\right) \hat{\mathbf{z}} \quad (2a) \quad \text{Te VIII}$$

References

- [1] A. Mar and J. A. Ibers, *Synthesis and physical properties of the new layered ternary tellurides $M\text{IrTe}_4$ ($M = \text{Nb}, \text{Ta}$), and the structure of NbIrTe_4* , J. Solid State Chem. **97**, 366–376 (1992), doi:10.1016/0022-4596(92)90045-W.

Found in

- [1] A. Mar, S. Jobic, and J. A. Ibers, *Metal-metal vs tellurium-tellurium bonding in WTe_2 and its ternary variants TaIrTe_4 and NbIrTe_4* , J. Am. Chem. Soc. **114**, 8963–8971 (1992), doi:10.1021/ja00049a029.

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