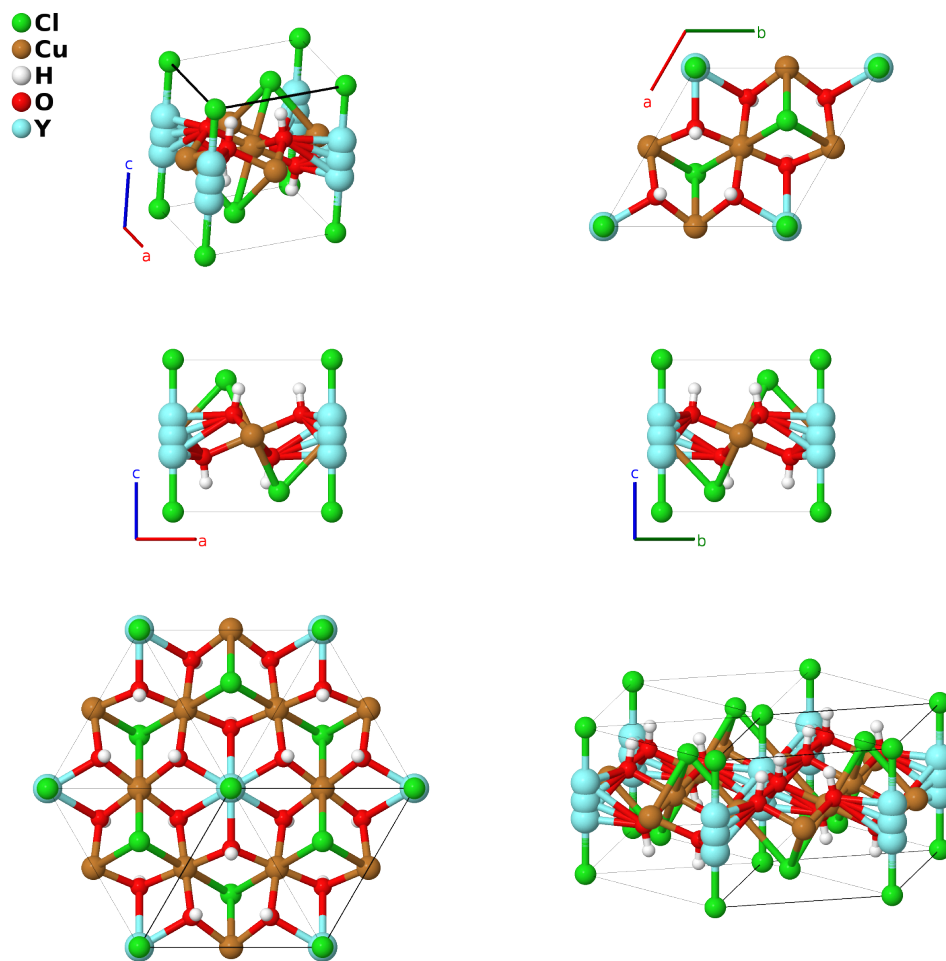


YCu₃(OH)₆Cl₃ Structure: ABC2D2E_hP21_164_bd_e_i_i_ac-001

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<https://afLOW.org/p/1PRT>

https://afLOW.org/p/ABC2D2E_hP21_164_bd_e_i_i_ac-001

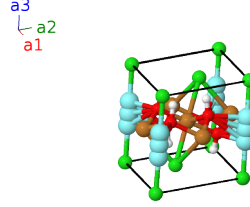


Prototype	Cl ₃ Cu ₃ H ₆ O ₆ Y
AFLOW prototype label	ABC2D2E_hP21_164_bd_e_i_i_ac-001
ICSD	32385
Pearson symbol	hP21
Space group number	164
Space group symbol	$P\bar{3}m1$
AFLOW prototype command	<code>afLOW --proto=ABC2D2E_hP21_164_bd_e_i_i_ac-001 --params=a, c/a, z₃, z₄, x₆, z₆, x₇, z₇</code>

- The Y-I (1b) site is occupied 95% of the time, with the other 5% of the yttrium atoms distributed on the Y-II (2c) sites. Thus only one of the triplet of yttrium atoms in the picture will be occupied at any one time, and most of the time it will be the central atom.
- (Zorko, 2019) give positions for the oxygen atoms which are not consistent with the (6i) Wyckoff positions. As the difference is slight, we assume that the x and z coordinates are correct and generate the y coordinate from the symmetry operations for the (6i) positions.
- The ICSD entry for this paper instead tries to solve the problem by placing the oxygen atoms on a half-filled (12j) site.

Trigonal (Hexagonal) primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}a \hat{\mathbf{y}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}a \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	0	$=$	0	(1a)	Y I
\mathbf{B}_2	$\frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}c \hat{\mathbf{z}}$	(1b)	Cl I
\mathbf{B}_3	$z_3 \mathbf{a}_3$	$=$	$cz_3 \hat{\mathbf{z}}$	(2c)	Y II
\mathbf{B}_4	$-z_3 \mathbf{a}_3$	$=$	$-cz_3 \hat{\mathbf{z}}$	(2c)	Y II
\mathbf{B}_5	$\frac{1}{3} \mathbf{a}_1 + \frac{2}{3} \mathbf{a}_2 + z_4 \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(2d)	Cl II
\mathbf{B}_6	$\frac{2}{3} \mathbf{a}_1 + \frac{1}{3} \mathbf{a}_2 - z_4 \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}}$	(2d)	Cl II
\mathbf{B}_7	$\frac{1}{2} \mathbf{a}_1$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} - \frac{\sqrt{3}}{4}a \hat{\mathbf{y}}$	(3e)	Cu I
\mathbf{B}_8	$\frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + \frac{\sqrt{3}}{4}a \hat{\mathbf{y}}$	(3e)	Cu I
\mathbf{B}_9	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2}a \hat{\mathbf{x}}$	(3e)	Cu I
\mathbf{B}_{10}	$x_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$-\sqrt{3}ax_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(6i)	H I
\mathbf{B}_{11}	$x_6 \mathbf{a}_1 + 2x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$\frac{3}{2}ax_6 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(6i)	H I
\mathbf{B}_{12}	$-2x_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$-\frac{3}{2}ax_6 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(6i)	H I
\mathbf{B}_{13}	$-x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$\sqrt{3}ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(6i)	H I
\mathbf{B}_{14}	$2x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$\frac{3}{2}ax_6 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(6i)	H I
\mathbf{B}_{15}	$-x_6 \mathbf{a}_1 - 2x_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$-\frac{3}{2}ax_6 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(6i)	H I
\mathbf{B}_{16}	$x_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$-\sqrt{3}ax_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(6i)	O I
\mathbf{B}_{17}	$x_7 \mathbf{a}_1 + 2x_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$\frac{3}{2}ax_7 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(6i)	O I
\mathbf{B}_{18}	$-2x_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$-\frac{3}{2}ax_7 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(6i)	O I
\mathbf{B}_{19}	$-x_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 - z_7 \mathbf{a}_3$	$=$	$\sqrt{3}ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(6i)	O I
\mathbf{B}_{20}	$2x_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 - z_7 \mathbf{a}_3$	$=$	$\frac{3}{2}ax_7 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(6i)	O I
\mathbf{B}_{21}	$-x_7 \mathbf{a}_1 - 2x_7 \mathbf{a}_2 - z_7 \mathbf{a}_3$	$=$	$-\frac{3}{2}ax_7 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(6i)	O I

References

- [1] A. Zorko, M. Pregelj, M. Gomilšek, M. Klanjšek, O. Zaharko, W. Sun, and J.-X. Mi, *Negative-vector-chirality 120° spin structure in the defect- and distortion-free quantum kagome antiferromagnet $YCu_3(OH)_6Cl_3$* , Phys. Rev. B **100**, 144420 (2019), doi:10.1103/PhysRevB.100.144420.