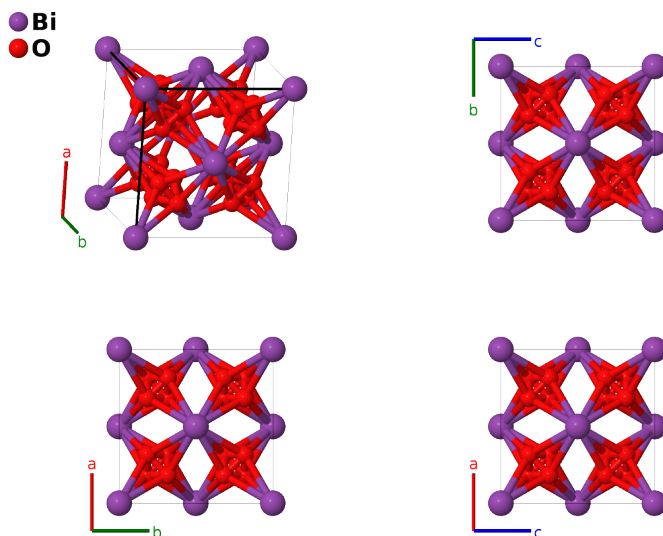


δ -Bi₂O₃ Structure: AB8_cF36_225_a.f-001

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<https://aflow.org/p/X2Q7>

https://aflow.org/p/AB8_cF36_225_a.f-001



Prototype	Bi ₂ O ₃
AFLOW prototype label	AB8_cF36_225_a.f-001
ICSD	2375
Pearson symbol	cF36
Space group number	225
Space group symbol	$Fm\bar{3}m$
AFLOW prototype command	<pre>aflow --proto=AB8_cF36_225_a.f-001 --params=a, x₂</pre>

Other compounds with this structure

α -CuI, γ -CuI

- Bi₂O₃ can be found in at least six forms (Harwig, 1978; Locherer, 2011):
 - monoclinic α -Bi₂O₃, the ground state, stable up to 729°,
 - tetragonal β -Bi₂O₃, D_{5h}^{12} , a metastable state observed at 650°C (this structure),
 - body-centered cubic γ -Bi₂O₃, another metastable phase observed at 639°C,
 - face-centered cubic δ -Bi₂O₃, the stable phase from 729° up to the melting point at 824°C (this structure),
 - a high-pressure HP-Bi₂O₃, and
 - a second “nonquenchable” high-pressure structure, HPC-Bi₂O₃.

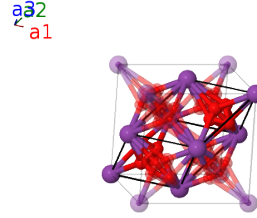
- The oxygen sites are occupied 18.75% of the time. If $z_2 \rightarrow 1/4$, they coalesce on the (2c) Wyckoff position, and this becomes the fluorite (C1) structure.
- Other compounds with different stoichiometries have this structure. In copper(I) iodide both the high temperature α -CuI and the ground state γ -CuI phases are in this structure, with the copper atoms occupying 1/8 of the (32f) sites. (Keen, 1995)

Face-centered Cubic primitive vectors

$$\mathbf{a}_1 = \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}a \hat{\mathbf{z}}$$

$$\mathbf{a}_2 = \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{z}}$$

$$\mathbf{a}_3 = \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1 =$	0	$=$	0	(4a)	Bi I
$\mathbf{B}_2 =$	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$	(32f)	O I
$\mathbf{B}_3 =$	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 - 3x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$	(32f)	O I
$\mathbf{B}_4 =$	$x_2 \mathbf{a}_1 - 3x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$	(32f)	O I
$\mathbf{B}_5 =$	$-3x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$	(32f)	O I
$\mathbf{B}_6 =$	$-x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 + 3x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$	(32f)	O I
$\mathbf{B}_7 =$	$-x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$	(32f)	O I
$\mathbf{B}_8 =$	$-x_2 \mathbf{a}_1 + 3x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$	(32f)	O I
$\mathbf{B}_9 =$	$3x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$	(32f)	O I

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