

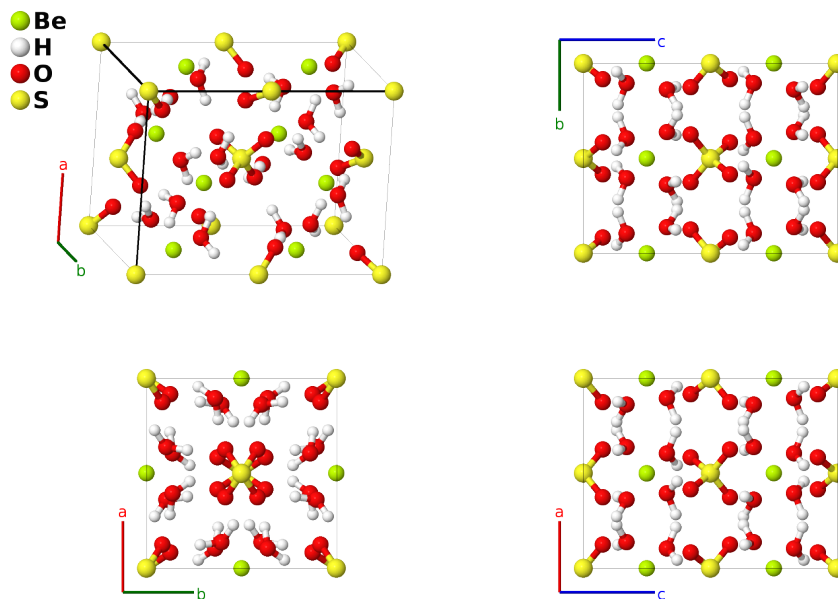
BeSO₄·4H₂O (*H*₄₃) Structure: AB8C8D_tI72_120_b_2i_2i_c-001

This structure originally had the label AB8C8D_tI72_120_c_2i_2i_b. Calls to that address will be redirected here.

Cite this page as: D. Hicks, M. J. Mehl, M. Esters, C. Oses, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/p/KR2S>

https://aflow.org/p/AB8C8D_tI72_120_b_2i_2i_c-001



Prototype	BeH ₈ O ₈ S
AFLOW prototype label	AB8C8D_tI72_120_b_2i_2i_c-001
<i>Strukturbericht</i> designation	<i>H</i> ₄₃
ICSD	23219
Pearson symbol	tI72
Space group number	120
Space group symbol	$\bar{I}4c2$
AFLOW prototype command	<code>aflow --proto=AB8C8D_tI72_120_b_2i_2i_c-001 --params=a, c/a, x₃, y₃, z₃, x₄, y₄, z₄, x₅, y₅, z₅, x₆, y₆, z₆</code>

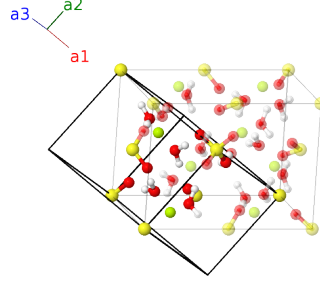
- The original determination of the *H*₄₃ structure did not determine the positions of the hydrogen atoms. Since (Sikka, 1969) showed that the placement of the hydrogen atoms did not substantially affect the positions of the other atoms in the primitive cell, nor change the space group, we retain the original *Strukturbericht* designation for the improved structure.

Body-centered Tetragonal primitive vectors

$$\mathbf{a}_1 = -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$$

$$\mathbf{a}_2 = \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$$

$$\mathbf{a}_3 = \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	0	$=$	0	(4b)	Be I
\mathbf{B}_2	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2}c \hat{\mathbf{z}}$	(4b)	Be I
\mathbf{B}_3	$\frac{3}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(4c)	S I
\mathbf{B}_4	$\frac{1}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{4}c \hat{\mathbf{z}}$	(4c)	S I
\mathbf{B}_5	$(y_3 + z_3) \mathbf{a}_1 + (x_3 + z_3) \mathbf{a}_2 + (x_3 + y_3) \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + ay_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(16i)	H I
\mathbf{B}_6	$-(y_3 - z_3) \mathbf{a}_1 - (x_3 - z_3) \mathbf{a}_2 - (x_3 + y_3) \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} - ay_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(16i)	H I
\mathbf{B}_7	$-(x_3 + z_3) \mathbf{a}_1 + (y_3 - z_3) \mathbf{a}_2 - (x_3 - y_3) \mathbf{a}_3$	$=$	$ay_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}}$	(16i)	H I
\mathbf{B}_8	$(x_3 - z_3) \mathbf{a}_1 - (y_3 + z_3) \mathbf{a}_2 + (x_3 - y_3) \mathbf{a}_3$	$=$	$-ay_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}}$	(16i)	H I
\mathbf{B}_9	$(-y_3 + z_3 + \frac{1}{2}) \mathbf{a}_1 + (x_3 + z_3 + \frac{1}{2}) \mathbf{a}_2 + (x_3 - y_3) \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} - ay_3 \hat{\mathbf{y}} + c(z_3 + \frac{1}{2}) \hat{\mathbf{z}}$	(16i)	H I
\mathbf{B}_{10}	$(y_3 + z_3 + \frac{1}{2}) \mathbf{a}_1 + (-x_3 + z_3 + \frac{1}{2}) \mathbf{a}_2 - (x_3 - y_3) \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} + ay_3 \hat{\mathbf{y}} + c(z_3 + \frac{1}{2}) \hat{\mathbf{z}}$	(16i)	H I
\mathbf{B}_{11}	$(x_3 - z_3 + \frac{1}{2}) \mathbf{a}_1 + (y_3 - z_3 + \frac{1}{2}) \mathbf{a}_2 + (x_3 + y_3) \mathbf{a}_3$	$=$	$ay_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} - c(z_3 - \frac{1}{2}) \hat{\mathbf{z}}$	(16i)	H I
\mathbf{B}_{12}	$-(x_3 + z_3 - \frac{1}{2}) \mathbf{a}_1 - (y_3 + z_3 - \frac{1}{2}) \mathbf{a}_2 - (x_3 + y_3) \mathbf{a}_3$	$=$	$-ay_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - c(z_3 - \frac{1}{2}) \hat{\mathbf{z}}$	(16i)	H I
\mathbf{B}_{13}	$(y_4 + z_4) \mathbf{a}_1 + (x_4 + z_4) \mathbf{a}_2 + (x_4 + y_4) \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + ay_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(16i)	H II
\mathbf{B}_{14}	$-(y_4 - z_4) \mathbf{a}_1 - (x_4 - z_4) \mathbf{a}_2 - (x_4 + y_4) \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} - ay_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(16i)	H II
\mathbf{B}_{15}	$-(x_4 + z_4) \mathbf{a}_1 + (y_4 - z_4) \mathbf{a}_2 - (x_4 - y_4) \mathbf{a}_3$	$=$	$ay_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}}$	(16i)	H II
\mathbf{B}_{16}	$(x_4 - z_4) \mathbf{a}_1 - (y_4 + z_4) \mathbf{a}_2 + (x_4 - y_4) \mathbf{a}_3$	$=$	$-ay_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}}$	(16i)	H II
\mathbf{B}_{17}	$(-y_4 + z_4 + \frac{1}{2}) \mathbf{a}_1 + (x_4 + z_4 + \frac{1}{2}) \mathbf{a}_2 + (x_4 - y_4) \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} - ay_4 \hat{\mathbf{y}} + c(z_4 + \frac{1}{2}) \hat{\mathbf{z}}$	(16i)	H II
\mathbf{B}_{18}	$(y_4 + z_4 + \frac{1}{2}) \mathbf{a}_1 + (-x_4 + z_4 + \frac{1}{2}) \mathbf{a}_2 - (x_4 - y_4) \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} + ay_4 \hat{\mathbf{y}} + c(z_4 + \frac{1}{2}) \hat{\mathbf{z}}$	(16i)	H II

$$\begin{aligned}
\mathbf{B}_{19} &= \begin{pmatrix} (x_4 - z_4 + \frac{1}{2}) \mathbf{a}_1 + \\ (y_4 - z_4 + \frac{1}{2}) \mathbf{a}_2 + (x_4 + y_4) \mathbf{a}_3 \end{pmatrix} = ay_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} - c(z_4 - \frac{1}{2}) \hat{\mathbf{z}} & (16i) & \text{H II} \\
\mathbf{B}_{20} &= \begin{pmatrix} -(x_4 + z_4 - \frac{1}{2}) \mathbf{a}_1 - \\ (y_4 + z_4 - \frac{1}{2}) \mathbf{a}_2 - (x_4 + y_4) \mathbf{a}_3 \end{pmatrix} = -ay_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} - c(z_4 - \frac{1}{2}) \hat{\mathbf{z}} & (16i) & \text{H II} \\
\mathbf{B}_{21} &= \begin{pmatrix} (y_5 + z_5) \mathbf{a}_1 + (x_5 + z_5) \mathbf{a}_2 + \\ (x_5 + y_5) \mathbf{a}_3 \end{pmatrix} = ax_5 \hat{\mathbf{x}} + ay_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}} & (16i) & \text{O I} \\
\mathbf{B}_{22} &= \begin{pmatrix} -(y_5 - z_5) \mathbf{a}_1 - (x_5 - z_5) \mathbf{a}_2 - \\ (x_5 + y_5) \mathbf{a}_3 \end{pmatrix} = -ax_5 \hat{\mathbf{x}} - ay_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}} & (16i) & \text{O I} \\
\mathbf{B}_{23} &= \begin{pmatrix} -(x_5 + z_5) \mathbf{a}_1 + (y_5 - z_5) \mathbf{a}_2 - \\ (x_5 - y_5) \mathbf{a}_3 \end{pmatrix} = ay_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}} & (16i) & \text{O I} \\
\mathbf{B}_{24} &= \begin{pmatrix} (x_5 - z_5) \mathbf{a}_1 - (y_5 + z_5) \mathbf{a}_2 + \\ (x_5 - y_5) \mathbf{a}_3 \end{pmatrix} = -ay_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}} & (16i) & \text{O I} \\
\mathbf{B}_{25} &= \begin{pmatrix} (-y_5 + z_5 + \frac{1}{2}) \mathbf{a}_1 + \\ (x_5 + z_5 + \frac{1}{2}) \mathbf{a}_2 + (x_5 - y_5) \mathbf{a}_3 \end{pmatrix} = ax_5 \hat{\mathbf{x}} - ay_5 \hat{\mathbf{y}} + c(z_5 + \frac{1}{2}) \hat{\mathbf{z}} & (16i) & \text{O I} \\
\mathbf{B}_{26} &= \begin{pmatrix} (y_5 + z_5 + \frac{1}{2}) \mathbf{a}_1 + \\ (-x_5 + z_5 + \frac{1}{2}) \mathbf{a}_2 - (x_5 - y_5) \mathbf{a}_3 \end{pmatrix} = -ax_5 \hat{\mathbf{x}} + ay_5 \hat{\mathbf{y}} + c(z_5 + \frac{1}{2}) \hat{\mathbf{z}} & (16i) & \text{O I} \\
\mathbf{B}_{27} &= \begin{pmatrix} (x_5 - z_5 + \frac{1}{2}) \mathbf{a}_1 + \\ (y_5 - z_5 + \frac{1}{2}) \mathbf{a}_2 + (x_5 + y_5) \mathbf{a}_3 \end{pmatrix} = ay_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - c(z_5 - \frac{1}{2}) \hat{\mathbf{z}} & (16i) & \text{O I} \\
\mathbf{B}_{28} &= \begin{pmatrix} -(x_5 + z_5 - \frac{1}{2}) \mathbf{a}_1 - \\ (y_5 + z_5 - \frac{1}{2}) \mathbf{a}_2 - (x_5 + y_5) \mathbf{a}_3 \end{pmatrix} = -ay_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - c(z_5 - \frac{1}{2}) \hat{\mathbf{z}} & (16i) & \text{O I} \\
\mathbf{B}_{29} &= \begin{pmatrix} (y_6 + z_6) \mathbf{a}_1 + (x_6 + z_6) \mathbf{a}_2 + \\ (x_6 + y_6) \mathbf{a}_3 \end{pmatrix} = ax_6 \hat{\mathbf{x}} + ay_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} & (16i) & \text{O II} \\
\mathbf{B}_{30} &= \begin{pmatrix} -(y_6 - z_6) \mathbf{a}_1 - (x_6 - z_6) \mathbf{a}_2 - \\ (x_6 + y_6) \mathbf{a}_3 \end{pmatrix} = -ax_6 \hat{\mathbf{x}} - ay_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} & (16i) & \text{O II} \\
\mathbf{B}_{31} &= \begin{pmatrix} -(x_6 + z_6) \mathbf{a}_1 + (y_6 - z_6) \mathbf{a}_2 - \\ (x_6 - y_6) \mathbf{a}_3 \end{pmatrix} = ay_6 \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} & (16i) & \text{O II} \\
\mathbf{B}_{32} &= \begin{pmatrix} (x_6 - z_6) \mathbf{a}_1 - (y_6 + z_6) \mathbf{a}_2 + \\ (x_6 - y_6) \mathbf{a}_3 \end{pmatrix} = -ay_6 \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} & (16i) & \text{O II} \\
\mathbf{B}_{33} &= \begin{pmatrix} (-y_6 + z_6 + \frac{1}{2}) \mathbf{a}_1 + \\ (x_6 + z_6 + \frac{1}{2}) \mathbf{a}_2 + (x_6 - y_6) \mathbf{a}_3 \end{pmatrix} = ax_6 \hat{\mathbf{x}} - ay_6 \hat{\mathbf{y}} + c(z_6 + \frac{1}{2}) \hat{\mathbf{z}} & (16i) & \text{O II} \\
\mathbf{B}_{34} &= \begin{pmatrix} (y_6 + z_6 + \frac{1}{2}) \mathbf{a}_1 + \\ (-x_6 + z_6 + \frac{1}{2}) \mathbf{a}_2 - (x_6 - y_6) \mathbf{a}_3 \end{pmatrix} = -ax_6 \hat{\mathbf{x}} + ay_6 \hat{\mathbf{y}} + c(z_6 + \frac{1}{2}) \hat{\mathbf{z}} & (16i) & \text{O II} \\
\mathbf{B}_{35} &= \begin{pmatrix} (x_6 - z_6 + \frac{1}{2}) \mathbf{a}_1 + \\ (y_6 - z_6 + \frac{1}{2}) \mathbf{a}_2 + (x_6 + y_6) \mathbf{a}_3 \end{pmatrix} = ay_6 \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} - c(z_6 - \frac{1}{2}) \hat{\mathbf{z}} & (16i) & \text{O II} \\
\mathbf{B}_{36} &= \begin{pmatrix} -(x_6 + z_6 - \frac{1}{2}) \mathbf{a}_1 - \\ (y_6 + z_6 - \frac{1}{2}) \mathbf{a}_2 - (x_6 + y_6) \mathbf{a}_3 \end{pmatrix} = -ay_6 \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} - c(z_6 - \frac{1}{2}) \hat{\mathbf{z}} & (16i) & \text{O II}
\end{aligned}$$

References

- [1] S. K. Sikka and R. Chidambaram, *A neutron diffraction determination of the structure of beryllium sulphate tetrahydrate, BeSO₄ · 4H₂O*, Acta Crystallogr. Sect. B **25**, 310–315 (1969), doi:10.1107/S0567740869002160.