

# Sanidine ( $\text{KAlSi}_3\text{O}_8$ , $S6_7$ ) Structure:

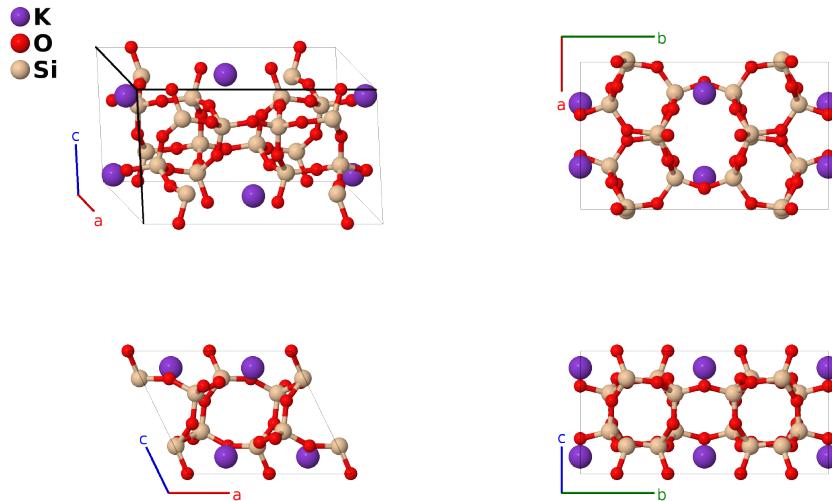
AB8C4\_mC52\_12\_i\_gi3j\_2j-001

This structure originally had the label AB8C4\_mC52\_12\_i\_gi3j\_2j. Calls to that address will be redirected here.

Cite this page as: D. Hicks, M. J. Mehl, M. Esters, C. Oses, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/p/JF0M>

[https://aflow.org/p/AB8C4\\_mC52\\_12\\_i\\_gi3j\\_2j-001](https://aflow.org/p/AB8C4_mC52_12_i_gi3j_2j-001)



<b>Prototype</b>	$\text{AlKO}_8\text{Si}_3$
<b>AFLOW prototype label</b>	AB8C4_mC52_12_i_gi3j_2j-001
<b>Strukturbericht designation</b>	$S6_7$
<b>Mineral name</b>	sanidine
<b>ICSD</b>	202476
<b>Pearson symbol</b>	mC52
<b>Space group number</b>	12
<b>Space group symbol</b>	$C2/m$
<b>AFLOW prototype command</b>	<pre>aflow --proto=AB8C4_mC52_12_i_gi3j_2j-001 --params=a,b/a,c/a,\beta,y_1,x_2,z_2,x_3,z_3,x_4,y_4,z_4,x_5,y_5,z_5,x_6,y_6,z_6,x_7,y_7,z_7,x_8,y_8, z_8</pre>

## Other compounds with this structure

$\text{NaAlSi}_3\text{O}_8$ ,  $(\text{BaKNa})\text{AlSi}_3\text{O}_8$  (orthoclase)

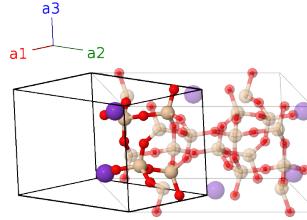
- Beginning with the  $S6_7$  defining paper of (Taylor, 1933) all researchers agree that the sites Si-I and Si-II are actually a random mixture of silicon and aluminum with overall stoichiometry  $\text{AlSi}_3$ . Most results found in (Downs, 2003) assume that this composition holds independently for both sites but (Scambos, 1987) states that the Si-I site is  $\text{Al}_{1.064}\text{Si}_{2.936}$  while the Si-II site is  $\text{Al}_{0.936}\text{Si}_{3.064}$ .

- (Scambos, 1987) list the coordinate  $y_8 = 0.18813$  for the Si-II site in Table 2. This position does not result in the expected  $\text{SiO}_4$  tetrahedra, and the interatomic distances and angles found do not agree with their Table 5. (Downs, 2003) correct this to  $y_8 = 0.11813$ , and this value results in good tetrahedra and reproduces the distances and angles reported by (Scambos, 1987). We use this later value on this page.

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### Base-centered Monoclinic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}b\hat{\mathbf{y}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}} \\ \mathbf{a}_3 &= c\cos\beta\hat{\mathbf{x}} + c\sin\beta\hat{\mathbf{z}}\end{aligned}$$




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### Basis vectors

	Lattice coordinates	Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$-y_1 \mathbf{a}_1 + y_1 \mathbf{a}_2$	$by_1 \hat{\mathbf{y}}$	(4g)	O I
$\mathbf{B}_2$	$y_1 \mathbf{a}_1 - y_1 \mathbf{a}_2$	$-by_1 \hat{\mathbf{y}}$	(4g)	O I
$\mathbf{B}_3$	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + z_2 \mathbf{a}_3$	$(ax_2 + cz_2 \cos\beta) \hat{\mathbf{x}} + cz_2 \sin\beta \hat{\mathbf{z}}$	(4i)	K I
$\mathbf{B}_4$	$-x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 - z_2 \mathbf{a}_3$	$-(ax_2 + cz_2 \cos\beta) \hat{\mathbf{x}} - cz_2 \sin\beta \hat{\mathbf{z}}$	(4i)	K I
$\mathbf{B}_5$	$x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + z_3 \mathbf{a}_3$	$(ax_3 + cz_3 \cos\beta) \hat{\mathbf{x}} + cz_3 \sin\beta \hat{\mathbf{z}}$	(4i)	O II
$\mathbf{B}_6$	$-x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 - z_3 \mathbf{a}_3$	$-(ax_3 + cz_3 \cos\beta) \hat{\mathbf{x}} - cz_3 \sin\beta \hat{\mathbf{z}}$	(4i)	O II
$\mathbf{B}_7$	$(x_4 - y_4) \mathbf{a}_1 + (x_4 + y_4) \mathbf{a}_2 + z_4 \mathbf{a}_3$	$(ax_4 + cz_4 \cos\beta) \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} + cz_4 \sin\beta \hat{\mathbf{z}}$	(8j)	O III
$\mathbf{B}_8$	$-(x_4 + y_4) \mathbf{a}_1 - (x_4 - y_4) \mathbf{a}_2 - z_4 \mathbf{a}_3$	$-(ax_4 + cz_4 \cos\beta) \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} - cz_4 \sin\beta \hat{\mathbf{z}}$	(8j)	O III
$\mathbf{B}_9$	$-(x_4 - y_4) \mathbf{a}_1 - (x_4 + y_4) \mathbf{a}_2 - z_4 \mathbf{a}_3$	$-(ax_4 + cz_4 \cos\beta) \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} - cz_4 \sin\beta \hat{\mathbf{z}}$	(8j)	O III
$\mathbf{B}_{10}$	$(x_4 + y_4) \mathbf{a}_1 + (x_4 - y_4) \mathbf{a}_2 + z_4 \mathbf{a}_3$	$(ax_4 + cz_4 \cos\beta) \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} + cz_4 \sin\beta \hat{\mathbf{z}}$	(8j)	O III
$\mathbf{B}_{11}$	$(x_5 - y_5) \mathbf{a}_1 + (x_5 + y_5) \mathbf{a}_2 + z_5 \mathbf{a}_3$	$(ax_5 + cz_5 \cos\beta) \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} + cz_5 \sin\beta \hat{\mathbf{z}}$	(8j)	O IV
$\mathbf{B}_{12}$	$-(x_5 + y_5) \mathbf{a}_1 - (x_5 - y_5) \mathbf{a}_2 - z_5 \mathbf{a}_3$	$-(ax_5 + cz_5 \cos\beta) \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} - cz_5 \sin\beta \hat{\mathbf{z}}$	(8j)	O IV
$\mathbf{B}_{13}$	$-(x_5 - y_5) \mathbf{a}_1 - (x_5 + y_5) \mathbf{a}_2 - z_5 \mathbf{a}_3$	$-(ax_5 + cz_5 \cos\beta) \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} - cz_5 \sin\beta \hat{\mathbf{z}}$	(8j)	O IV
$\mathbf{B}_{14}$	$(x_5 + y_5) \mathbf{a}_1 + (x_5 - y_5) \mathbf{a}_2 + z_5 \mathbf{a}_3$	$(ax_5 + cz_5 \cos\beta) \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} + cz_5 \sin\beta \hat{\mathbf{z}}$	(8j)	O IV
$\mathbf{B}_{15}$	$(x_6 - y_6) \mathbf{a}_1 + (x_6 + y_6) \mathbf{a}_2 + z_6 \mathbf{a}_3$	$(ax_6 + cz_6 \cos\beta) \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \sin\beta \hat{\mathbf{z}}$	(8j)	O V
$\mathbf{B}_{16}$	$-(x_6 + y_6) \mathbf{a}_1 - (x_6 - y_6) \mathbf{a}_2 - z_6 \mathbf{a}_3$	$-(ax_6 + cz_6 \cos\beta) \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} - cz_6 \sin\beta \hat{\mathbf{z}}$	(8j)	O V
$\mathbf{B}_{17}$	$-(x_6 - y_6) \mathbf{a}_1 - (x_6 + y_6) \mathbf{a}_2 - z_6 \mathbf{a}_3$	$-(ax_6 + cz_6 \cos\beta) \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} - cz_6 \sin\beta \hat{\mathbf{z}}$	(8j)	O V
$\mathbf{B}_{18}$	$(x_6 + y_6) \mathbf{a}_1 + (x_6 - y_6) \mathbf{a}_2 + z_6 \mathbf{a}_3$	$(ax_6 + cz_6 \cos\beta) \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + cz_6 \sin\beta \hat{\mathbf{z}}$	(8j)	O V

$$\begin{aligned}
\mathbf{B}_{19} &= (x_7 - y_7) \mathbf{a}_1 + (x_7 + y_7) \mathbf{a}_2 + z_7 \mathbf{a}_3 & = & (ax_7 + cz_7 \cos \beta) \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} + cz_7 \sin \beta \hat{\mathbf{z}} & (8j) & \text{Si I} \\
\mathbf{B}_{20} &= -(x_7 + y_7) \mathbf{a}_1 - (x_7 - y_7) \mathbf{a}_2 - z_7 \mathbf{a}_3 & = & -(ax_7 + cz_7 \cos \beta) \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} - cz_7 \sin \beta \hat{\mathbf{z}} & (8j) & \text{Si I} \\
\mathbf{B}_{21} &= -(x_7 - y_7) \mathbf{a}_1 - (x_7 + y_7) \mathbf{a}_2 - z_7 \mathbf{a}_3 & = & -(ax_7 + cz_7 \cos \beta) \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} - cz_7 \sin \beta \hat{\mathbf{z}} & (8j) & \text{Si I} \\
\mathbf{B}_{22} &= (x_7 + y_7) \mathbf{a}_1 + (x_7 - y_7) \mathbf{a}_2 + z_7 \mathbf{a}_3 & = & (ax_7 + cz_7 \cos \beta) \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} + cz_7 \sin \beta \hat{\mathbf{z}} & (8j) & \text{Si I} \\
\mathbf{B}_{23} &= (x_8 - y_8) \mathbf{a}_1 + (x_8 + y_8) \mathbf{a}_2 + z_8 \mathbf{a}_3 & = & (ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} + cz_8 \sin \beta \hat{\mathbf{z}} & (8j) & \text{Si II} \\
\mathbf{B}_{24} &= -(x_8 + y_8) \mathbf{a}_1 - (x_8 - y_8) \mathbf{a}_2 - z_8 \mathbf{a}_3 & = & -(ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} - cz_8 \sin \beta \hat{\mathbf{z}} & (8j) & \text{Si II} \\
\mathbf{B}_{25} &= -(x_8 - y_8) \mathbf{a}_1 - (x_8 + y_8) \mathbf{a}_2 - z_8 \mathbf{a}_3 & = & -(ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} - cz_8 \sin \beta \hat{\mathbf{z}} & (8j) & \text{Si II} \\
\mathbf{B}_{26} &= (x_8 + y_8) \mathbf{a}_1 + (x_8 - y_8) \mathbf{a}_2 + z_8 \mathbf{a}_3 & = & (ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} + cz_8 \sin \beta \hat{\mathbf{z}} & (8j) & \text{Si II}
\end{aligned}$$

## References

- [1] T. A. Scambos, J. R. Smyth, and T. C. McCormick, *Crystal-structure refinement of high sanidine from the upper mantle*, Am. Mineral. **72**, 973–978 (1987).
- [2] W. H. Taylor, *The Structure of Sanidine and Other Felspars*, Z. Kristallogr. **85**, 425–442 (1933), doi:10.1524/zkri.1933.85.1.425.
- [3] R. T. Downs and M. Hall-Wallace, *The American Mineralogist Crystal Structure Database*, Am. Mineral. **88**, 247–250 (2003).