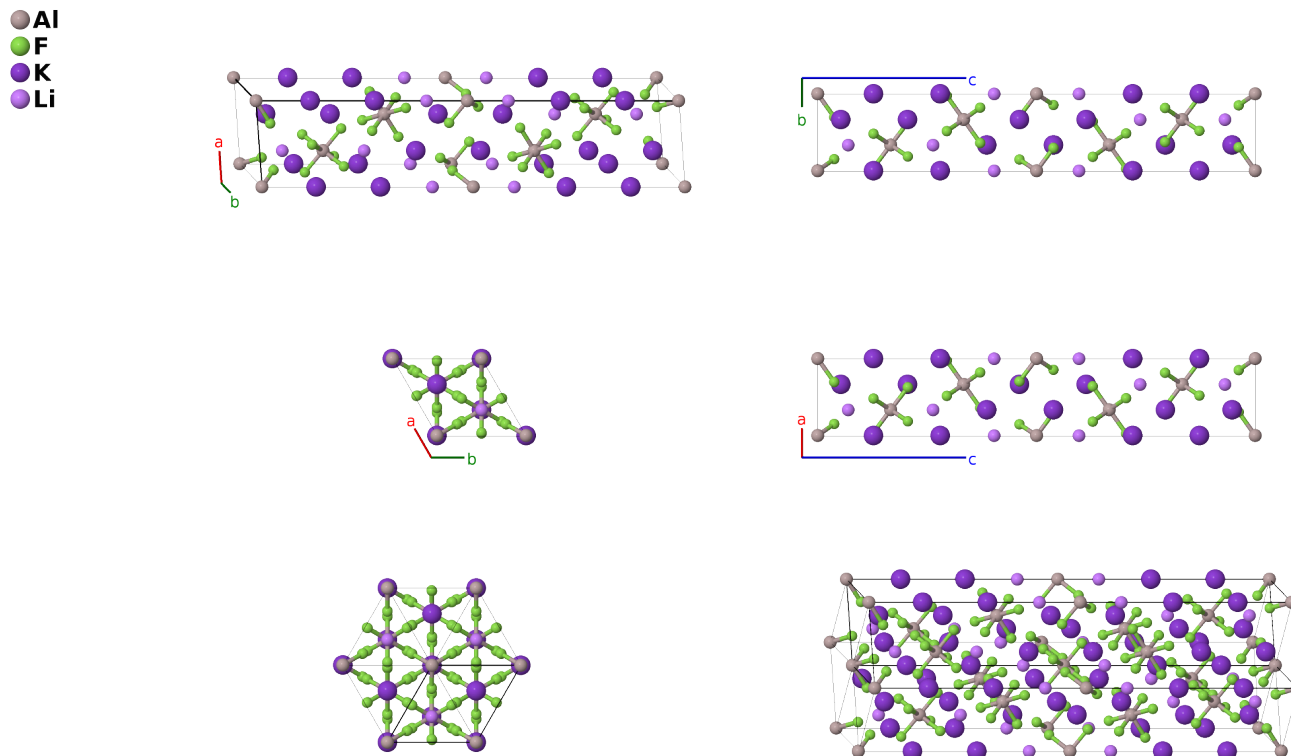


High Temperature K_2LiAlF_6 Structure: AB6C2D_hR20_166_ab_2h_2c_c-001

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<https://aflow.org/p/KTF5>

https://aflow.org/p/AB6C2D_hR20_166_ab_2h_2c_c-001



Prototype	AlF_6K_2Li
AFLOW prototype label	AB6C2D_hR20_166_ab_2h_2c_c-001
ICSD	48149
Pearson symbol	hR20
Space group number	166
Space group symbol	$R\bar{3}m$
AFLOW prototype command	<pre>aflow --proto=AB6C2D_hR20_166_ab_2h_2c_c-001 --params=a, c/a, x3, x4, x5, x6, z6, x7, z7</pre>

Other compounds with this structure

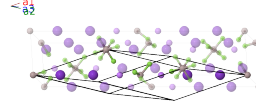
Ba_2MnTeO_6 , Cs_2NaCrF_6

- This is the high temperature phase of K_2LiAlF_6 , stable above $650^\circ C$ (Tressaud, 1984). The low-temperature structure is hexagonal, but its exact space group is uncertain.

- Hexagonal settings of this structure can be obtained with the option `--hex`.

Rhombohedral primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a \hat{\mathbf{y}} + \frac{1}{3}c \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{\sqrt{3}}a \hat{\mathbf{y}} + \frac{1}{3}c \hat{\mathbf{z}} \\ \mathbf{a}_3 &= -\frac{1}{2}a \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a \hat{\mathbf{y}} + \frac{1}{3}c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$=$	0	$=$	0	(1a) Al I
\mathbf{B}_2	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}c \hat{\mathbf{z}}$	(1b) Al II
\mathbf{B}_3	$=$	$x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	$=$	$cx_3 \hat{\mathbf{z}}$	(2c) K I
\mathbf{B}_4	$=$	$-x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 - x_3 \mathbf{a}_3$	$=$	$-cx_3 \hat{\mathbf{z}}$	(2c) K I
\mathbf{B}_5	$=$	$x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + x_4 \mathbf{a}_3$	$=$	$cx_4 \hat{\mathbf{z}}$	(2c) K II
\mathbf{B}_6	$=$	$-x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 - x_4 \mathbf{a}_3$	$=$	$-cx_4 \hat{\mathbf{z}}$	(2c) K II
\mathbf{B}_7	$=$	$x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	$=$	$cx_5 \hat{\mathbf{z}}$	(2c) Li I
\mathbf{B}_8	$=$	$-x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$	$=$	$-cx_5 \hat{\mathbf{z}}$	(2c) Li I
\mathbf{B}_9	$=$	$x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$\frac{1}{2}a(x_6 - z_6) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a(x_6 - z_6) \hat{\mathbf{y}} + \frac{1}{3}c(2x_6 + z_6) \hat{\mathbf{z}}$	(6h) F I
\mathbf{B}_{10}	$=$	$z_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 + x_6 \mathbf{a}_3$	$=$	$-\frac{1}{2}a(x_6 - z_6) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a(x_6 - z_6) \hat{\mathbf{y}} + \frac{1}{3}c(2x_6 + z_6) \hat{\mathbf{z}}$	(6h) F I
\mathbf{B}_{11}	$=$	$x_6 \mathbf{a}_1 + z_6 \mathbf{a}_2 + x_6 \mathbf{a}_3$	$=$	$-\frac{1}{\sqrt{3}}a(x_6 - z_6) \hat{\mathbf{y}} + \frac{1}{3}c(2x_6 + z_6) \hat{\mathbf{z}}$	(6h) F I
\mathbf{B}_{12}	$=$	$-z_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 - x_6 \mathbf{a}_3$	$=$	$\frac{1}{2}a(x_6 - z_6) \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a(x_6 - z_6) \hat{\mathbf{y}} - \frac{1}{3}c(2x_6 + z_6) \hat{\mathbf{z}}$	(6h) F I
\mathbf{B}_{13}	$=$	$-x_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$-\frac{1}{2}a(x_6 - z_6) \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a(x_6 - z_6) \hat{\mathbf{y}} - \frac{1}{3}c(2x_6 + z_6) \hat{\mathbf{z}}$	(6h) F I
\mathbf{B}_{14}	$=$	$-x_6 \mathbf{a}_1 - z_6 \mathbf{a}_2 - x_6 \mathbf{a}_3$	$=$	$\frac{1}{\sqrt{3}}a(x_6 - z_6) \hat{\mathbf{y}} - \frac{1}{3}c(2x_6 + z_6) \hat{\mathbf{z}}$	(6h) F I
\mathbf{B}_{15}	$=$	$x_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$\frac{1}{2}a(x_7 - z_7) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a(x_7 - z_7) \hat{\mathbf{y}} + \frac{1}{3}c(2x_7 + z_7) \hat{\mathbf{z}}$	(6h) F II
\mathbf{B}_{16}	$=$	$z_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$-\frac{1}{2}a(x_7 - z_7) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a(x_7 - z_7) \hat{\mathbf{y}} + \frac{1}{3}c(2x_7 + z_7) \hat{\mathbf{z}}$	(6h) F II
\mathbf{B}_{17}	$=$	$x_7 \mathbf{a}_1 + z_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$-\frac{1}{\sqrt{3}}a(x_7 - z_7) \hat{\mathbf{y}} + \frac{1}{3}c(2x_7 + z_7) \hat{\mathbf{z}}$	(6h) F II
\mathbf{B}_{18}	$=$	$-z_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 - x_7 \mathbf{a}_3$	$=$	$\frac{1}{2}a(x_7 - z_7) \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a(x_7 - z_7) \hat{\mathbf{y}} - \frac{1}{3}c(2x_7 + z_7) \hat{\mathbf{z}}$	(6h) F II
\mathbf{B}_{19}	$=$	$-x_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 - z_7 \mathbf{a}_3$	$=$	$-\frac{1}{2}a(x_7 - z_7) \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a(x_7 - z_7) \hat{\mathbf{y}} - \frac{1}{3}c(2x_7 + z_7) \hat{\mathbf{z}}$	(6h) F II
\mathbf{B}_{20}	$=$	$-x_7 \mathbf{a}_1 - z_7 \mathbf{a}_2 - x_7 \mathbf{a}_3$	$=$	$\frac{1}{\sqrt{3}}a(x_7 - z_7) \hat{\mathbf{y}} - \frac{1}{3}c(2x_7 + z_7) \hat{\mathbf{z}}$	(6h) F II

References

- [1] A. Tressaud, J. Darriet, P. Lagassié, J. Grannec, and P. Hagenmuller, *On new K_2LiMF_6 phases ($M = d$ -element, Al, Ga, In): Crystal structure of the rhombohedral high-temperature form of K_2LiAlF_6* , Mater. Res. Bull. **19**, 983–988 (1984), doi:10.1016/0025-5408(84)90211-3.