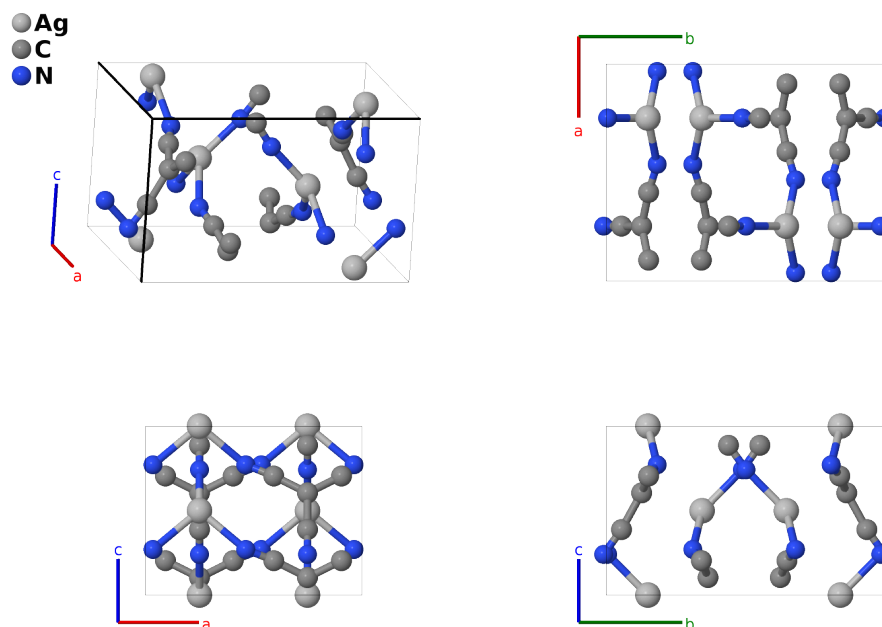


Room Temperature AgC_4N_3 Structure: AB4C3_oI32_46_b_2bc_bc-001

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<https://afLOW.org/p/77VH>

https://afLOW.org/p/AB4C3_oI32_46_b_2bc_bc-001

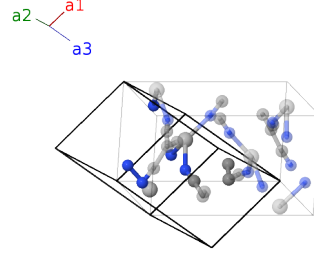


Prototype	AgC_4N_3
AFLOW prototype label	AB4C3_oI32_46_b_2bc_bc-001
ICSD	43823
Pearson symbol	oI32
Space group number	46
Space group symbol	$Ima2$
AFLOW prototype command	<pre>afLOW --proto=AB4C3_oI32_46_b_2bc_bc-001 --params=a, b/a, c/a, y1, z1, y2, z2, y3, z3, y4, z4, x5, y5, z5, x6, y6, z6</pre>

- This is the room temperature structure of AgC_4N_3 . Around 100K it undergoes a significant change in structure which does not change the space group or Wyckoff positions. (Hodgson, 2014). This can be found on the low temperature AgC_4N_3 structure page.
- In chemical literature this is often referred to as $\text{Ag}(\text{tcm})$, where tcm is an abbreviation for tricyanomethanide.
- (Konnert, 2014) swapped the x - and z -axes compared to the standard setting of space group $Ima2$ #46. We used AFLOW to transform this to the standard orientation.

Body-centered Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$(y_1 + z_1) \mathbf{a}_1 + (z_1 + \frac{1}{4}) \mathbf{a}_2 + (y_1 + \frac{1}{4}) \mathbf{a}_3$	=	$\frac{1}{4}a \hat{\mathbf{x}} + by_1 \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(4b)	Ag I
\mathbf{B}_2	$-(y_1 - z_1) \mathbf{a}_1 + (z_1 + \frac{3}{4}) \mathbf{a}_2 - (y_1 - \frac{3}{4}) \mathbf{a}_3$	=	$\frac{3}{4}a \hat{\mathbf{x}} - by_1 \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(4b)	Ag I
\mathbf{B}_3	$(y_2 + z_2) \mathbf{a}_1 + (z_2 + \frac{1}{4}) \mathbf{a}_2 + (y_2 + \frac{1}{4}) \mathbf{a}_3$	=	$\frac{1}{4}a \hat{\mathbf{x}} + by_2 \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(4b)	C I
\mathbf{B}_4	$-(y_2 - z_2) \mathbf{a}_1 + (z_2 + \frac{3}{4}) \mathbf{a}_2 - (y_2 - \frac{3}{4}) \mathbf{a}_3$	=	$\frac{3}{4}a \hat{\mathbf{x}} - by_2 \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(4b)	C I
\mathbf{B}_5	$(y_3 + z_3) \mathbf{a}_1 + (z_3 + \frac{1}{4}) \mathbf{a}_2 + (y_3 + \frac{1}{4}) \mathbf{a}_3$	=	$\frac{1}{4}a \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(4b)	C II
\mathbf{B}_6	$-(y_3 - z_3) \mathbf{a}_1 + (z_3 + \frac{3}{4}) \mathbf{a}_2 - (y_3 - \frac{3}{4}) \mathbf{a}_3$	=	$\frac{3}{4}a \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(4b)	C II
\mathbf{B}_7	$(y_4 + z_4) \mathbf{a}_1 + (z_4 + \frac{1}{4}) \mathbf{a}_2 + (y_4 + \frac{1}{4}) \mathbf{a}_3$	=	$\frac{1}{4}a \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(4b)	N I
\mathbf{B}_8	$-(y_4 - z_4) \mathbf{a}_1 + (z_4 + \frac{3}{4}) \mathbf{a}_2 - (y_4 - \frac{3}{4}) \mathbf{a}_3$	=	$\frac{3}{4}a \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(4b)	N I
\mathbf{B}_9	$(y_5 + z_5) \mathbf{a}_1 + (x_5 + z_5) \mathbf{a}_2 + (x_5 + y_5) \mathbf{a}_3$	=	$ax_5 \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(8c)	C III
\mathbf{B}_{10}	$-(y_5 - z_5) \mathbf{a}_1 - (x_5 - z_5) \mathbf{a}_2 - (x_5 + y_5) \mathbf{a}_3$	=	$-ax_5 \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(8c)	C III
\mathbf{B}_{11}	$-(y_5 - z_5) \mathbf{a}_1 + (x_5 + z_5 + \frac{1}{2}) \mathbf{a}_2 + (x_5 - y_5 + \frac{1}{2}) \mathbf{a}_3$	=	$a(x_5 + \frac{1}{2}) \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(8c)	C III
\mathbf{B}_{12}	$(y_5 + z_5) \mathbf{a}_1 + (-x_5 + z_5 + \frac{1}{2}) \mathbf{a}_2 + (-x_5 + y_5 + \frac{1}{2}) \mathbf{a}_3$	=	$-a(x_5 - \frac{1}{2}) \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(8c)	C III
\mathbf{B}_{13}	$(y_6 + z_6) \mathbf{a}_1 + (x_6 + z_6) \mathbf{a}_2 + (x_6 + y_6) \mathbf{a}_3$	=	$ax_6 \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(8c)	N II
\mathbf{B}_{14}	$-(y_6 - z_6) \mathbf{a}_1 - (x_6 - z_6) \mathbf{a}_2 - (x_6 + y_6) \mathbf{a}_3$	=	$-ax_6 \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(8c)	N II
\mathbf{B}_{15}	$-(y_6 - z_6) \mathbf{a}_1 + (x_6 + z_6 + \frac{1}{2}) \mathbf{a}_2 + (x_6 - y_6 + \frac{1}{2}) \mathbf{a}_3$	=	$a(x_6 + \frac{1}{2}) \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(8c)	N II

$$\mathbf{B}_{16} = \begin{pmatrix} (y_6 + z_6) \mathbf{a}_1 + \\ (-x_6 + z_6 + \frac{1}{2}) \mathbf{a}_2 + \\ (-x_6 + y_6 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = -a \left(x_6 - \frac{1}{2}\right) \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} \quad (8c) \quad \text{N II}$$

References

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- [2] S. A. Hodgson, J. Adamson, S. J. Hunt, M. J. Cliffe, A. B. Cairns, A. L. Thompson, M. G. Tucker, N. P. Funnell, and A. L. Goodwin, *Negative area compressibility in silver(I) tricyanomethanide*, *Chem. Commun.* **50**, 5264–5266 (2014), doi:10.1039/C3CC47032F.