

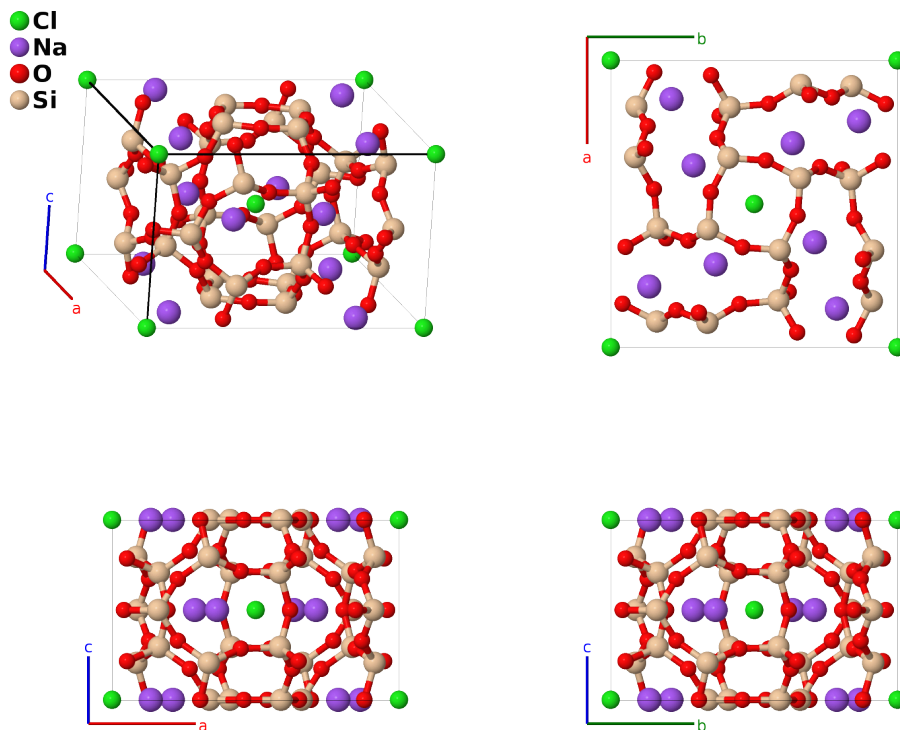
Marialite Scapolite $[\text{Na}_4\text{Cl}(\text{AlSi}_3)_3\text{O}_{24}, S6_4]$ Structure: AB4C24D12_tI82_87_a_h_2h2i_hi-001

This structure originally had the label AB4C24D12_tI82_87_a_h_2h2i_hi. Calls to that address will be redirected here.

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<https://aflow.org/p/8NAD>

https://aflow.org/p/AB4C24D12_tI82_87_a_h_2h2i_hi-001

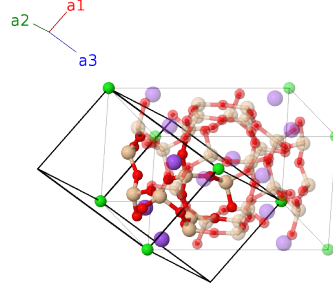


Prototype	$\text{Al}_3\text{ClNa}_4\text{O}_{24}\text{Si}_9$
AFLOW prototype label	AB4C24D12_tI82_87_a_h_2h2i_hi-001
<i>Strukturbericht</i> designation	$S6_4$
Mineral name	marialite scapolite
ICSD	9502
Pearson symbol	tI82
Space group number	87
Space group symbol	$I4/m$
AFLOW prototype command	<code>aflow --proto=AB4C24D12_tI82_87_a_h_2h2i_hi-001 --params=a, c/a, x2, y2, x3, y3, x4, y4, x5, y5, x6, y6, z6, x7, y7, z7, x8, y8, z8</code>

- (Papike, 1965) found that the composition of the Si-II (16h) site was actually $\text{Al}_{0.458}\text{Si}_{0.542}$, and which we list as silicon. This is richer in aluminum than assumed by Pauli, who gave the total aluminum/silicon composition as AlSi_3 . If we assume that the Si-I (8h) site is only filled by silicon atoms, then Pauli's composition for the Si-II site is $\text{Al}_{0.375}\text{Si}_{0.625}$. The name "marialite" scapolite distinguishes this from meionite scapolite, which replaces the sodium atoms by calcium but also includes SiO_4 and CO_3 , which replace the chlorine atoms. According to Pauli, "The minerals of the scapolite group can be considered as solid solution of two end-members, marialite, $\text{Na}_4\text{Al}_3\text{Si}_9\text{O}_{24}\text{Cl}$, and meionite, $\text{Ca}_4\text{Al}_6\text{Si}_6\text{O}_{24}(\text{SO}_4, \text{CO}_3)$, in various proportions."

Body-centered Tetragonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$=$	0	$=$	0	(2a) Cl I
\mathbf{B}_2	$=$	$y_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + (x_2 + y_2) \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + ay_2 \hat{\mathbf{y}}$	(8h) Na I
\mathbf{B}_3	$=$	$-y_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 - (x_2 + y_2) \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} - ay_2 \hat{\mathbf{y}}$	(8h) Na I
\mathbf{B}_4	$=$	$x_2 \mathbf{a}_1 - y_2 \mathbf{a}_2 + (x_2 - y_2) \mathbf{a}_3$	$=$	$-ay_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}}$	(8h) Na I
\mathbf{B}_5	$=$	$-x_2 \mathbf{a}_1 + y_2 \mathbf{a}_2 - (x_2 - y_2) \mathbf{a}_3$	$=$	$ay_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}}$	(8h) Na I
\mathbf{B}_6	$=$	$y_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + (x_3 + y_3) \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + ay_3 \hat{\mathbf{y}}$	(8h) O I
\mathbf{B}_7	$=$	$-y_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 - (x_3 + y_3) \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} - ay_3 \hat{\mathbf{y}}$	(8h) O I
\mathbf{B}_8	$=$	$x_3 \mathbf{a}_1 - y_3 \mathbf{a}_2 + (x_3 - y_3) \mathbf{a}_3$	$=$	$-ay_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}}$	(8h) O I
\mathbf{B}_9	$=$	$-x_3 \mathbf{a}_1 + y_3 \mathbf{a}_2 - (x_3 - y_3) \mathbf{a}_3$	$=$	$ay_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}}$	(8h) O I
\mathbf{B}_{10}	$=$	$y_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + (x_4 + y_4) \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + ay_4 \hat{\mathbf{y}}$	(8h) O II
\mathbf{B}_{11}	$=$	$-y_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 - (x_4 + y_4) \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} - ay_4 \hat{\mathbf{y}}$	(8h) O II
\mathbf{B}_{12}	$=$	$x_4 \mathbf{a}_1 - y_4 \mathbf{a}_2 + (x_4 - y_4) \mathbf{a}_3$	$=$	$-ay_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}}$	(8h) O II
\mathbf{B}_{13}	$=$	$-x_4 \mathbf{a}_1 + y_4 \mathbf{a}_2 - (x_4 - y_4) \mathbf{a}_3$	$=$	$ay_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}}$	(8h) O II
\mathbf{B}_{14}	$=$	$y_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + (x_5 + y_5) \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} + ay_5 \hat{\mathbf{y}}$	(8h) Si I
\mathbf{B}_{15}	$=$	$-y_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - (x_5 + y_5) \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} - ay_5 \hat{\mathbf{y}}$	(8h) Si I
\mathbf{B}_{16}	$=$	$x_5 \mathbf{a}_1 - y_5 \mathbf{a}_2 + (x_5 - y_5) \mathbf{a}_3$	$=$	$-ay_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}}$	(8h) Si I
\mathbf{B}_{17}	$=$	$-x_5 \mathbf{a}_1 + y_5 \mathbf{a}_2 - (x_5 - y_5) \mathbf{a}_3$	$=$	$ay_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}}$	(8h) Si I
\mathbf{B}_{18}	$=$	$(y_6 + z_6) \mathbf{a}_1 + (x_6 + z_6) \mathbf{a}_2 + (x_6 + y_6) \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} + ay_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(16i) O III
\mathbf{B}_{19}	$=$	$-(y_6 - z_6) \mathbf{a}_1 - (x_6 - z_6) \mathbf{a}_2 - (x_6 + y_6) \mathbf{a}_3$	$=$	$-ax_6 \hat{\mathbf{x}} - ay_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(16i) O III
\mathbf{B}_{20}	$=$	$(x_6 + z_6) \mathbf{a}_1 - (y_6 - z_6) \mathbf{a}_2 + (x_6 - y_6) \mathbf{a}_3$	$=$	$-ay_6 \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(16i) O III

$$\begin{aligned}
\mathbf{B}_{21} &= \begin{matrix} -(x_6 - z_6) \mathbf{a}_1 + (y_6 + z_6) \mathbf{a}_2 - \\ (x_6 - y_6) \mathbf{a}_3 \end{matrix} = ay_6 \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} & (16i) & \text{O III} \\
\mathbf{B}_{22} &= \begin{matrix} -(y_6 + z_6) \mathbf{a}_1 - (x_6 + z_6) \mathbf{a}_2 - \\ (x_6 + y_6) \mathbf{a}_3 \end{matrix} = -ax_6 \hat{\mathbf{x}} - ay_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} & (16i) & \text{O III} \\
\mathbf{B}_{23} &= \begin{matrix} (y_6 - z_6) \mathbf{a}_1 + (x_6 - z_6) \mathbf{a}_2 + \\ (x_6 + y_6) \mathbf{a}_3 \end{matrix} = ax_6 \hat{\mathbf{x}} + ay_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} & (16i) & \text{O III} \\
\mathbf{B}_{24} &= \begin{matrix} -(x_6 + z_6) \mathbf{a}_1 + (y_6 - z_6) \mathbf{a}_2 - \\ (x_6 - y_6) \mathbf{a}_3 \end{matrix} = ay_6 \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} & (16i) & \text{O III} \\
\mathbf{B}_{25} &= \begin{matrix} (x_6 - z_6) \mathbf{a}_1 - (y_6 + z_6) \mathbf{a}_2 + \\ (x_6 - y_6) \mathbf{a}_3 \end{matrix} = -ay_6 \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} & (16i) & \text{O III} \\
\mathbf{B}_{26} &= \begin{matrix} (y_7 + z_7) \mathbf{a}_1 + (x_7 + z_7) \mathbf{a}_2 + \\ (x_7 + y_7) \mathbf{a}_3 \end{matrix} = ax_7 \hat{\mathbf{x}} + ay_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (16i) & \text{O IV} \\
\mathbf{B}_{27} &= \begin{matrix} -(y_7 - z_7) \mathbf{a}_1 - (x_7 - z_7) \mathbf{a}_2 - \\ (x_7 + y_7) \mathbf{a}_3 \end{matrix} = -ax_7 \hat{\mathbf{x}} - ay_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (16i) & \text{O IV} \\
\mathbf{B}_{28} &= \begin{matrix} (x_7 + z_7) \mathbf{a}_1 - (y_7 - z_7) \mathbf{a}_2 + \\ (x_7 - y_7) \mathbf{a}_3 \end{matrix} = -ay_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (16i) & \text{O IV} \\
\mathbf{B}_{29} &= \begin{matrix} -(x_7 - z_7) \mathbf{a}_1 + (y_7 + z_7) \mathbf{a}_2 - \\ (x_7 - y_7) \mathbf{a}_3 \end{matrix} = ay_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (16i) & \text{O IV} \\
\mathbf{B}_{30} &= \begin{matrix} -(y_7 + z_7) \mathbf{a}_1 - (x_7 + z_7) \mathbf{a}_2 - \\ (x_7 + y_7) \mathbf{a}_3 \end{matrix} = -ax_7 \hat{\mathbf{x}} - ay_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (16i) & \text{O IV} \\
\mathbf{B}_{31} &= \begin{matrix} (y_7 - z_7) \mathbf{a}_1 + (x_7 - z_7) \mathbf{a}_2 + \\ (x_7 + y_7) \mathbf{a}_3 \end{matrix} = ax_7 \hat{\mathbf{x}} + ay_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (16i) & \text{O IV} \\
\mathbf{B}_{32} &= \begin{matrix} -(x_7 + z_7) \mathbf{a}_1 + (y_7 - z_7) \mathbf{a}_2 - \\ (x_7 - y_7) \mathbf{a}_3 \end{matrix} = ay_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (16i) & \text{O IV} \\
\mathbf{B}_{33} &= \begin{matrix} (x_7 - z_7) \mathbf{a}_1 - (y_7 + z_7) \mathbf{a}_2 + \\ (x_7 - y_7) \mathbf{a}_3 \end{matrix} = -ay_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (16i) & \text{O IV} \\
\mathbf{B}_{34} &= \begin{matrix} (y_8 + z_8) \mathbf{a}_1 + (x_8 + z_8) \mathbf{a}_2 + \\ (x_8 + y_8) \mathbf{a}_3 \end{matrix} = ax_8 \hat{\mathbf{x}} + ay_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}} & (16i) & \text{Si II} \\
\mathbf{B}_{35} &= \begin{matrix} -(y_8 - z_8) \mathbf{a}_1 - (x_8 - z_8) \mathbf{a}_2 - \\ (x_8 + y_8) \mathbf{a}_3 \end{matrix} = -ax_8 \hat{\mathbf{x}} - ay_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}} & (16i) & \text{Si II} \\
\mathbf{B}_{36} &= \begin{matrix} (x_8 + z_8) \mathbf{a}_1 - (y_8 - z_8) \mathbf{a}_2 + \\ (x_8 - y_8) \mathbf{a}_3 \end{matrix} = -ay_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}} & (16i) & \text{Si II} \\
\mathbf{B}_{37} &= \begin{matrix} -(x_8 - z_8) \mathbf{a}_1 + (y_8 + z_8) \mathbf{a}_2 - \\ (x_8 - y_8) \mathbf{a}_3 \end{matrix} = ay_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}} & (16i) & \text{Si II} \\
\mathbf{B}_{38} &= \begin{matrix} -(y_8 + z_8) \mathbf{a}_1 - (x_8 + z_8) \mathbf{a}_2 - \\ (x_8 + y_8) \mathbf{a}_3 \end{matrix} = -ax_8 \hat{\mathbf{x}} - ay_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}} & (16i) & \text{Si II} \\
\mathbf{B}_{39} &= \begin{matrix} (y_8 - z_8) \mathbf{a}_1 + (x_8 - z_8) \mathbf{a}_2 + \\ (x_8 + y_8) \mathbf{a}_3 \end{matrix} = ax_8 \hat{\mathbf{x}} + ay_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}} & (16i) & \text{Si II} \\
\mathbf{B}_{40} &= \begin{matrix} -(x_8 + z_8) \mathbf{a}_1 + (y_8 - z_8) \mathbf{a}_2 - \\ (x_8 - y_8) \mathbf{a}_3 \end{matrix} = ay_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}} & (16i) & \text{Si II} \\
\mathbf{B}_{41} &= \begin{matrix} (x_8 - z_8) \mathbf{a}_1 - (y_8 + z_8) \mathbf{a}_2 + \\ (x_8 - y_8) \mathbf{a}_3 \end{matrix} = -ay_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}} & (16i) & \text{Si II}
\end{aligned}$$

References

- [1] J. J. Papike and T. Zoltai, *The crystal structure of a marialite scapolite*, Am. Mineral. **50**, 641–655 (1965).
- [2] L. Pauling, *The Structure of Some Sodium and Calcium Aluminosilicates*, Proc. Natl. Acad. Sci. **16**, 453–459 (1930), doi:10.1073/pnas.16.7.453.