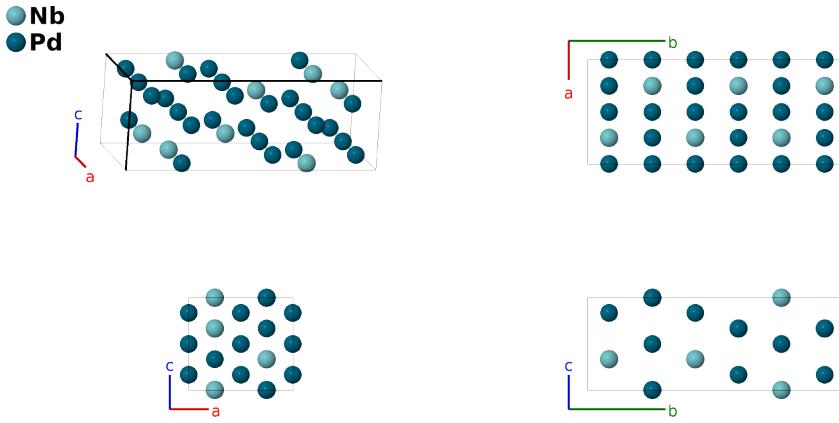


# $\beta$ -NbPd<sub>3</sub> Structure: AB<sub>3</sub>\_oP24\_59\_ae\_befg-001

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<https://aflow.org/p/5BSF>

[https://aflow.org/p/AB3\\_oP24\\_59\\_ae\\_befg-001](https://aflow.org/p/AB3_oP24_59_ae_befg-001)



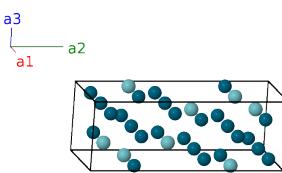
<b>Prototype</b>	NbPd <sub>3</sub>
<b>AFLOW prototype label</b>	AB <sub>3</sub> _oP24_59_ae_befg-001
<b>ICSD</b>	105193
<b>Pearson symbol</b>	oP24
<b>Space group number</b>	59
<b>Space group symbol</b>	<i>Pmmn</i>
<b>AFLOW prototype command</b>	<code>aflow --proto=AB3_oP24_59_ae_befg-001 --params=a,b/a,c/a,z<sub>1</sub>,z<sub>2</sub>,y<sub>3</sub>,z<sub>3</sub>,y<sub>4</sub>,z<sub>4</sub>,x<sub>5</sub>,z<sub>5</sub>,x<sub>6</sub>,y<sub>6</sub>,z<sub>6</sub></code>

- Although  $\beta$ -NbPd<sub>3</sub> and  $\alpha$ -NbPd<sub>3</sub>, which has the  $D0_{22}$  structure, coexist over a wide range of temperatures, it is thought that  $\alpha$ -NbPd<sub>3</sub> is the ground state (Chandrasekharaiyah, 1988).
- (Giessen, 1964) state that their coordinates are given in the *Pmmn* setting of space group #59, but it is apparent that they actually use the *Pmnm* setting. We transformed this to *Pmmn*.

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## Simple Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= b \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}}\end{aligned}$$




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## Basis vectors

	Lattice coordinates	=	Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$\frac{1}{4}\mathbf{a}_1 + \frac{1}{4}\mathbf{a}_2 + z_1\mathbf{a}_3$	=	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}b\hat{\mathbf{y}} + cz_1\hat{\mathbf{z}}$	(2a)	Nb I
$\mathbf{B}_2$	$\frac{3}{4}\mathbf{a}_1 + \frac{3}{4}\mathbf{a}_2 - z_1\mathbf{a}_3$	=	$\frac{3}{4}a\hat{\mathbf{x}} + \frac{3}{4}b\hat{\mathbf{y}} - cz_1\hat{\mathbf{z}}$	(2a)	Nb I
$\mathbf{B}_3$	$\frac{1}{4}\mathbf{a}_1 + \frac{3}{4}\mathbf{a}_2 + z_2\mathbf{a}_3$	=	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{3}{4}b\hat{\mathbf{y}} + cz_2\hat{\mathbf{z}}$	(2b)	Pd I
$\mathbf{B}_4$	$\frac{3}{4}\mathbf{a}_1 + \frac{1}{4}\mathbf{a}_2 - z_2\mathbf{a}_3$	=	$\frac{3}{4}a\hat{\mathbf{x}} + \frac{1}{4}b\hat{\mathbf{y}} - cz_2\hat{\mathbf{z}}$	(2b)	Pd I
$\mathbf{B}_5$	$\frac{1}{4}\mathbf{a}_1 + y_3\mathbf{a}_2 + z_3\mathbf{a}_3$	=	$\frac{1}{4}a\hat{\mathbf{x}} + by_3\hat{\mathbf{y}} + cz_3\hat{\mathbf{z}}$	(4e)	Nb II
$\mathbf{B}_6$	$\frac{1}{4}\mathbf{a}_1 - (y_3 - \frac{1}{2})\mathbf{a}_2 + z_3\mathbf{a}_3$	=	$\frac{1}{4}a\hat{\mathbf{x}} - b(y_3 - \frac{1}{2})\hat{\mathbf{y}} + cz_3\hat{\mathbf{z}}$	(4e)	Nb II
$\mathbf{B}_7$	$\frac{3}{4}\mathbf{a}_1 + (y_3 + \frac{1}{2})\mathbf{a}_2 - z_3\mathbf{a}_3$	=	$\frac{3}{4}a\hat{\mathbf{x}} + b(y_3 + \frac{1}{2})\hat{\mathbf{y}} - cz_3\hat{\mathbf{z}}$	(4e)	Nb II
$\mathbf{B}_8$	$\frac{3}{4}\mathbf{a}_1 - y_3\mathbf{a}_2 - z_3\mathbf{a}_3$	=	$\frac{3}{4}a\hat{\mathbf{x}} - by_3\hat{\mathbf{y}} - cz_3\hat{\mathbf{z}}$	(4e)	Nb II
$\mathbf{B}_9$	$\frac{1}{4}\mathbf{a}_1 + y_4\mathbf{a}_2 + z_4\mathbf{a}_3$	=	$\frac{1}{4}a\hat{\mathbf{x}} + by_4\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(4e)	Pd II
$\mathbf{B}_{10}$	$\frac{1}{4}\mathbf{a}_1 - (y_4 - \frac{1}{2})\mathbf{a}_2 + z_4\mathbf{a}_3$	=	$\frac{1}{4}a\hat{\mathbf{x}} - b(y_4 - \frac{1}{2})\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(4e)	Pd II
$\mathbf{B}_{11}$	$\frac{3}{4}\mathbf{a}_1 + (y_4 + \frac{1}{2})\mathbf{a}_2 - z_4\mathbf{a}_3$	=	$\frac{3}{4}a\hat{\mathbf{x}} + b(y_4 + \frac{1}{2})\hat{\mathbf{y}} - cz_4\hat{\mathbf{z}}$	(4e)	Pd II
$\mathbf{B}_{12}$	$\frac{3}{4}\mathbf{a}_1 - y_4\mathbf{a}_2 - z_4\mathbf{a}_3$	=	$\frac{3}{4}a\hat{\mathbf{x}} - by_4\hat{\mathbf{y}} - cz_4\hat{\mathbf{z}}$	(4e)	Pd II
$\mathbf{B}_{13}$	$x_5\mathbf{a}_1 + \frac{1}{4}\mathbf{a}_2 + z_5\mathbf{a}_3$	=	$ax_5\hat{\mathbf{x}} + \frac{1}{4}b\hat{\mathbf{y}} + cz_5\hat{\mathbf{z}}$	(4f)	Pd III
$\mathbf{B}_{14}$	$-(x_5 - \frac{1}{2})\mathbf{a}_1 + \frac{1}{4}\mathbf{a}_2 + z_5\mathbf{a}_3$	=	$-a(x_5 - \frac{1}{2})\hat{\mathbf{x}} + \frac{1}{4}b\hat{\mathbf{y}} + cz_5\hat{\mathbf{z}}$	(4f)	Pd III
$\mathbf{B}_{15}$	$-x_5\mathbf{a}_1 + \frac{3}{4}\mathbf{a}_2 - z_5\mathbf{a}_3$	=	$-ax_5\hat{\mathbf{x}} + \frac{3}{4}b\hat{\mathbf{y}} - cz_5\hat{\mathbf{z}}$	(4f)	Pd III
$\mathbf{B}_{16}$	$(x_5 + \frac{1}{2})\mathbf{a}_1 + \frac{3}{4}\mathbf{a}_2 - z_5\mathbf{a}_3$	=	$a(x_5 + \frac{1}{2})\hat{\mathbf{x}} + \frac{3}{4}b\hat{\mathbf{y}} - cz_5\hat{\mathbf{z}}$	(4f)	Pd III
$\mathbf{B}_{17}$	$x_6\mathbf{a}_1 + y_6\mathbf{a}_2 + z_6\mathbf{a}_3$	=	$ax_6\hat{\mathbf{x}} + by_6\hat{\mathbf{y}} + cz_6\hat{\mathbf{z}}$	(8g)	Pd IV
$\mathbf{B}_{18}$	$-(x_6 - \frac{1}{2})\mathbf{a}_1 - (y_6 - \frac{1}{2})\mathbf{a}_2 + z_6\mathbf{a}_3$	=	$-a(x_6 - \frac{1}{2})\hat{\mathbf{x}} - b(y_6 - \frac{1}{2})\hat{\mathbf{y}} + cz_6\hat{\mathbf{z}}$	(8g)	Pd IV
$\mathbf{B}_{19}$	$-x_6\mathbf{a}_1 + (y_6 + \frac{1}{2})\mathbf{a}_2 - z_6\mathbf{a}_3$	=	$-ax_6\hat{\mathbf{x}} + b(y_6 + \frac{1}{2})\hat{\mathbf{y}} - cz_6\hat{\mathbf{z}}$	(8g)	Pd IV
$\mathbf{B}_{20}$	$(x_6 + \frac{1}{2})\mathbf{a}_1 - y_6\mathbf{a}_2 - z_6\mathbf{a}_3$	=	$a(x_6 + \frac{1}{2})\hat{\mathbf{x}} - by_6\hat{\mathbf{y}} - cz_6\hat{\mathbf{z}}$	(8g)	Pd IV
$\mathbf{B}_{21}$	$-x_6\mathbf{a}_1 - y_6\mathbf{a}_2 - z_6\mathbf{a}_3$	=	$-ax_6\hat{\mathbf{x}} - by_6\hat{\mathbf{y}} - cz_6\hat{\mathbf{z}}$	(8g)	Pd IV
$\mathbf{B}_{22}$	$(x_6 + \frac{1}{2})\mathbf{a}_1 + (y_6 + \frac{1}{2})\mathbf{a}_2 - z_6\mathbf{a}_3$	=	$a(x_6 + \frac{1}{2})\hat{\mathbf{x}} + b(y_6 + \frac{1}{2})\hat{\mathbf{y}} - cz_6\hat{\mathbf{z}}$	(8g)	Pd IV
$\mathbf{B}_{23}$	$x_6\mathbf{a}_1 - (y_6 - \frac{1}{2})\mathbf{a}_2 + z_6\mathbf{a}_3$	=	$ax_6\hat{\mathbf{x}} - b(y_6 - \frac{1}{2})\hat{\mathbf{y}} + cz_6\hat{\mathbf{z}}$	(8g)	Pd IV
$\mathbf{B}_{24}$	$-(x_6 - \frac{1}{2})\mathbf{a}_1 + y_6\mathbf{a}_2 + z_6\mathbf{a}_3$	=	$-a(x_6 - \frac{1}{2})\hat{\mathbf{x}} + by_6\hat{\mathbf{y}} + cz_6\hat{\mathbf{z}}$	(8g)	Pd IV

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