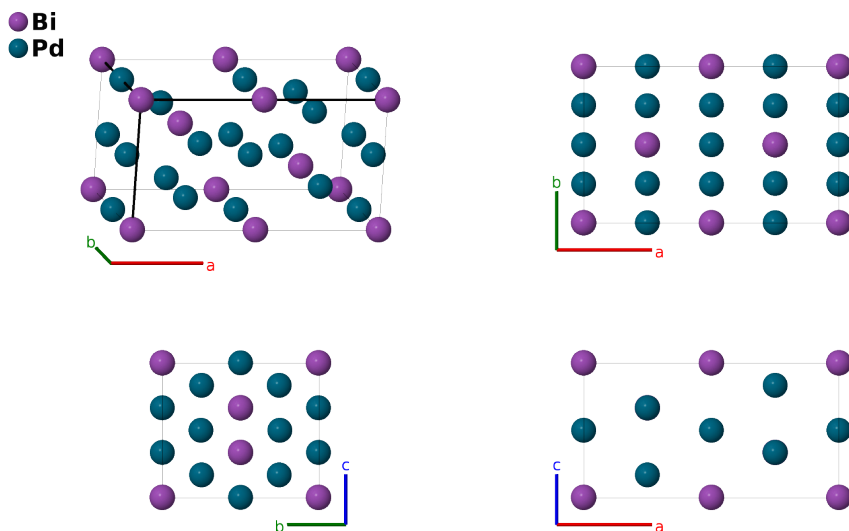


α -BiPd₃ Structure: AB3_oP16_51_af_behk-001

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<https://aflow.org/p/9W5L>

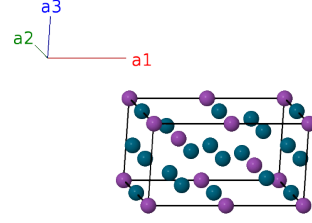
https://aflow.org/p/AB3_oP16_51_af_behk-001



Prototype	BiPd ₃
AFLOW prototype label	AB3_oP16_51_af_behk-001
ICSD	58839
Pearson symbol	oP16
Space group number	51
Space group symbol	<i>Pmma</i>
AFLOW prototype command	<code>aflow --proto=AB3_oP16_51_af_behk-001 --params=<i>a, b/a, c/a, z3, z4, y5, y6, z6</i></code>

- This is the room temperature structure of BiPd.
- Okamoto's phase diagram (Villars, 2018) shows a transition to a high-temperature phase at 800°C, but says that no data is available for that structure.
- (Schubert, 1968) puts one bismuth atom on the (2c) (0 0 1/2) Wyckoff position. We shift this so that atom is at the origin, Wyckoff position (2a).

Simple Orthorhombic primitive vectors



$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= b \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}}\end{aligned}$$

Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	0	$=$	0	(2a)	Bi I
\mathbf{B}_2	$\frac{1}{2} \mathbf{a}_1$	$=$	$\frac{1}{2} a \hat{\mathbf{x}}$	(2a)	Bi I
\mathbf{B}_3	$\frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2} b \hat{\mathbf{y}}$	(2b)	Pd I
\mathbf{B}_4	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} b \hat{\mathbf{y}}$	(2b)	Pd I
\mathbf{B}_5	$\frac{1}{4} \mathbf{a}_1 + z_3 \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{x}} + cz_3 \hat{\mathbf{z}}$	(2e)	Pd II
\mathbf{B}_6	$\frac{3}{4} \mathbf{a}_1 - z_3 \mathbf{a}_3$	$=$	$\frac{3}{4} a \hat{\mathbf{x}} - cz_3 \hat{\mathbf{z}}$	(2e)	Pd II
\mathbf{B}_7	$\frac{1}{4} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + z_4 \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{x}} + \frac{1}{2} b \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(2f)	Bi II
\mathbf{B}_8	$\frac{3}{4} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 - z_4 \mathbf{a}_3$	$=$	$\frac{3}{4} a \hat{\mathbf{x}} + \frac{1}{2} b \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}}$	(2f)	Bi II
\mathbf{B}_9	$y_5 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$by_5 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4h)	Pd III
\mathbf{B}_{10}	$\frac{1}{2} \mathbf{a}_1 - y_5 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4h)	Pd III
\mathbf{B}_{11}	$-y_5 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-by_5 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4h)	Pd III
\mathbf{B}_{12}	$\frac{1}{2} \mathbf{a}_1 + y_5 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4h)	Pd III
\mathbf{B}_{13}	$\frac{1}{4} \mathbf{a}_1 + y_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(4k)	Pd IV
\mathbf{B}_{14}	$\frac{1}{4} \mathbf{a}_1 - y_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(4k)	Pd IV
\mathbf{B}_{15}	$\frac{3}{4} \mathbf{a}_1 + y_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$\frac{3}{4} a \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(4k)	Pd IV
\mathbf{B}_{16}	$\frac{3}{4} \mathbf{a}_1 - y_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$\frac{3}{4} a \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(4k)	Pd IV

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