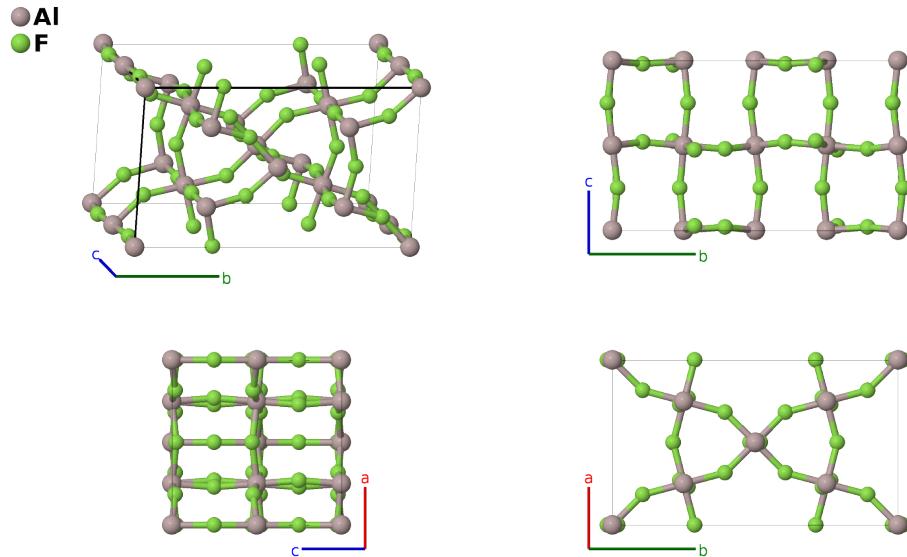


β -AlF₃ Structure: AB3_oC48_63_ad_cfgh-001

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<https://aflow.org/p/W7TS>

https://aflow.org/p/AB3_oC48_63_ad_cfgh-001



Prototype	AlF ₃
AFLOW prototype label	AB3_oC48_63_ad_cfgh-001
ICSD	202681
Pearson symbol	oC48
Space group number	63
Space group symbol	<i>Cmcm</i>
AFLOW prototype command	<code>aflow --proto=AB3_oC48_63_ad_cfgh-001 --params=a,b/a,c/a,y₂,y₄,z₄,x₅,y₅,x₆,y₆,z₆</code>

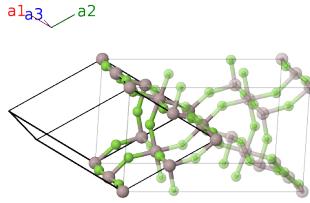
Other compounds with this structure

α' -AlH₃, β -GaF₃, β -InF₃

- AlF₃ has a variety of polymorphs (Le Bail, 2006) including:
 - α -AlF₃, which takes the rhombohedral FeF₃ (*D*0₁₂) structure.
 - β -AlF₃ is this body-centered orthorhombic structure.
 - η -AlF₃ has the β -AlH₃ structure.
 - κ -AlF₃ is a tetragonal structure.
 - θ -AlF₃, also known as τ -AlF₃, is a larger tetragonal structure.
 - Above 713K AlF₃ transforms into the cubic ReO₃ (*D*0₉) structure (Morelock, 2014).

Base-centered Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}b\hat{\mathbf{y}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}} \\ \mathbf{a}_3 &= c\hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates	Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	= 0	= 0	(4a)	Al I
\mathbf{B}_2	= $\frac{1}{2}\mathbf{a}_3$	= $\frac{1}{2}c\hat{\mathbf{z}}$	(4a)	Al I
\mathbf{B}_3	= $-y_2\mathbf{a}_1 + y_2\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$	= $by_2\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(4c)	F I
\mathbf{B}_4	= $y_2\mathbf{a}_1 - y_2\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$	= $-by_2\hat{\mathbf{y}} + \frac{3}{4}c\hat{\mathbf{z}}$	(4c)	F I
\mathbf{B}_5	= $\frac{1}{2}\mathbf{a}_2$	= $\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}b\hat{\mathbf{y}}$	(8d)	Al II
\mathbf{B}_6	= $\frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	= $\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$	(8d)	Al II
\mathbf{B}_7	= $\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_3$	= $\frac{1}{4}a\hat{\mathbf{x}} - \frac{1}{4}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$	(8d)	Al II
\mathbf{B}_8	= $\frac{1}{2}\mathbf{a}_1$	= $\frac{1}{4}a\hat{\mathbf{x}} - \frac{1}{4}b\hat{\mathbf{y}}$	(8d)	Al II
\mathbf{B}_9	= $-y_4\mathbf{a}_1 + y_4\mathbf{a}_2 + z_4\mathbf{a}_3$	= $by_4\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(8f)	F II
\mathbf{B}_{10}	= $y_4\mathbf{a}_1 - y_4\mathbf{a}_2 + (z_4 + \frac{1}{2})\mathbf{a}_3$	= $-by_4\hat{\mathbf{y}} + c(z_4 + \frac{1}{2})\hat{\mathbf{z}}$	(8f)	F II
\mathbf{B}_{11}	= $-y_4\mathbf{a}_1 + y_4\mathbf{a}_2 - (z_4 - \frac{1}{2})\mathbf{a}_3$	= $by_4\hat{\mathbf{y}} - c(z_4 - \frac{1}{2})\hat{\mathbf{z}}$	(8f)	F II
\mathbf{B}_{12}	= $y_4\mathbf{a}_1 - y_4\mathbf{a}_2 - z_4\mathbf{a}_3$	= $-by_4\hat{\mathbf{y}} - cz_4\hat{\mathbf{z}}$	(8f)	F II
\mathbf{B}_{13}	= $(x_5 - y_5)\mathbf{a}_1 + (x_5 + y_5)\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$	= $ax_5\hat{\mathbf{x}} + by_5\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(8g)	F III
\mathbf{B}_{14}	= $-(x_5 - y_5)\mathbf{a}_1 - (x_5 + y_5)\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$	= $-ax_5\hat{\mathbf{x}} - by_5\hat{\mathbf{y}} + \frac{3}{4}c\hat{\mathbf{z}}$	(8g)	F III
\mathbf{B}_{15}	= $-(x_5 + y_5)\mathbf{a}_1 - (x_5 - y_5)\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$	= $-ax_5\hat{\mathbf{x}} + by_5\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(8g)	F III
\mathbf{B}_{16}	= $(x_5 + y_5)\mathbf{a}_1 + (x_5 - y_5)\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$	= $ax_5\hat{\mathbf{x}} - by_5\hat{\mathbf{y}} + \frac{3}{4}c\hat{\mathbf{z}}$	(8g)	F III
\mathbf{B}_{17}	= $(x_6 - y_6)\mathbf{a}_1 + (x_6 + y_6)\mathbf{a}_2 + z_6\mathbf{a}_3$	= $ax_6\hat{\mathbf{x}} + by_6\hat{\mathbf{y}} + cz_6\hat{\mathbf{z}}$	(16h)	F IV
\mathbf{B}_{18}	= $-(x_6 - y_6)\mathbf{a}_1 - (x_6 + y_6)\mathbf{a}_2 + (z_6 + \frac{1}{2})\mathbf{a}_3$	= $-ax_6\hat{\mathbf{x}} - by_6\hat{\mathbf{y}} + c(z_6 + \frac{1}{2})\hat{\mathbf{z}}$	(16h)	F IV
\mathbf{B}_{19}	= $-(x_6 + y_6)\mathbf{a}_1 - (x_6 - y_6)\mathbf{a}_2 - (z_6 - \frac{1}{2})\mathbf{a}_3$	= $-ax_6\hat{\mathbf{x}} + by_6\hat{\mathbf{y}} - c(z_6 - \frac{1}{2})\hat{\mathbf{z}}$	(16h)	F IV
\mathbf{B}_{20}	= $(x_6 + y_6)\mathbf{a}_1 + (x_6 - y_6)\mathbf{a}_2 - z_6\mathbf{a}_3$	= $ax_6\hat{\mathbf{x}} - by_6\hat{\mathbf{y}} - cz_6\hat{\mathbf{z}}$	(16h)	F IV
\mathbf{B}_{21}	= $-(x_6 - y_6)\mathbf{a}_1 - (x_6 + y_6)\mathbf{a}_2 - z_6\mathbf{a}_3$	= $-ax_6\hat{\mathbf{x}} - by_6\hat{\mathbf{y}} - cz_6\hat{\mathbf{z}}$	(16h)	F IV
\mathbf{B}_{22}	= $(x_6 - y_6)\mathbf{a}_1 + (x_6 + y_6)\mathbf{a}_2 - (z_6 - \frac{1}{2})\mathbf{a}_3$	= $ax_6\hat{\mathbf{x}} + by_6\hat{\mathbf{y}} - c(z_6 - \frac{1}{2})\hat{\mathbf{z}}$	(16h)	F IV
\mathbf{B}_{23}	= $(x_6 + y_6)\mathbf{a}_1 + (x_6 - y_6)\mathbf{a}_2 + (z_6 + \frac{1}{2})\mathbf{a}_3$	= $ax_6\hat{\mathbf{x}} - by_6\hat{\mathbf{y}} + c(z_6 + \frac{1}{2})\hat{\mathbf{z}}$	(16h)	F IV

$$\mathbf{B}_{24} = -(x_6 + y_6) \mathbf{a}_1 - (x_6 - y_6) \mathbf{a}_2 + z_6 \mathbf{a}_3 = -ax_6 \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} \quad (16h) \quad \text{F IV}$$

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