

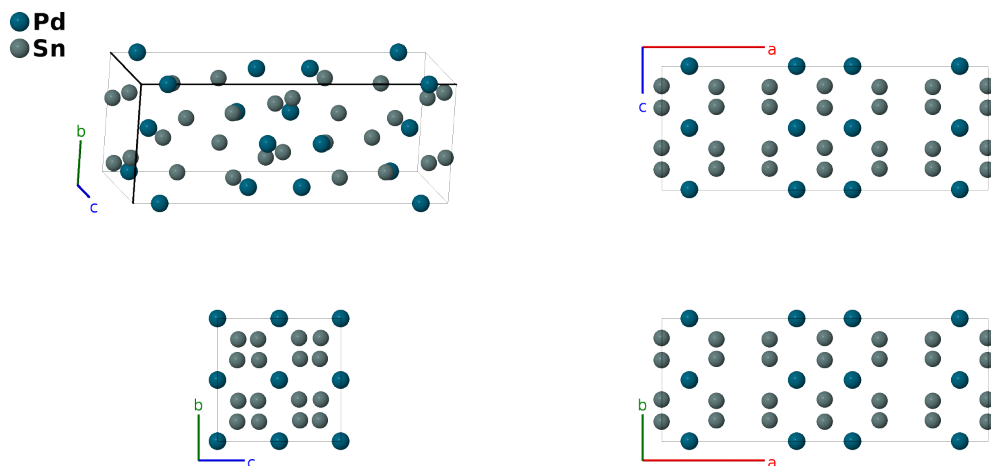
# PdSn<sub>3</sub> Structure:

## AB3\_oC32\_64\_d\_fg-001

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<https://aflow.org/p/J38S>

[https://aflow.org/p/AB3\\_oC32\\_64\\_d\\_fg-001](https://aflow.org/p/AB3_oC32_64_d_fg-001)



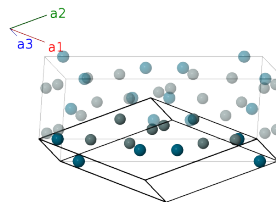
Prototype	PdSn <sub>3</sub>
AFLOW prototype label	AB3_oC32_64_d_fg-001
ICSD	413279
Pearson symbol	oC32
Space group number	64
Space group symbol	<i>Cmce</i>
AFLOW prototype command	<code>aflow --proto=AB3_oC32_64_d_fg-001</code> <code>--params=a, b/a, c/a, x<sub>1</sub>, y<sub>2</sub>, z<sub>2</sub>, x<sub>3</sub>, y<sub>3</sub>, z<sub>3</sub></code>

### Base-centered Orthorhombic primitive vectors

$$\mathbf{a}_1 = \frac{1}{2}a \hat{x} - \frac{1}{2}b \hat{y}$$

$$\mathbf{a}_2 = \frac{1}{2}a \hat{x} + \frac{1}{2}b \hat{y}$$

$$\mathbf{a}_3 = c \hat{z}$$



### Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$=$	$x_1 \mathbf{a}_1 + x_1 \mathbf{a}_2$	$=$	$ax_1 \hat{x}$	(8d) Pd I

$$\begin{aligned}
\mathbf{B}_2 &= -\left(x_1 - \frac{1}{2}\right) \mathbf{a}_1 - \left(x_1 - \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3 &= & -a \left(x_1 - \frac{1}{2}\right) \hat{\mathbf{x}} + \frac{1}{2} c \hat{\mathbf{z}} & (8d) & \text{Pd I} \\
\mathbf{B}_3 &= -x_1 \mathbf{a}_1 - x_1 \mathbf{a}_2 &= & -ax_1 \hat{\mathbf{x}} & (8d) & \text{Pd I} \\
\mathbf{B}_4 &= \left(x_1 + \frac{1}{2}\right) \mathbf{a}_1 + \left(x_1 + \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3 &= & a \left(x_1 + \frac{1}{2}\right) \hat{\mathbf{x}} + \frac{1}{2} c \hat{\mathbf{z}} & (8d) & \text{Pd I} \\
\mathbf{B}_5 &= -y_2 \mathbf{a}_1 + y_2 \mathbf{a}_2 + z_2 \mathbf{a}_3 &= & by_2 \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}} & (8f) & \text{Sn I} \\
\mathbf{B}_6 &= \left(y_2 + \frac{1}{2}\right) \mathbf{a}_1 - \left(y_2 - \frac{1}{2}\right) \mathbf{a}_2 + \left(z_2 + \frac{1}{2}\right) \mathbf{a}_3 &= & \frac{1}{2} a \hat{\mathbf{x}} - by_2 \hat{\mathbf{y}} + c \left(z_2 + \frac{1}{2}\right) \hat{\mathbf{z}} & (8f) & \text{Sn I} \\
\mathbf{B}_7 &= -\left(y_2 - \frac{1}{2}\right) \mathbf{a}_1 + \left(y_2 + \frac{1}{2}\right) \mathbf{a}_2 - \left(z_2 - \frac{1}{2}\right) \mathbf{a}_3 &= & \frac{1}{2} a \hat{\mathbf{x}} + by_2 \hat{\mathbf{y}} - c \left(z_2 - \frac{1}{2}\right) \hat{\mathbf{z}} & (8f) & \text{Sn I} \\
\mathbf{B}_8 &= y_2 \mathbf{a}_1 - y_2 \mathbf{a}_2 - z_2 \mathbf{a}_3 &= & -by_2 \hat{\mathbf{y}} - cz_2 \hat{\mathbf{z}} & (8f) & \text{Sn I} \\
\mathbf{B}_9 &= (x_3 - y_3) \mathbf{a}_1 + (x_3 + y_3) \mathbf{a}_2 + z_3 \mathbf{a}_3 &= & ax_3 \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}} & (16g) & \text{Sn II} \\
\mathbf{B}_{10} &= \left(-x_3 + y_3 + \frac{1}{2}\right) \mathbf{a}_1 - \left(x_3 + y_3 - \frac{1}{2}\right) \mathbf{a}_2 + \left(z_3 + \frac{1}{2}\right) \mathbf{a}_3 &= & -a \left(x_3 - \frac{1}{2}\right) \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} + c \left(z_3 + \frac{1}{2}\right) \hat{\mathbf{z}} & (16g) & \text{Sn II} \\
\mathbf{B}_{11} &= -\left(x_3 + y_3 - \frac{1}{2}\right) \mathbf{a}_1 + \left(-x_3 + y_3 + \frac{1}{2}\right) \mathbf{a}_2 - \left(z_3 - \frac{1}{2}\right) \mathbf{a}_3 &= & -a \left(x_3 - \frac{1}{2}\right) \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} - c \left(z_3 - \frac{1}{2}\right) \hat{\mathbf{z}} & (16g) & \text{Sn II} \\
\mathbf{B}_{12} &= (x_3 + y_3) \mathbf{a}_1 + (x_3 - y_3) \mathbf{a}_2 - z_3 \mathbf{a}_3 &= & ax_3 \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}} & (16g) & \text{Sn II} \\
\mathbf{B}_{13} &= -(x_3 - y_3) \mathbf{a}_1 - (x_3 + y_3) \mathbf{a}_2 - z_3 \mathbf{a}_3 &= & -ax_3 \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}} & (16g) & \text{Sn II} \\
\mathbf{B}_{14} &= \left(x_3 - y_3 + \frac{1}{2}\right) \mathbf{a}_1 + \left(x_3 + y_3 + \frac{1}{2}\right) \mathbf{a}_2 - \left(z_3 - \frac{1}{2}\right) \mathbf{a}_3 &= & a \left(x_3 + \frac{1}{2}\right) \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} - c \left(z_3 - \frac{1}{2}\right) \hat{\mathbf{z}} & (16g) & \text{Sn II} \\
\mathbf{B}_{15} &= \left(x_3 + y_3 + \frac{1}{2}\right) \mathbf{a}_1 + \left(x_3 - y_3 + \frac{1}{2}\right) \mathbf{a}_2 + \left(z_3 + \frac{1}{2}\right) \mathbf{a}_3 &= & a \left(x_3 + \frac{1}{2}\right) \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} + c \left(z_3 + \frac{1}{2}\right) \hat{\mathbf{z}} & (16g) & \text{Sn II} \\
\mathbf{B}_{16} &= -(x_3 + y_3) \mathbf{a}_1 - (x_3 - y_3) \mathbf{a}_2 + z_3 \mathbf{a}_3 &= & -ax_3 \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}} & (16g) & \text{Sn II}
\end{aligned}$$

## References

- [1] J. Nylén, F. J. G. Garcìa, B. D. Mosel, R. Pöttgen, and U. Häussermann, *Structural relationships, phase stability and bonding of compounds PdSn<sub>n</sub> (n=2, 3, 4)*, Solid State Sci. **6**, 147–155 (2004), doi:10.1016/j.solidstatesciences.2003.09.011.

## Found in

- [1] A. Jain, S. Ping, G. Hautier, W. Chen, W. D. Richards, S. Dacek, S. Cholia, D. Gunter, D. Skinner, G. Ceder, and K. A. Persson, *Commentary: The Materials Project: A materials genome approach to accelerating materials innovation*, APL Materials **1**, 011002 (2013), doi:10.1063/1.4812323.