

# TaTi<sub>3</sub>-I (BCC SQS-16) Structure:

AB3\_mC32\_8\_4a\_12a-001

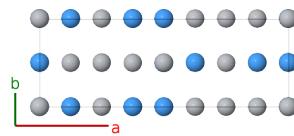
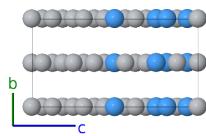
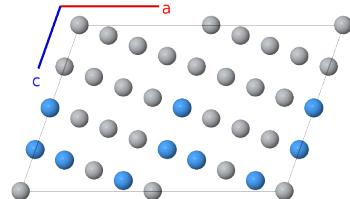
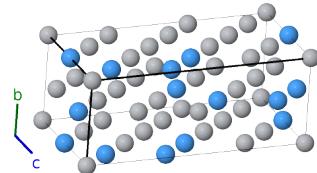
This structure originally had the label AB3\_mC32\_8\_4a\_12a. Calls to that address will be redirected here.

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<https://aflow.org/p/QVN8>

[https://aflow.org/p/AB3\\_mC32\\_8\\_4a\\_12a-001](https://aflow.org/p/AB3_mC32_8_4a_12a-001)

● Ta  
● Ti



**Prototype** TaTi<sub>3</sub>

**AFLOW prototype label** AB3\_mC32\_8\_4a\_12a-001

**ICSD** none

**Pearson symbol** mC32

**Space group number** 8

**Space group symbol** Cm

**AFLOW prototype command**

```
aflow --proto=AB3_mC32_8_4a_12a-001
--params=a,b/a,c/a,\beta,x_1,z_1,x_2,z_2,x_3,z_3,x_4,z_4,x_5,z_5,x_6,z_6,x_7,z_7,x_8,z_8,x_9,z_9,x_10,
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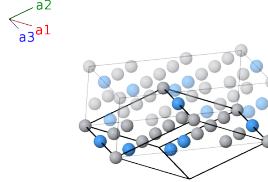
- This is a special quasirandom structure with 16 atoms per unit cell (SQS-16) for a bcc binary substitutional alloy A<sub>x</sub>B<sub>1-x</sub> (Jiang, 2004; Chakraborty, 2016)).
- Several compositions are available:
  - TaTi<sub>7</sub> (AB7\_hR16\_166\_c\_c2h),
  - Ta<sub>3</sub>Ti<sub>13</sub> (A3B13\_oC32\_38\_ac\_a2bcdef),
  - TaTi<sub>3</sub>-I (AB3\_mC32\_8\_4a\_12a) (this structure),
  - TaTi<sub>3</sub>-II (AB3\_mC32\_8\_4a\_4a4b) ,

- Ta<sub>5</sub>Ti<sub>11</sub> (A5B11\_mP16\_6\_2abc\_2a3b3c) ,
- Ta<sub>3</sub>Ti<sub>8</sub> (A3B5\_oC32\_38\_abce\_abcdf) ,
- TaTi (AB\_aP16\_2\_4i\_4i).

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### Base-centered Monoclinic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}b\hat{\mathbf{y}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \cos \beta \hat{\mathbf{x}} + c \sin \beta \hat{\mathbf{z}}\end{aligned}$$




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### Basis vectors

	Lattice coordinates	=	Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$x_1 \mathbf{a}_1 + x_1 \mathbf{a}_2 + z_1 \mathbf{a}_3$	=	$(ax_1 + cz_1 \cos \beta) \hat{\mathbf{x}} + cz_1 \sin \beta \hat{\mathbf{z}}$	(2a)	Ta I
$\mathbf{B}_2$	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + z_2 \mathbf{a}_3$	=	$(ax_2 + cz_2 \cos \beta) \hat{\mathbf{x}} + cz_2 \sin \beta \hat{\mathbf{z}}$	(2a)	Ta II
$\mathbf{B}_3$	$x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + z_3 \mathbf{a}_3$	=	$(ax_3 + cz_3 \cos \beta) \hat{\mathbf{x}} + cz_3 \sin \beta \hat{\mathbf{z}}$	(2a)	Ta III
$\mathbf{B}_4$	$x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + z_4 \mathbf{a}_3$	=	$(ax_4 + cz_4 \cos \beta) \hat{\mathbf{x}} + cz_4 \sin \beta \hat{\mathbf{z}}$	(2a)	Ta IV
$\mathbf{B}_5$	$x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	=	$(ax_5 + cz_5 \cos \beta) \hat{\mathbf{x}} + cz_5 \sin \beta \hat{\mathbf{z}}$	(2a)	Ti I
$\mathbf{B}_6$	$x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	=	$(ax_6 + cz_6 \cos \beta) \hat{\mathbf{x}} + cz_6 \sin \beta \hat{\mathbf{z}}$	(2a)	Ti II
$\mathbf{B}_7$	$x_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	=	$(ax_7 + cz_7 \cos \beta) \hat{\mathbf{x}} + cz_7 \sin \beta \hat{\mathbf{z}}$	(2a)	Ti III
$\mathbf{B}_8$	$x_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 + z_8 \mathbf{a}_3$	=	$(ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} + cz_8 \sin \beta \hat{\mathbf{z}}$	(2a)	Ti IV
$\mathbf{B}_9$	$x_9 \mathbf{a}_1 + x_9 \mathbf{a}_2 + z_9 \mathbf{a}_3$	=	$(ax_9 + cz_9 \cos \beta) \hat{\mathbf{x}} + cz_9 \sin \beta \hat{\mathbf{z}}$	(2a)	Ti V
$\mathbf{B}_{10}$	$x_{10} \mathbf{a}_1 + x_{10} \mathbf{a}_2 + z_{10} \mathbf{a}_3$	=	$(ax_{10} + cz_{10} \cos \beta) \hat{\mathbf{x}} + cz_{10} \sin \beta \hat{\mathbf{z}}$	(2a)	Ti VI
$\mathbf{B}_{11}$	$x_{11} \mathbf{a}_1 + x_{11} \mathbf{a}_2 + z_{11} \mathbf{a}_3$	=	$(ax_{11} + cz_{11} \cos \beta) \hat{\mathbf{x}} + cz_{11} \sin \beta \hat{\mathbf{z}}$	(2a)	Ti VII
$\mathbf{B}_{12}$	$x_{12} \mathbf{a}_1 + x_{12} \mathbf{a}_2 + z_{12} \mathbf{a}_3$	=	$(ax_{12} + cz_{12} \cos \beta) \hat{\mathbf{x}} + cz_{12} \sin \beta \hat{\mathbf{z}}$	(2a)	Ti VIII
$\mathbf{B}_{13}$	$x_{13} \mathbf{a}_1 + x_{13} \mathbf{a}_2 + z_{13} \mathbf{a}_3$	=	$(ax_{13} + cz_{13} \cos \beta) \hat{\mathbf{x}} + cz_{13} \sin \beta \hat{\mathbf{z}}$	(2a)	Ti IX
$\mathbf{B}_{14}$	$x_{14} \mathbf{a}_1 + x_{14} \mathbf{a}_2 + z_{14} \mathbf{a}_3$	=	$(ax_{14} + cz_{14} \cos \beta) \hat{\mathbf{x}} + cz_{14} \sin \beta \hat{\mathbf{z}}$	(2a)	Ti X
$\mathbf{B}_{15}$	$x_{15} \mathbf{a}_1 + x_{15} \mathbf{a}_2 + z_{15} \mathbf{a}_3$	=	$(ax_{15} + cz_{15} \cos \beta) \hat{\mathbf{x}} + cz_{15} \sin \beta \hat{\mathbf{z}}$	(2a)	Ti XI
$\mathbf{B}_{16}$	$x_{16} \mathbf{a}_1 + x_{16} \mathbf{a}_2 + z_{16} \mathbf{a}_3$	=	$(ax_{16} + cz_{16} \cos \beta) \hat{\mathbf{x}} + cz_{16} \sin \beta \hat{\mathbf{z}}$	(2a)	Ti XII

### References

- [1] C. Jiang, C. Wolverton, J. Sofo, L.-Q. Chen, and Z.-K. Liu, *First-principles study of binary bcc alloys using special quasirandom structures*, Phys. Rev. B **69**, 214202 (2004), doi:10.1103/PhysRevB.69.214202.
- [2] T. Chakraborty, J. Rogal, and R. Drautz, *Unraveling the composition dependence of the martensitic transformation temperature: A first-principles study of Ti-Ta alloys*, Phys. Rev. B **94**, 224104 (2016), doi:10.1103/PhysRevB.94.224104.