

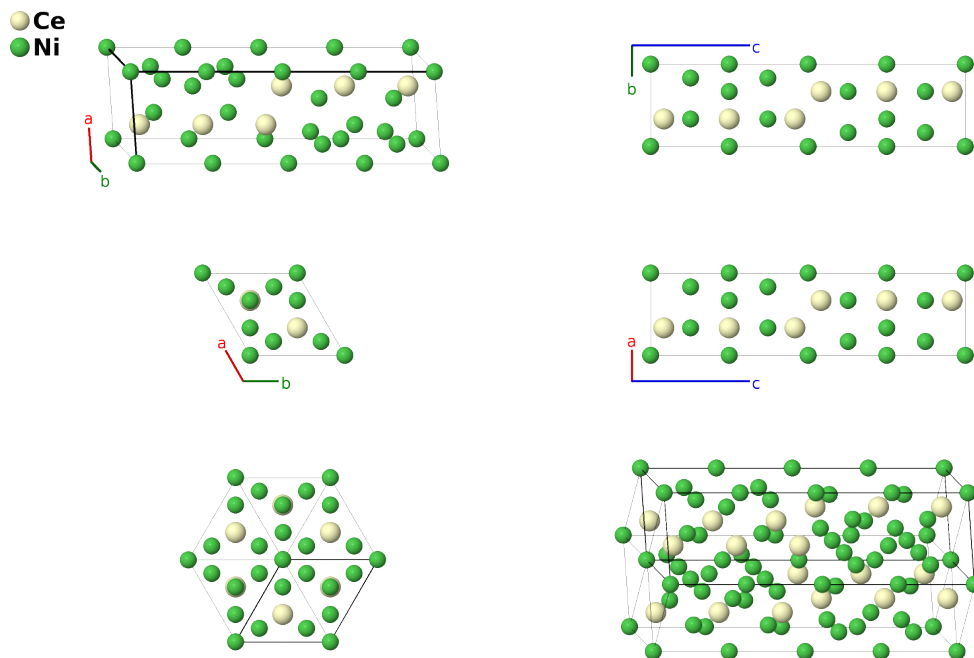
CeNi₃ Structure:

AB3_hP24_194_cf_abdk-001

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<https://afLOW.org/p/1SSV>

https://afLOW.org/p/AB3_hP24_194_cf_abdk-001



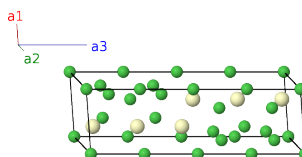
Prototype	CeNi ₃
AFLOW prototype label	AB3_hP24_194_cf_abdk-001
ICSD	102230
Pearson symbol	hP24
Space group number	194
Space group symbol	<i>P</i> 6 ₃ / <i>mmc</i>
AFLOW prototype command	afLOW --proto=AB3_hP24_194_cf_abdk-001 --params= <i>a</i> , <i>c/a</i> , <i>z</i> ₅ , <i>x</i> ₆ , <i>z</i> ₆

Other compounds with this structure

DyFe₃, GdNi₃, GdRh₃, LaRh₃, LuNi₃, NdNi₃, NdRh₃, SmCo₃, SmRh₃, TbFe₃, YCo₃, YFe₃, YRh₃

Hexagonal primitive vectors

$$\begin{aligned} \mathbf{a}_1 &= \frac{1}{2}a \hat{x} - \frac{\sqrt{3}}{2}a \hat{y} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{x} + \frac{\sqrt{3}}{2}a \hat{y} \\ \mathbf{a}_3 &= c \hat{z} \end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$=$	0	$=$	0	(2a) Ni I
\mathbf{B}_2	$=$	$\frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} c \hat{\mathbf{z}}$	(2a) Ni I
\mathbf{B}_3	$=$	$\frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{4} c \hat{\mathbf{z}}$	(2b) Ni II
\mathbf{B}_4	$=$	$\frac{3}{4} \mathbf{a}_3$	$=$	$\frac{3}{4} c \hat{\mathbf{z}}$	(2b) Ni II
\mathbf{B}_5	$=$	$\frac{1}{3} \mathbf{a}_1 + \frac{2}{3} \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}}$	(2c) Ce I
\mathbf{B}_6	$=$	$\frac{2}{3} \mathbf{a}_1 + \frac{1}{3} \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} + \frac{3}{4} c \hat{\mathbf{z}}$	(2c) Ce I
\mathbf{B}_7	$=$	$\frac{1}{3} \mathbf{a}_1 + \frac{2}{3} \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} + \frac{3}{4} c \hat{\mathbf{z}}$	(2d) Ni III
\mathbf{B}_8	$=$	$\frac{2}{3} \mathbf{a}_1 + \frac{1}{3} \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}}$	(2d) Ni III
\mathbf{B}_9	$=$	$\frac{1}{3} \mathbf{a}_1 + \frac{2}{3} \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(4f) Ce II
\mathbf{B}_{10}	$=$	$\frac{2}{3} \mathbf{a}_1 + \frac{1}{3} \mathbf{a}_2 + (z_5 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} + c(z_5 + \frac{1}{2}) \hat{\mathbf{z}}$	(4f) Ce II
\mathbf{B}_{11}	$=$	$\frac{2}{3} \mathbf{a}_1 + \frac{1}{3} \mathbf{a}_2 - z_5 \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}}$	(4f) Ce II
\mathbf{B}_{12}	$=$	$\frac{1}{3} \mathbf{a}_1 + \frac{2}{3} \mathbf{a}_2 - (z_5 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} - c(z_5 - \frac{1}{2}) \hat{\mathbf{z}}$	(4f) Ce II
\mathbf{B}_{13}	$=$	$x_6 \mathbf{a}_1 + 2x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$\frac{3}{2} ax_6 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2} ax_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(12k) Ni IV
\mathbf{B}_{14}	$=$	$-2x_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$-\frac{3}{2} ax_6 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2} ax_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(12k) Ni IV
\mathbf{B}_{15}	$=$	$x_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$-\sqrt{3} ax_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(12k) Ni IV
\mathbf{B}_{16}	$=$	$-x_6 \mathbf{a}_1 - 2x_6 \mathbf{a}_2 + (z_6 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-\frac{3}{2} ax_6 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2} ax_6 \hat{\mathbf{y}} + c(z_6 + \frac{1}{2}) \hat{\mathbf{z}}$	(12k) Ni IV
\mathbf{B}_{17}	$=$	$2x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 + (z_6 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{3}{2} ax_6 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2} ax_6 \hat{\mathbf{y}} + c(z_6 + \frac{1}{2}) \hat{\mathbf{z}}$	(12k) Ni IV
\mathbf{B}_{18}	$=$	$-x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 + (z_6 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\sqrt{3} ax_6 \hat{\mathbf{y}} + c(z_6 + \frac{1}{2}) \hat{\mathbf{z}}$	(12k) Ni IV
\mathbf{B}_{19}	$=$	$2x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$\frac{3}{2} ax_6 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2} ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(12k) Ni IV
\mathbf{B}_{20}	$=$	$-x_6 \mathbf{a}_1 - 2x_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$-\frac{3}{2} ax_6 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2} ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(12k) Ni IV
\mathbf{B}_{21}	$=$	$-x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$\sqrt{3} ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(12k) Ni IV
\mathbf{B}_{22}	$=$	$-2x_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 - (z_6 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-\frac{3}{2} ax_6 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2} ax_6 \hat{\mathbf{y}} - c(z_6 - \frac{1}{2}) \hat{\mathbf{z}}$	(12k) Ni IV
\mathbf{B}_{23}	$=$	$x_6 \mathbf{a}_1 + 2x_6 \mathbf{a}_2 - (z_6 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{3}{2} ax_6 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2} ax_6 \hat{\mathbf{y}} - c(z_6 - \frac{1}{2}) \hat{\mathbf{z}}$	(12k) Ni IV
\mathbf{B}_{24}	$=$	$x_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 - (z_6 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-\sqrt{3} ax_6 \hat{\mathbf{y}} - c(z_6 - \frac{1}{2}) \hat{\mathbf{z}}$	(12k) Ni IV

References

- [1] D. T. Cromer and C. E. Olsen, *The crystal structure of PuNi₃ and CeNi₃*, *Acta Cryst.* **12**, 689–694 (1959), doi:10.1107/S0365110X59002006.