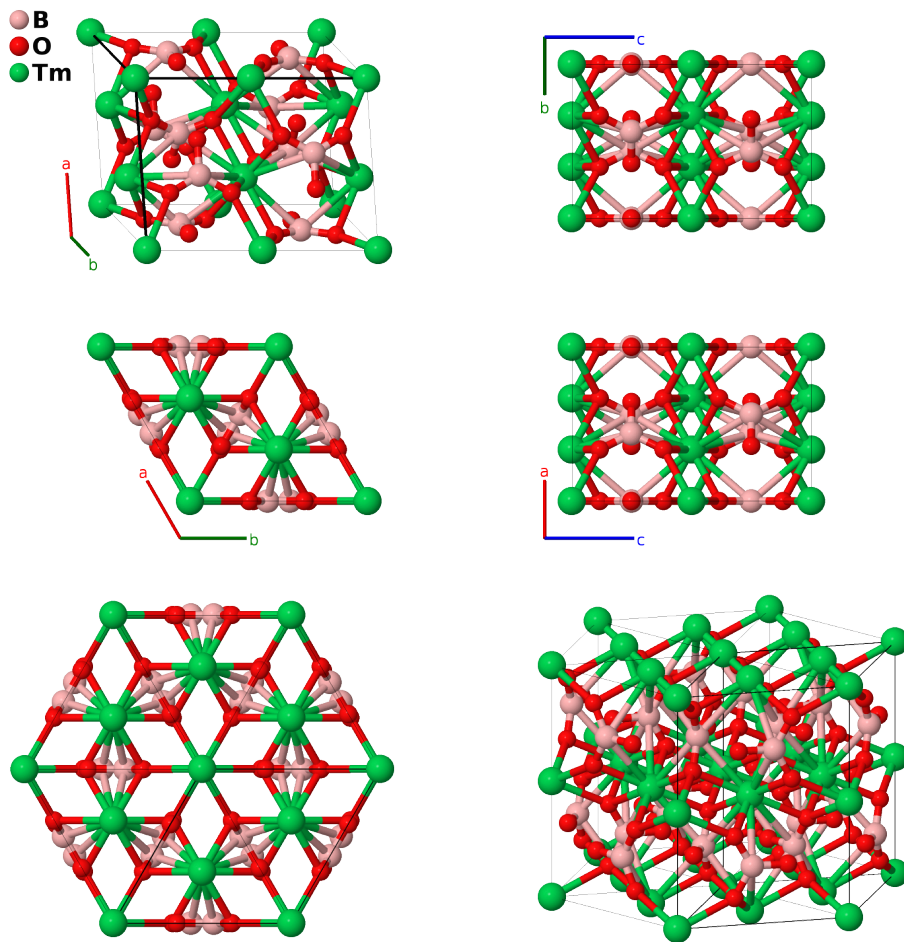


Ordered TmBO_3 Structure: AB3C_hP30_193_g_gk_bd-001

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<https://aflow.org/p/AE3Q>

https://aflow.org/p/AB3C_hP30_193_g_gk_bd-001



Prototype	BO_3Tm
AFLOW prototype label	AB3C_hP30_193_g_gk_bd-001
ICSD	27942
Pearson symbol	hP30
Space group number	193
Space group symbol	$P6_3/mcm$
AFLOW prototype command	<code>aflow --proto=AB3C_hP30_193_g_gk_bd-001 --params=a, c/a, x3, x4, x5, z5</code>

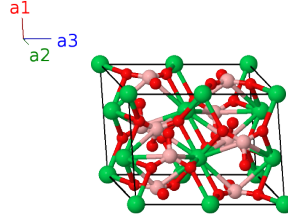
Other compounds with this structure

DyBO₃, ErBO₃, EuBO₃, GdBO₃, HoBO₃, LuBO₃, SmBO₃, YBO₃, YbBO₃

- (Newnham, 1963) found two possible structures for TmBO₃ and YBO₃:
 - A compact hexagonal cell with partially disordered boron and oxygen atoms, and
 - this structure, which has a larger hexagonal cell but completely ordered atoms.
- There are several problems with this structure:
 - The ICSD entry 27942 places this structure in space group $P\bar{6}c2$ #188 even though the positions are such that the structure can be resolved in the higher symmetry $P6_3/mcm$ space group, and
 - the positions of the O I atoms are such that the O-O distance is less than 1Å.
 - The ICSD entry gives what seem to be reasonable O-O distances, so we use those coordinates, using AFLOW to transform the structure into space group $P6_3/mcm$.

Hexagonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{x} - \frac{\sqrt{3}}{2}a\hat{y} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{x} + \frac{\sqrt{3}}{2}a\hat{y} \\ \mathbf{a}_3 &= c\hat{z}\end{aligned}$$



Basis vectors

	Lattice coordinates	=	Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	= 0	=	0	(2b)	Tm I
\mathbf{B}_2	= $\frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{2}c\hat{z}$	(2b)	Tm I
\mathbf{B}_3	= $\frac{1}{3}\mathbf{a}_1 + \frac{2}{3}\mathbf{a}_2$	=	$\frac{1}{2}a\hat{x} + \frac{\sqrt{3}}{6}a\hat{y}$	(4d)	Tm II
\mathbf{B}_4	= $\frac{2}{3}\mathbf{a}_1 + \frac{1}{3}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{2}a\hat{x} - \frac{\sqrt{3}}{6}a\hat{y} + \frac{1}{2}c\hat{z}$	(4d)	Tm II
\mathbf{B}_5	= $\frac{2}{3}\mathbf{a}_1 + \frac{1}{3}\mathbf{a}_2$	=	$\frac{1}{2}a\hat{x} - \frac{\sqrt{3}}{6}a\hat{y}$	(4d)	Tm II
\mathbf{B}_6	= $\frac{1}{3}\mathbf{a}_1 + \frac{2}{3}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{2}a\hat{x} + \frac{\sqrt{3}}{6}a\hat{y} + \frac{1}{2}c\hat{z}$	(4d)	Tm II
\mathbf{B}_7	= $x_3\mathbf{a}_1 + \frac{1}{4}\mathbf{a}_3$	=	$\frac{1}{2}ax_3\hat{x} - \frac{\sqrt{3}}{2}ax_3\hat{y} + \frac{1}{4}c\hat{z}$	(6g)	B I
\mathbf{B}_8	= $x_3\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$	=	$\frac{1}{2}ax_3\hat{x} + \frac{\sqrt{3}}{2}ax_3\hat{y} + \frac{1}{4}c\hat{z}$	(6g)	B I
\mathbf{B}_9	= $-x_3\mathbf{a}_1 - x_3\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$	=	$-ax_3\hat{x} + \frac{1}{4}c\hat{z}$	(6g)	B I
\mathbf{B}_{10}	= $-x_3\mathbf{a}_1 + \frac{3}{4}\mathbf{a}_3$	=	$-\frac{1}{2}ax_3\hat{x} + \frac{\sqrt{3}}{2}ax_3\hat{y} + \frac{3}{4}c\hat{z}$	(6g)	B I
\mathbf{B}_{11}	= $-x_3\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$	=	$-\frac{1}{2}ax_3\hat{x} - \frac{\sqrt{3}}{2}ax_3\hat{y} + \frac{3}{4}c\hat{z}$	(6g)	B I
\mathbf{B}_{12}	= $x_3\mathbf{a}_1 + x_3\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$	=	$ax_3\hat{x} + \frac{3}{4}c\hat{z}$	(6g)	B I
\mathbf{B}_{13}	= $x_4\mathbf{a}_1 + \frac{1}{4}\mathbf{a}_3$	=	$\frac{1}{2}ax_4\hat{x} - \frac{\sqrt{3}}{2}ax_4\hat{y} + \frac{1}{4}c\hat{z}$	(6g)	O I
\mathbf{B}_{14}	= $x_4\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$	=	$\frac{1}{2}ax_4\hat{x} + \frac{\sqrt{3}}{2}ax_4\hat{y} + \frac{1}{4}c\hat{z}$	(6g)	O I
\mathbf{B}_{15}	= $-x_4\mathbf{a}_1 - x_4\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$	=	$-ax_4\hat{x} + \frac{1}{4}c\hat{z}$	(6g)	O I
\mathbf{B}_{16}	= $-x_4\mathbf{a}_1 + \frac{3}{4}\mathbf{a}_3$	=	$-\frac{1}{2}ax_4\hat{x} + \frac{\sqrt{3}}{2}ax_4\hat{y} + \frac{3}{4}c\hat{z}$	(6g)	O I

$$\begin{aligned}
\mathbf{B}_{17} &= -x_4 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3 &= -\frac{1}{2}ax_4 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_4 \hat{\mathbf{y}} + \frac{3}{4}c \hat{\mathbf{z}} &(6g) & \text{O I} \\
\mathbf{B}_{18} &= x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3 &= ax_4 \hat{\mathbf{x}} + \frac{3}{4}c \hat{\mathbf{z}} &(6g) & \text{O I} \\
\mathbf{B}_{19} &= x_5 \mathbf{a}_1 + z_5 \mathbf{a}_3 &= \frac{1}{2}ax_5 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}} &(12k) & \text{O II} \\
\mathbf{B}_{20} &= x_5 \mathbf{a}_2 + z_5 \mathbf{a}_3 &= \frac{1}{2}ax_5 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}} &(12k) & \text{O II} \\
\mathbf{B}_{21} &= -x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + z_5 \mathbf{a}_3 &= -ax_5 \hat{\mathbf{x}} + cz_5 \hat{\mathbf{z}} &(12k) & \text{O II} \\
\mathbf{B}_{22} &= -x_5 \mathbf{a}_1 + \left(z_5 + \frac{1}{2}\right) \mathbf{a}_3 &= -\frac{1}{2}ax_5 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_5 \hat{\mathbf{y}} + c\left(z_5 + \frac{1}{2}\right) \hat{\mathbf{z}} &(12k) & \text{O II} \\
\mathbf{B}_{23} &= -x_5 \mathbf{a}_2 + \left(z_5 + \frac{1}{2}\right) \mathbf{a}_3 &= -\frac{1}{2}ax_5 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_5 \hat{\mathbf{y}} + c\left(z_5 + \frac{1}{2}\right) \hat{\mathbf{z}} &(12k) & \text{O II} \\
\mathbf{B}_{24} &= x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + \left(z_5 + \frac{1}{2}\right) \mathbf{a}_3 &= ax_5 \hat{\mathbf{x}} + c\left(z_5 + \frac{1}{2}\right) \hat{\mathbf{z}} &(12k) & \text{O II} \\
\mathbf{B}_{25} &= x_5 \mathbf{a}_2 - \left(z_5 - \frac{1}{2}\right) \mathbf{a}_3 &= \frac{1}{2}ax_5 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_5 \hat{\mathbf{y}} - c\left(z_5 - \frac{1}{2}\right) \hat{\mathbf{z}} &(12k) & \text{O II} \\
\mathbf{B}_{26} &= x_5 \mathbf{a}_1 - \left(z_5 - \frac{1}{2}\right) \mathbf{a}_3 &= \frac{1}{2}ax_5 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_5 \hat{\mathbf{y}} - c\left(z_5 - \frac{1}{2}\right) \hat{\mathbf{z}} &(12k) & \text{O II} \\
\mathbf{B}_{27} &= -x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - \left(z_5 - \frac{1}{2}\right) \mathbf{a}_3 &= -ax_5 \hat{\mathbf{x}} - c\left(z_5 - \frac{1}{2}\right) \hat{\mathbf{z}} &(12k) & \text{O II} \\
\mathbf{B}_{28} &= -x_5 \mathbf{a}_2 - z_5 \mathbf{a}_3 &= -\frac{1}{2}ax_5 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}} &(12k) & \text{O II} \\
\mathbf{B}_{29} &= -x_5 \mathbf{a}_1 - z_5 \mathbf{a}_3 &= -\frac{1}{2}ax_5 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}} &(12k) & \text{O II} \\
\mathbf{B}_{30} &= x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 - z_5 \mathbf{a}_3 &= ax_5 \hat{\mathbf{x}} - cz_5 \hat{\mathbf{z}} &(12k) & \text{O II}
\end{aligned}$$

References

- [1] R. E. Newnham, M. J. Redman, and R. P. Santoro, *Crystal Structure of Yttrium and Other Rare-Earth Borates*, J. Am. Ceram. Soc. **46**, 253–256 (1963), doi:10.1111/j.1151-2916.1963.tb11721.x.