

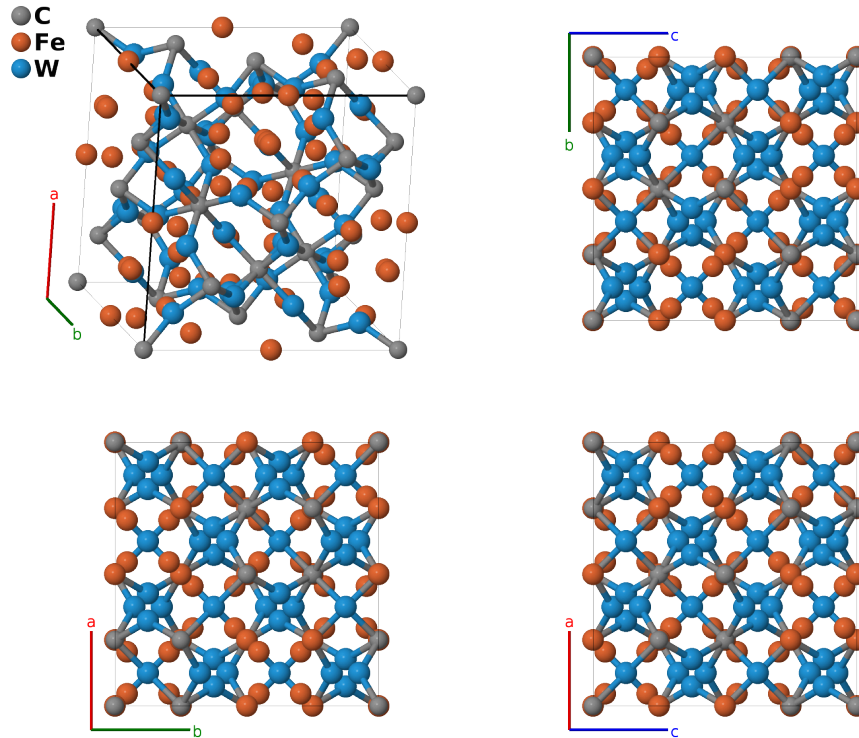
# $\eta$ -carbide ( $\text{Fe}_3\text{W}_3\text{C}$ , $E9_3$ ) Structure: AB3C3\_cF112\_227\_c\_de\_f-001

This structure originally had the label AB3C3\_cF112\_227\_c\_de\_f. Calls to that address will be redirected here.

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<https://aflow.org/p/WVM5>

[https://aflow.org/p/AB3C3\\_cF112\\_227\\_c\\_de\\_f-001](https://aflow.org/p/AB3C3_cF112_227_c_de_f-001)



Prototype	$\text{CFe}_3\text{W}_3$
AFLOW prototype label	AB3C3_cF112_227_c_de_f-001
<i>Strukturbericht</i> designation	$E9_3$
Mineral name	$\eta$ -carbide
ICSD	43230
Pearson symbol	cF112
Space group number	227
Space group symbol	$Fd\bar{3}m$
AFLOW prototype command	<code>aflow --proto=AB3C3_cF112_227_c_de_f-001 --params=a, x3, x4</code>

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### Other compounds with this structure

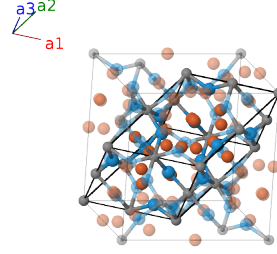
Cr<sub>3</sub>Nb<sub>3</sub>C, Fe<sub>3</sub>Mo<sub>3</sub>C, Fe<sub>4</sub>Mo<sub>2</sub>C, Fe<sub>6</sub>W<sub>6</sub>C, Hf<sub>5</sub>Zn<sub>3</sub>C, Mn<sub>3</sub>Mo<sub>3</sub>C, Mn<sub>3</sub>Ni<sub>3</sub>Si, Mn<sub>3</sub>Ti<sub>3</sub>O, Mn<sub>3</sub>W<sub>3</sub>C, Mo<sub>3</sub>Ni<sub>3</sub>C, Mo<sub>4</sub>Co<sub>2</sub>C, Mo<sub>4</sub>Co<sub>2</sub>C, Mo<sub>4</sub>Ni<sub>2</sub>C, Nb<sub>2</sub>ZnC<sub>x</sub>, Nb<sub>2</sub>ZnC<sub>x</sub>, Nb<sub>4</sub>Rh<sub>2</sub>C<sub>x</sub>, Ni<sub>3</sub>W<sub>3</sub>C, Ni<sub>5</sub>W<sub>6</sub>C, Ti<sub>2</sub>ZnC<sub>x</sub>, Ti<sub>2</sub>ZnC<sub>x</sub>, Ti<sub>4</sub>Pt<sub>2</sub>O, Ti<sub>4</sub>Rh<sub>2</sub>O, V<sub>3</sub>Zr<sub>3</sub>C, W<sub>3</sub>Co<sub>3</sub>C, W<sub>4</sub>Co<sub>2</sub>C, Zn<sub>2</sub>ZnN<sub>x</sub>, Zr<sub>2</sub>ZnC<sub>x</sub>, Zr<sub>4</sub>Pt<sub>2</sub>O

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- Experimentally, the (48f) site is a random mixture of composition W<sub>2/3</sub>Fe<sub>1/3</sub>. We use W for this site in the pictures above.
  - In many compounds the carbon sites has vacancies, which accounts for the varying stoichiometries in the compounds list.
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### Face-centered Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{y} + \frac{1}{2}a\hat{z} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{x} + \frac{1}{2}a\hat{z} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{x} + \frac{1}{2}a\hat{y}\end{aligned}$$




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### Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	=	0	=	0	(16c) C I
$\mathbf{B}_2$	=	$\frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{4}a\hat{x} + \frac{1}{4}a\hat{y}$	(16c) C I
$\mathbf{B}_3$	=	$\frac{1}{2}\mathbf{a}_2$	=	$\frac{1}{4}a\hat{x} + \frac{1}{4}a\hat{z}$	(16c) C I
$\mathbf{B}_4$	=	$\frac{1}{2}\mathbf{a}_1$	=	$\frac{1}{4}a\hat{y} + \frac{1}{4}a\hat{z}$	(16c) C I
$\mathbf{B}_5$	=	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{2}a\hat{x} + \frac{1}{2}a\hat{y} + \frac{1}{2}a\hat{z}$	(16d) Fe I
$\mathbf{B}_6$	=	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2$	=	$\frac{1}{4}a\hat{x} + \frac{1}{4}a\hat{y} + \frac{1}{2}a\hat{z}$	(16d) Fe I
$\mathbf{B}_7$	=	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{4}a\hat{x} + \frac{1}{2}a\hat{y} + \frac{1}{4}a\hat{z}$	(16d) Fe I
$\mathbf{B}_8$	=	$\frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{2}a\hat{x} + \frac{1}{4}a\hat{y} + \frac{1}{4}a\hat{z}$	(16d) Fe I
$\mathbf{B}_9$	=	$x_3\mathbf{a}_1 + x_3\mathbf{a}_2 + x_3\mathbf{a}_3$	=	$ax_3\hat{x} + ax_3\hat{y} + ax_3\hat{z}$	(32e) Fe II
$\mathbf{B}_{10}$	=	$x_3\mathbf{a}_1 + x_3\mathbf{a}_2 - (3x_3 - \frac{1}{2})\mathbf{a}_3$	=	$-a(x_3 - \frac{1}{4})\hat{x} - a(x_3 - \frac{1}{4})\hat{y} + ax_3\hat{z}$	(32e) Fe II
$\mathbf{B}_{11}$	=	$x_3\mathbf{a}_1 - (3x_3 - \frac{1}{2})\mathbf{a}_2 + x_3\mathbf{a}_3$	=	$-a(x_3 - \frac{1}{4})\hat{x} + ax_3\hat{y} - a(x_3 - \frac{1}{4})\hat{z}$	(32e) Fe II
$\mathbf{B}_{12}$	=	$-(3x_3 - \frac{1}{2})\mathbf{a}_1 + x_3\mathbf{a}_2 + x_3\mathbf{a}_3$	=	$ax_3\hat{x} - a(x_3 - \frac{1}{4})\hat{y} - a(x_3 - \frac{1}{4})\hat{z}$	(32e) Fe II
$\mathbf{B}_{13}$	=	$-x_3\mathbf{a}_1 - x_3\mathbf{a}_2 + (3x_3 + \frac{1}{2})\mathbf{a}_3$	=	$a(x_3 + \frac{1}{4})\hat{x} + a(x_3 + \frac{1}{4})\hat{y} - ax_3\hat{z}$	(32e) Fe II
$\mathbf{B}_{14}$	=	$-x_3\mathbf{a}_1 - x_3\mathbf{a}_2 - x_3\mathbf{a}_3$	=	$-ax_3\hat{x} - ax_3\hat{y} - ax_3\hat{z}$	(32e) Fe II
$\mathbf{B}_{15}$	=	$-x_3\mathbf{a}_1 + (3x_3 + \frac{1}{2})\mathbf{a}_2 - x_3\mathbf{a}_3$	=	$a(x_3 + \frac{1}{4})\hat{x} - ax_3\hat{y} + a(x_3 + \frac{1}{4})\hat{z}$	(32e) Fe II
$\mathbf{B}_{16}$	=	$(3x_3 + \frac{1}{2})\mathbf{a}_1 - x_3\mathbf{a}_2 - x_3\mathbf{a}_3$	=	$-ax_3\hat{x} + a(x_3 + \frac{1}{4})\hat{y} + a(x_3 + \frac{1}{4})\hat{z}$	(32e) Fe II
$\mathbf{B}_{17}$	=	$-(x_4 - \frac{1}{4})\mathbf{a}_1 + x_4\mathbf{a}_2 + x_4\mathbf{a}_3$	=	$ax_4\hat{x} + \frac{1}{8}a\hat{y} + \frac{1}{8}a\hat{z}$	(48f) W I
$\mathbf{B}_{18}$	=	$x_4\mathbf{a}_1 - (x_4 - \frac{1}{4})\mathbf{a}_2 - (x_4 - \frac{1}{4})\mathbf{a}_3$	=	$-a(x_4 - \frac{1}{4})\hat{x} + \frac{1}{8}a\hat{y} + \frac{1}{8}a\hat{z}$	(48f) W I
$\mathbf{B}_{19}$	=	$x_4\mathbf{a}_1 - (x_4 - \frac{1}{4})\mathbf{a}_2 + x_4\mathbf{a}_3$	=	$\frac{1}{8}a\hat{x} + ax_4\hat{y} + \frac{1}{8}a\hat{z}$	(48f) W I
$\mathbf{B}_{20}$	=	$-(x_4 - \frac{1}{4})\mathbf{a}_1 + x_4\mathbf{a}_2 - (x_4 - \frac{1}{4})\mathbf{a}_3$	=	$\frac{1}{8}a\hat{x} - a(x_4 - \frac{1}{4})\hat{y} + \frac{1}{8}a\hat{z}$	(48f) W I

$$\begin{aligned}
\mathbf{B}_{21} &= x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 - \left(x_4 - \frac{1}{4}\right) \mathbf{a}_3 &= & \frac{1}{8}a \hat{\mathbf{x}} + \frac{1}{8}a \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}} & (48f) & \text{W I} \\
\mathbf{B}_{22} &= -\left(x_4 - \frac{1}{4}\right) \mathbf{a}_1 - \left(x_4 - \frac{1}{4}\right) \mathbf{a}_2 + &= & \frac{1}{8}a \hat{\mathbf{x}} + \frac{1}{8}a \hat{\mathbf{y}} - a\left(x_4 - \frac{1}{4}\right) \hat{\mathbf{z}} & (48f) & \text{W I} \\
&& x_4 \mathbf{a}_3 & & & \\
\mathbf{B}_{23} &= \left(x_4 + \frac{3}{4}\right) \mathbf{a}_1 - x_4 \mathbf{a}_2 + \left(x_4 + \frac{3}{4}\right) \mathbf{a}_3 &= & \frac{3}{8}a \hat{\mathbf{x}} + a\left(x_4 + \frac{3}{4}\right) \hat{\mathbf{y}} + \frac{3}{8}a \hat{\mathbf{z}} & (48f) & \text{W I} \\
\mathbf{B}_{24} &= -x_4 \mathbf{a}_1 + \left(x_4 + \frac{3}{4}\right) \mathbf{a}_2 - x_4 \mathbf{a}_3 &= & \frac{3}{8}a \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} + \frac{3}{8}a \hat{\mathbf{z}} & (48f) & \text{W I} \\
\mathbf{B}_{25} &= -x_4 \mathbf{a}_1 + \left(x_4 + \frac{3}{4}\right) \mathbf{a}_2 + &= & a\left(x_4 + \frac{3}{4}\right) \hat{\mathbf{x}} + \frac{3}{8}a \hat{\mathbf{y}} + \frac{3}{8}a \hat{\mathbf{z}} & (48f) & \text{W I} \\
&& \left(x_4 + \frac{3}{4}\right) \mathbf{a}_3 & & & \\
\mathbf{B}_{26} &= \left(x_4 + \frac{3}{4}\right) \mathbf{a}_1 - x_4 \mathbf{a}_2 - x_4 \mathbf{a}_3 &= & -ax_4 \hat{\mathbf{x}} + \frac{3}{8}a \hat{\mathbf{y}} + \frac{3}{8}a \hat{\mathbf{z}} & (48f) & \text{W I} \\
\mathbf{B}_{27} &= -x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 + \left(x_4 + \frac{3}{4}\right) \mathbf{a}_3 &= & \frac{3}{8}a \hat{\mathbf{x}} + \frac{3}{8}a \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}} & (48f) & \text{W I} \\
\mathbf{B}_{28} &= \left(x_4 + \frac{3}{4}\right) \mathbf{a}_1 + \left(x_4 + \frac{3}{4}\right) \mathbf{a}_2 - x_4 \mathbf{a}_3 &= & \frac{3}{8}a \hat{\mathbf{x}} + \frac{3}{8}a \hat{\mathbf{y}} + a\left(x_4 + \frac{3}{4}\right) \hat{\mathbf{z}} & (48f) & \text{W I}
\end{aligned}$$

## References

- [1] Q.-B. Yang and S. Andersson, *Application of coincidence site lattices for crystal structure description. Part I:  $\Sigma = 3$* , Acta Crystallogr. Sect. B **43**, 1–14 (1987), doi:10.1107/S0108768187098380.