

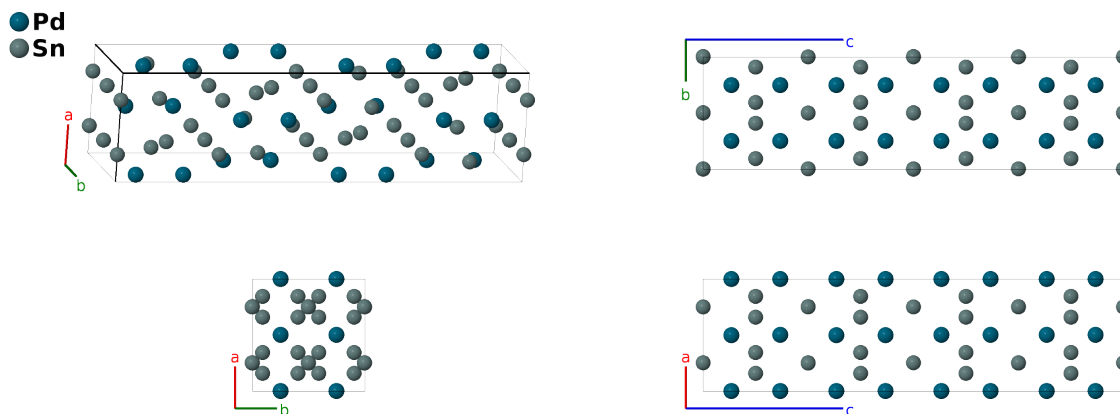
α -PdSn₂ Structure:

AB2_tI48_142_d_ef-001

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<https://aflow.org/p/FUUU>

https://aflow.org/p/AB2_tI48_142_d_ef-001



Prototype	PdSn ₂
AFLOW prototype label	AB2_tI48_142_d_ef-001
ICSD	30235
Pearson symbol	tI48
Space group number	142
Space group symbol	$I4_1/acd$
AFLOW prototype command	<code>aflow --proto=AB2_tI48_142_d_ef-001 --params=a, c/a, z1, x2, x3</code>

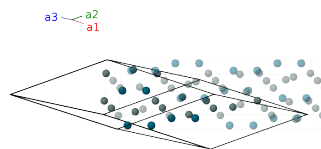
- This structure is stable up to 600°C. (Villars, 2016)
- PdSn₂ has also been found in the orthorhombic C_e structure.
- The ICSD entry is from (Hellner, 1956), but we use the refined data from (Künnen, 2000) for this presentation.

Body-centered Tetragonal primitive vectors

$$\mathbf{a}_1 = -\frac{1}{2}a \hat{x} + \frac{1}{2}a \hat{y} + \frac{1}{2}c \hat{z}$$

$$\mathbf{a}_2 = \frac{1}{2}a \hat{x} - \frac{1}{2}a \hat{y} + \frac{1}{2}c \hat{z}$$

$$\mathbf{a}_3 = \frac{1}{2}a \hat{x} + \frac{1}{2}a \hat{y} - \frac{1}{2}c \hat{z}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= (z_1 + \frac{1}{4}) \mathbf{a}_1 + z_1 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(16d)	Pd I
\mathbf{B}_2	$= z_1 \mathbf{a}_1 + (z_1 + \frac{1}{4}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{4} a \hat{\mathbf{y}} + c (z_1 - \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Pd I
\mathbf{B}_3	$= -(z_1 - \frac{1}{4}) \mathbf{a}_1 - (z_1 - \frac{1}{2}) \mathbf{a}_2 +$ $\frac{3}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{4} a \hat{\mathbf{y}} - cz_1 \hat{\mathbf{z}}$	(16d)	Pd I
\mathbf{B}_4	$= -(z_1 - \frac{1}{2}) \mathbf{a}_1 - (z_1 - \frac{1}{4}) \mathbf{a}_2 +$ $\frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{y}} - c (z_1 - \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Pd I
\mathbf{B}_5	$= -(z_1 - \frac{3}{4}) \mathbf{a}_1 - z_1 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{3}{4} a \hat{\mathbf{y}} - cz_1 \hat{\mathbf{z}}$	(16d)	Pd I
\mathbf{B}_6	$= -z_1 \mathbf{a}_1 - (z_1 - \frac{3}{4}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - \frac{1}{4} a \hat{\mathbf{y}} - c (z_1 - \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Pd I
\mathbf{B}_7	$= (z_1 + \frac{3}{4}) \mathbf{a}_1 + (z_1 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{y}} + c (z_1 + \frac{1}{2}) \hat{\mathbf{z}}$	(16d)	Pd I
\mathbf{B}_8	$= (z_1 + \frac{1}{2}) \mathbf{a}_1 + (z_1 + \frac{3}{4}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{4} a \hat{\mathbf{y}} + c (z_1 + \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Pd I
\mathbf{B}_9	$= \frac{1}{4} \mathbf{a}_1 + (x_2 + \frac{1}{4}) \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + \frac{1}{4} c \hat{\mathbf{z}}$	(16e)	Sn I
\mathbf{B}_{10}	$= \frac{3}{4} \mathbf{a}_1 - (x_2 - \frac{1}{4}) \mathbf{a}_2 - (x_2 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}}$	(16e)	Sn I
\mathbf{B}_{11}	$= (x_2 + \frac{1}{4}) \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{x}} + a (x_2 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(16e)	Sn I
\mathbf{B}_{12}	$= -(x_2 - \frac{1}{4}) \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 -$ $(x_2 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{x}} - a (x_2 - \frac{1}{4}) \hat{\mathbf{y}}$	(16e)	Sn I
\mathbf{B}_{13}	$= \frac{3}{4} \mathbf{a}_1 - (x_2 - \frac{3}{4}) \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + \frac{3}{4} c \hat{\mathbf{z}}$	(16e)	Sn I
\mathbf{B}_{14}	$= \frac{1}{4} \mathbf{a}_1 + (x_2 + \frac{3}{4}) \mathbf{a}_2 + (x_2 + \frac{1}{2}) \mathbf{a}_3$	$=$	$a (x_2 + \frac{1}{2}) \hat{\mathbf{x}} + \frac{1}{4} c \hat{\mathbf{z}}$	(16e)	Sn I
\mathbf{B}_{15}	$= -(x_2 - \frac{3}{4}) \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$-\frac{1}{4} a \hat{\mathbf{x}} - a (x_2 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(16e)	Sn I
\mathbf{B}_{16}	$= (x_2 + \frac{3}{4}) \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + (x_2 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{x}} + a (x_2 + \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(16e)	Sn I
\mathbf{B}_{17}	$= (x_3 + \frac{3}{8}) \mathbf{a}_1 + (x_3 + \frac{1}{8}) \mathbf{a}_2 +$ $(2x_3 + \frac{1}{4}) \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + a (x_3 + \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{8} c \hat{\mathbf{z}}$	(16f)	Sn II
\mathbf{B}_{18}	$= -(x_3 - \frac{3}{8}) \mathbf{a}_1 - (x_3 - \frac{1}{8}) \mathbf{a}_2 -$ $(2x_3 - \frac{1}{4}) \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} - a (x_3 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{8} c \hat{\mathbf{z}}$	(16f)	Sn II
\mathbf{B}_{19}	$= (x_3 + \frac{1}{8}) \mathbf{a}_1 - (x_3 - \frac{3}{8}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$-a (x_3 - \frac{1}{2}) \hat{\mathbf{x}} + a (x_3 + \frac{1}{4}) \hat{\mathbf{y}} - \frac{1}{8} c \hat{\mathbf{z}}$	(16f)	Sn II
\mathbf{B}_{20}	$= -(x_3 - \frac{1}{8}) \mathbf{a}_1 + (x_3 + \frac{3}{8}) \mathbf{a}_2 +$ $\frac{3}{4} \mathbf{a}_3$	$=$	$a (x_3 + \frac{1}{2}) \hat{\mathbf{x}} - a (x_3 - \frac{1}{4}) \hat{\mathbf{y}} - \frac{1}{8} c \hat{\mathbf{z}}$	(16f)	Sn II
\mathbf{B}_{21}	$= -(x_3 - \frac{5}{8}) \mathbf{a}_1 - (x_3 - \frac{7}{8}) \mathbf{a}_2 -$ $(2x_3 - \frac{3}{4}) \mathbf{a}_3$	$=$	$-a (x_3 - \frac{1}{2}) \hat{\mathbf{x}} - a (x_3 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{3}{8} c \hat{\mathbf{z}}$	(16f)	Sn II
\mathbf{B}_{22}	$= (x_3 + \frac{5}{8}) \mathbf{a}_1 + (x_3 + \frac{7}{8}) \mathbf{a}_2 +$ $(2x_3 + \frac{3}{4}) \mathbf{a}_3$	$=$	$a (x_3 + \frac{1}{2}) \hat{\mathbf{x}} + a (x_3 + \frac{1}{4}) \hat{\mathbf{y}} + \frac{3}{8} c \hat{\mathbf{z}}$	(16f)	Sn II
\mathbf{B}_{23}	$= -(x_3 - \frac{7}{8}) \mathbf{a}_1 + (x_3 + \frac{5}{8}) \mathbf{a}_2 +$ $\frac{1}{4} \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} - a (x_3 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{5}{8} c \hat{\mathbf{z}}$	(16f)	Sn II
\mathbf{B}_{24}	$= (x_3 + \frac{7}{8}) \mathbf{a}_1 - (x_3 - \frac{5}{8}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} + a (x_3 + \frac{1}{4}) \hat{\mathbf{y}} + \frac{5}{8} c \hat{\mathbf{z}}$	(16f)	Sn II

References

- [1] E. Hellner, *Flu-Misch-Typen*, Zeitschrift für Kristallographie **107**, 99–123 (1956), doi:10.1524/zkri.1956.107.16.99.
- [2] P. Villars, ed., *PAULING FILE* (Springer, 2016), chap. Pd-Sn Binary Phase Diagram 0-100 at.% Sn.

Found in

- [1] B. Künnen, D. Niepmann, and W. Jeitschko, *Structure refinements and some properties of the transition metal stanides Os_3Sn_7 , Ir_5Sn_7 , $Ni_{0.402(4)}Pd_{0.598}Sn_4$, α - $PdSn_2$ and $PtSn_4$* , J. Alloys Compd. **309**, 1–9 (2000), doi:10.1016/S0925-8388(00)01042-2.