

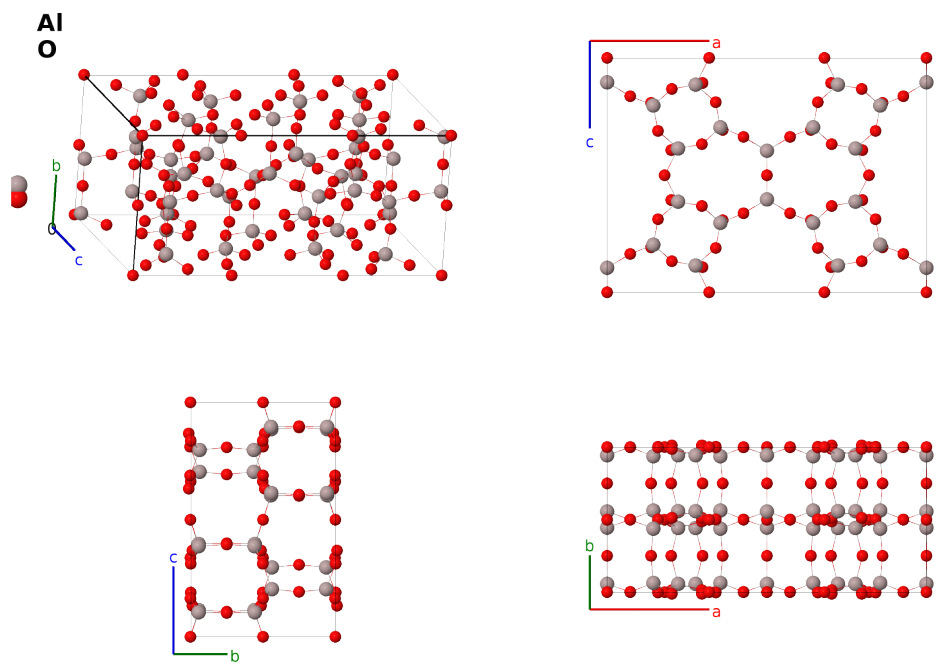
Disordered Calcined AlPO_4 -11 Structure: AB2_oI120_74_h2j_aef2i3j-001

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- D. Hicks, M. J. Mehl, M. Esters, C. Oses, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/prototype-encyclopedia/VR57>

https://aflow.org/prototype-encyclopedia/AB2_oI120_74_h2j_aef2i3j-001



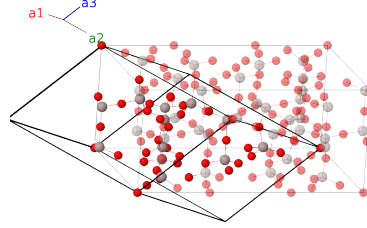
Prototype	AlO_4P
AFLOW prototype label	AB2_oI120_74_h2j_aef2i3j-001
ICSD	63665
CCDC	1626746
Pearson symbol	oI120
Space group number	74
Space group symbol	$Imma$
AFLOW prototype command	<code>aflow --proto=AB2_oI120_74_h2j_aef2i3j-001</code> <code>--params=a, b/a, c/a, z2, x3, y4, z4, x5, z5, x6, z6, x7, y7, z7, x8, y8, z8, x9, y9, z9, x10, y10,</code> <code>z10, x11, y11, z11</code>

- Samples of AlPO_4 -11 were calcined at 873K to remove impurities and then dehydrated at 573K. Data was collected at 295K.

- (Richardson, 1988) found an ordered structure, but also found a good fit to the data by assuming this disordered phase where the aluminum and phosphorous atoms are randomly distributed. We arbitrarily label these mixed Al/P sites as aluminum. This randomization changes the space group from polar *Ima2* #46 to centrosymmetric *Imma* #74.
- More information about AlPO_4 structures can be found on the SiO_2 and AlPO_4 page.
- (Richardson, 1988) give the data for this structure in the *Icmm* setting of space group #74. We used AFLOW to transform it into the standard *Imma* setting.

Body-centered Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}} - \frac{1}{2}c\hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= 0$	$=$	0	(4a)	O I
$\mathbf{B}_2$	$= \frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}b\hat{\mathbf{y}}$	(4a)	O I
$\mathbf{B}_3$	$= (z_2 + \frac{1}{4})\mathbf{a}_1 + z_2\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$	$=$	$\frac{1}{4}b\hat{\mathbf{y}} + cz_2\hat{\mathbf{z}}$	(4e)	O II
$\mathbf{B}_4$	$= -(z_2 - \frac{3}{4})\mathbf{a}_1 - z_2\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$	$=$	$\frac{3}{4}b\hat{\mathbf{y}} - cz_2\hat{\mathbf{z}}$	(4e)	O II
$\mathbf{B}_5$	$= x_3\mathbf{a}_2 + x_3\mathbf{a}_3$	$=$	$ax_3\hat{\mathbf{x}}$	(8f)	O III
$\mathbf{B}_6$	$= \frac{1}{2}\mathbf{a}_1 - x_3\mathbf{a}_2 - (x_3 - \frac{1}{2})\mathbf{a}_3$	$=$	$-ax_3\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}}$	(8f)	O III
$\mathbf{B}_7$	$= -x_3\mathbf{a}_2 - x_3\mathbf{a}_3$	$=$	$-ax_3\hat{\mathbf{x}}$	(8f)	O III
$\mathbf{B}_8$	$= \frac{1}{2}\mathbf{a}_1 + x_3\mathbf{a}_2 + (x_3 + \frac{1}{2})\mathbf{a}_3$	$=$	$ax_3\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}}$	(8f)	O III
$\mathbf{B}_9$	$= (y_4 + z_4)\mathbf{a}_1 + z_4\mathbf{a}_2 + y_4\mathbf{a}_3$	$=$	$by_4\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(8h)	Al I
$\mathbf{B}_{10}$	$= (-y_4 + z_4 + \frac{1}{2})\mathbf{a}_1 + z_4\mathbf{a}_2 - (y_4 - \frac{1}{2})\mathbf{a}_3$	$=$	$-b(y_4 - \frac{1}{2})\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(8h)	Al I
$\mathbf{B}_{11}$	$= (y_4 - z_4 + \frac{1}{2})\mathbf{a}_1 - z_4\mathbf{a}_2 + (y_4 + \frac{1}{2})\mathbf{a}_3$	$=$	$b(y_4 + \frac{1}{2})\hat{\mathbf{y}} - cz_4\hat{\mathbf{z}}$	(8h)	Al I
$\mathbf{B}_{12}$	$= -(y_4 + z_4)\mathbf{a}_1 - z_4\mathbf{a}_2 - y_4\mathbf{a}_3$	$=$	$-by_4\hat{\mathbf{y}} - cz_4\hat{\mathbf{z}}$	(8h)	Al I
$\mathbf{B}_{13}$	$= (z_5 + \frac{1}{4})\mathbf{a}_1 + (x_5 + z_5)\mathbf{a}_2 + (x_5 + \frac{1}{4})\mathbf{a}_3$	$=$	$ax_5\hat{\mathbf{x}} + \frac{1}{4}b\hat{\mathbf{y}} + cz_5\hat{\mathbf{z}}$	(8i)	O IV
$\mathbf{B}_{14}$	$= (z_5 + \frac{1}{4})\mathbf{a}_1 - (x_5 - z_5)\mathbf{a}_2 - (x_5 - \frac{1}{4})\mathbf{a}_3$	$=$	$-ax_5\hat{\mathbf{x}} + \frac{1}{4}b\hat{\mathbf{y}} + cz_5\hat{\mathbf{z}}$	(8i)	O IV
$\mathbf{B}_{15}$	$= -(z_5 - \frac{3}{4})\mathbf{a}_1 - (x_5 + z_5)\mathbf{a}_2 - (x_5 - \frac{3}{4})\mathbf{a}_3$	$=$	$-ax_5\hat{\mathbf{x}} + \frac{3}{4}b\hat{\mathbf{y}} - cz_5\hat{\mathbf{z}}$	(8i)	O IV
$\mathbf{B}_{16}$	$= -(z_5 - \frac{3}{4})\mathbf{a}_1 + (x_5 - z_5)\mathbf{a}_2 + (x_5 + \frac{3}{4})\mathbf{a}_3$	$=$	$ax_5\hat{\mathbf{x}} + \frac{3}{4}b\hat{\mathbf{y}} - cz_5\hat{\mathbf{z}}$	(8i)	O IV
$\mathbf{B}_{17}$	$= (z_6 + \frac{1}{4})\mathbf{a}_1 + (x_6 + z_6)\mathbf{a}_2 + (x_6 + \frac{1}{4})\mathbf{a}_3$	$=$	$ax_6\hat{\mathbf{x}} + \frac{1}{4}b\hat{\mathbf{y}} + cz_6\hat{\mathbf{z}}$	(8i)	O V

$\mathbf{B}_{18}$	$=$	$(z_6 + \frac{1}{4}) \mathbf{a}_1 - (x_6 - z_6) \mathbf{a}_2 -$	$=$	$-ax_6 \hat{\mathbf{x}} + \frac{1}{4}b \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	$(8i)$	O V
		$(x_6 - \frac{1}{4}) \mathbf{a}_3$				
$\mathbf{B}_{19}$	$=$	$-(z_6 - \frac{3}{4}) \mathbf{a}_1 - (x_6 + z_6) \mathbf{a}_2 -$	$=$	$-ax_6 \hat{\mathbf{x}} + \frac{3}{4}b \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	$(8i)$	O V
		$(x_6 - \frac{3}{4}) \mathbf{a}_3$				
$\mathbf{B}_{20}$	$=$	$-(z_6 - \frac{3}{4}) \mathbf{a}_1 + (x_6 - z_6) \mathbf{a}_2 +$	$=$	$ax_6 \hat{\mathbf{x}} + \frac{3}{4}b \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	$(8i)$	O V
		$(x_6 + \frac{3}{4}) \mathbf{a}_3$				
$\mathbf{B}_{21}$	$=$	$(y_7 + z_7) \mathbf{a}_1 + (x_7 + z_7) \mathbf{a}_2 +$	$=$	$ax_7 \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	$(16j)$	Al II
		$(x_7 + y_7) \mathbf{a}_3$				
$\mathbf{B}_{22}$	$=$	$(-y_7 + z_7 + \frac{1}{2}) \mathbf{a}_1 -$	$=$	$-ax_7 \hat{\mathbf{x}} - b(y_7 - \frac{1}{2}) \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	$(16j)$	Al II
		$(x_7 - z_7) \mathbf{a}_2 - (x_7 + y_7 - \frac{1}{2}) \mathbf{a}_3$				
$\mathbf{B}_{23}$	$=$	$(y_7 - z_7 + \frac{1}{2}) \mathbf{a}_1 - (x_7 + z_7) \mathbf{a}_2 +$	$=$	$-ax_7 \hat{\mathbf{x}} + b(y_7 + \frac{1}{2}) \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	$(16j)$	Al II
		$(-x_7 + y_7 + \frac{1}{2}) \mathbf{a}_3$				
$\mathbf{B}_{24}$	$=$	$-(y_7 + z_7) \mathbf{a}_1 + (x_7 - z_7) \mathbf{a}_2 +$	$=$	$ax_7 \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	$(16j)$	Al II
		$(x_7 - y_7) \mathbf{a}_3$				
$\mathbf{B}_{25}$	$=$	$-(y_7 + z_7) \mathbf{a}_1 - (x_7 + z_7) \mathbf{a}_2 -$	$=$	$-ax_7 \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	$(16j)$	Al II
		$(x_7 + y_7) \mathbf{a}_3$				
$\mathbf{B}_{26}$	$=$	$(y_7 - z_7 + \frac{1}{2}) \mathbf{a}_1 +$	$=$	$ax_7 \hat{\mathbf{x}} + b(y_7 + \frac{1}{2}) \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	$(16j)$	Al II
		$(x_7 - z_7) \mathbf{a}_2 + (x_7 + y_7 + \frac{1}{2}) \mathbf{a}_3$				
$\mathbf{B}_{27}$	$=$	$(-y_7 + z_7 + \frac{1}{2}) \mathbf{a}_1 +$	$=$	$ax_7 \hat{\mathbf{x}} - b(y_7 - \frac{1}{2}) \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	$(16j)$	Al II
		$(x_7 + z_7) \mathbf{a}_2 + (x_7 - y_7 + \frac{1}{2}) \mathbf{a}_3$				
$\mathbf{B}_{28}$	$=$	$(y_7 + z_7) \mathbf{a}_1 - (x_7 - z_7) \mathbf{a}_2 -$	$=$	$-ax_7 \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	$(16j)$	Al II
		$(x_7 - y_7) \mathbf{a}_3$				
$\mathbf{B}_{29}$	$=$	$(y_8 + z_8) \mathbf{a}_1 + (x_8 + z_8) \mathbf{a}_2 +$	$=$	$ax_8 \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	$(16j)$	Al III
		$(x_8 + y_8) \mathbf{a}_3$				
$\mathbf{B}_{30}$	$=$	$(-y_8 + z_8 + \frac{1}{2}) \mathbf{a}_1 -$	$=$	$-ax_8 \hat{\mathbf{x}} - b(y_8 - \frac{1}{2}) \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	$(16j)$	Al III
		$(x_8 - z_8) \mathbf{a}_2 - (x_8 + y_8 - \frac{1}{2}) \mathbf{a}_3$				
$\mathbf{B}_{31}$	$=$	$(y_8 - z_8 + \frac{1}{2}) \mathbf{a}_1 - (x_8 + z_8) \mathbf{a}_2 +$	$=$	$-ax_8 \hat{\mathbf{x}} + b(y_8 + \frac{1}{2}) \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	$(16j)$	Al III
		$(-x_8 + y_8 + \frac{1}{2}) \mathbf{a}_3$				
$\mathbf{B}_{32}$	$=$	$-(y_8 + z_8) \mathbf{a}_1 + (x_8 - z_8) \mathbf{a}_2 +$	$=$	$ax_8 \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	$(16j)$	Al III
		$(x_8 - y_8) \mathbf{a}_3$				
$\mathbf{B}_{33}$	$=$	$-(y_8 + z_8) \mathbf{a}_1 - (x_8 + z_8) \mathbf{a}_2 -$	$=$	$-ax_8 \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	$(16j)$	Al III
		$(x_8 + y_8) \mathbf{a}_3$				
$\mathbf{B}_{34}$	$=$	$(y_8 - z_8 + \frac{1}{2}) \mathbf{a}_1 +$	$=$	$ax_8 \hat{\mathbf{x}} + b(y_8 + \frac{1}{2}) \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	$(16j)$	Al III
		$(x_8 - z_8) \mathbf{a}_2 + (x_8 + y_8 + \frac{1}{2}) \mathbf{a}_3$				
$\mathbf{B}_{35}$	$=$	$(-y_8 + z_8 + \frac{1}{2}) \mathbf{a}_1 +$	$=$	$ax_8 \hat{\mathbf{x}} - b(y_8 - \frac{1}{2}) \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	$(16j)$	Al III
		$(x_8 + z_8) \mathbf{a}_2 + (x_8 - y_8 + \frac{1}{2}) \mathbf{a}_3$				
$\mathbf{B}_{36}$	$=$					

$$\begin{aligned}
\mathbf{B}_{41} &= \begin{matrix} -(y_9 + z_9) \mathbf{a}_1 - (x_9 + z_9) \mathbf{a}_2 - \\ (x_9 + y_9) \mathbf{a}_3 \end{matrix} = -ax_9 \hat{\mathbf{x}} - by_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}} & (16j) & \text{O VI} \\
\mathbf{B}_{42} &= \begin{matrix} (y_9 - z_9 + \frac{1}{2}) \mathbf{a}_1 + \\ (x_9 - z_9) \mathbf{a}_2 + (x_9 + y_9 + \frac{1}{2}) \mathbf{a}_3 \end{matrix} = ax_9 \hat{\mathbf{x}} + b(y_9 + \frac{1}{2}) \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}} & (16j) & \text{O VI} \\
\mathbf{B}_{43} &= \begin{matrix} (-y_9 + z_9 + \frac{1}{2}) \mathbf{a}_1 + \\ (x_9 + z_9) \mathbf{a}_2 + (x_9 - y_9 + \frac{1}{2}) \mathbf{a}_3 \end{matrix} = ax_9 \hat{\mathbf{x}} - b(y_9 - \frac{1}{2}) \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}} & (16j) & \text{O VI} \\
\mathbf{B}_{44} &= \begin{matrix} (y_9 + z_9) \mathbf{a}_1 - (x_9 - z_9) \mathbf{a}_2 - \\ (x_9 - y_9) \mathbf{a}_3 \end{matrix} = -ax_9 \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}} & (16j) & \text{O VI} \\
\mathbf{B}_{45} &= \begin{matrix} (y_{10} + z_{10}) \mathbf{a}_1 + (x_{10} + z_{10}) \mathbf{a}_2 + \\ (x_{10} + y_{10}) \mathbf{a}_3 \end{matrix} = ax_{10} \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} & (16j) & \text{O VII} \\
\mathbf{B}_{46} &= \begin{matrix} (-y_{10} + z_{10} + \frac{1}{2}) \mathbf{a}_1 - \\ (x_{10} - z_{10}) \mathbf{a}_2 - \\ (x_{10} + y_{10} - \frac{1}{2}) \mathbf{a}_3 \end{matrix} = -ax_{10} \hat{\mathbf{x}} - b(y_{10} - \frac{1}{2}) \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} & (16j) & \text{O VII} \\
\mathbf{B}_{47} &= \begin{matrix} (y_{10} - z_{10} + \frac{1}{2}) \mathbf{a}_1 - \\ (x_{10} + z_{10}) \mathbf{a}_2 + \\ (-x_{10} + y_{10} + \frac{1}{2}) \mathbf{a}_3 \end{matrix} = -ax_{10} \hat{\mathbf{x}} + b(y_{10} + \frac{1}{2}) \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}} & (16j) & \text{O VII} \\
\mathbf{B}_{48} &= \begin{matrix} -(y_{10} + z_{10}) \mathbf{a}_1 + \\ (x_{10} - z_{10}) \mathbf{a}_2 + (x_{10} - y_{10}) \mathbf{a}_3 \end{matrix} = ax_{10} \hat{\mathbf{x}} - by_{10} \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}} & (16j) & \text{O VII} \\
\mathbf{B}_{49} &= \begin{matrix} -(y_{10} + z_{10}) \mathbf{a}_1 - \\ (x_{10} + z_{10}) \mathbf{a}_2 - (x_{10} + y_{10}) \mathbf{a}_3 \end{matrix} = -ax_{10} \hat{\mathbf{x}} - by_{10} \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}} & (16j) & \text{O VII} \\
\mathbf{B}_{50} &= \begin{matrix} (y_{10} - z_{10} + \frac{1}{2}) \mathbf{a}_1 + \\ (x_{10} - z_{10}) \mathbf{a}_2 + \\ (x_{10} + y_{10} + \frac{1}{2}) \mathbf{a}_3 \end{matrix} = ax_{10} \hat{\mathbf{x}} + b(y_{10} + \frac{1}{2}) \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}} & (16j) & \text{O VII} \\
\mathbf{B}_{51} &= \begin{matrix} (-y_{10} + z_{10} + \frac{1}{2}) \mathbf{a}_1 + \\ (x_{10} + z_{10}) \mathbf{a}_2 + \\ (x_{10} - y_{10} + \frac{1}{2}) \mathbf{a}_3 \end{matrix} = ax_{10} \hat{\mathbf{x}} - b(y_{10} - \frac{1}{2}) \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} & (16j) & \text{O VII} \\
\mathbf{B}_{52} &= \begin{matrix} (y_{10} + z_{10}) \mathbf{a}_1 - (x_{10} - z_{10}) \mathbf{a}_2 - \\ (x_{10} - y_{10}) \mathbf{a}_3 \end{matrix} = -ax_{10} \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} & (16j) & \text{O VII} \\
\mathbf{B}_{53} &= \begin{matrix} (y_{11} + z_{11}) \mathbf{a}_1 + (x_{11} + z_{11}) \mathbf{a}_2 + \\ (x_{11} + y_{11}) \mathbf{a}_3 \end{matrix} = ax_{11} \hat{\mathbf{x}} + by_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} & (16j) & \text{O VIII} \\
\mathbf{B}_{54} &= \begin{matrix} (-y_{11} + z_{11} + \frac{1}{2}) \mathbf{a}_1 - \\ (x_{11} - z_{11}) \mathbf{a}_2 - \\ (x_{11} + y_{11} - \frac{1}{2}) \mathbf{a}_3 \end{matrix} = -ax_{11} \hat{\mathbf{x}} - b(y_{11} - \frac{1}{2}) \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} & (16j) & \text{O VIII} \\
\mathbf{B}_{55} &= \begin{matrix} (y_{11} - z_{11} + \frac{1}{2}) \mathbf{a}_1 - \\ (x_{11} + z_{11}) \mathbf{a}_2 + \\ (-x_{11} + y_{11} + \frac{1}{2}) \mathbf{a}_3 \end{matrix} = -ax_{11} \hat{\mathbf{x}} + b(y_{11} + \frac{1}{2}) \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} & (16j) & \text{O VIII} \\
\mathbf{B}_{56} &= \begin{matrix} -(y_{11} + z_{11}) \mathbf{a}_1 + \\ (x_{11} - z_{11}) \mathbf{a}_2 + (x_{11} - y_{11}) \mathbf{a}_3 \end{matrix} = ax_{11} \hat{\mathbf{x}} - by_{11} \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} & (16j) & \text{O VIII} \\
\mathbf{B}_{57} &= \begin{matrix} -(y_{11} + z_{11}) \mathbf{a}_1 - \\ (x_{11} + z_{11}) \mathbf{a}_2 - (x_{11} + y_{11}) \mathbf{a}_3 \end{matrix} = -ax_{11} \hat{\mathbf{x}} - by_{11} \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} & (16j) & \text{O VIII} \\
\mathbf{B}_{58} &= \begin{matrix} (y_{11} - z_{11} + \frac{1}{2}) \mathbf{a}_1 + \\ (x_{11} - z_{11}) \mathbf{a}_2 + \\ (x_{11} + y_{11} + \frac{1}{2}) \mathbf{a}_3 \end{matrix} = ax_{11} \hat{\mathbf{x}} + b(y_{11} + \frac{1}{2}) \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} & (16j) & \text{O VIII} \\
\mathbf{B}_{59} &= \begin{matrix} (-y_{11} + z_{11} + \frac{1}{2}) \mathbf{a}_1 + \\ (x_{11} + z_{11}) \mathbf{a}_2 + \\ (x_{11} - y_{11} + \frac{1}{2}) \mathbf{a}_3 \end{matrix} = ax_{11} \hat{\mathbf{x}} - b(y_{11} - \frac{1}{2}) \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} & (16j) & \text{O VIII} \\
\mathbf{B}_{60} &= \begin{matrix} (y_{11} + z_{11}) \mathbf{a}_1 - (x_{11} - z_{11}) \mathbf{a}_2 - \\ (x_{11} - y_{11}) \mathbf{a}_3 \end{matrix} = -ax_{11} \hat{\mathbf{x}} + by_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} & (16j) & \text{O VIII}
\end{aligned}$$

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