

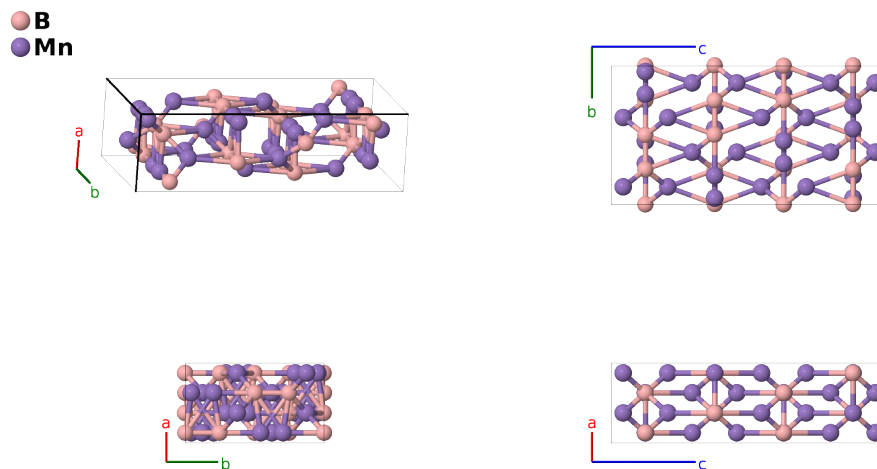
Mn₂B (*D*1_{*f*}) Structure: AB2_oF48_70_e_ef-001

This structure originally had the label AB2_oF48_70_f_fg. Calls to that address will be redirected here.

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<https://afLOW.org/p/RZ74>

https://afLOW.org/p/AB2_oF48_70_e_ef-001



Prototype	BMn ₂
AFLOW prototype label	AB2_oF48_70_e_ef-001
<i>Strukturbericht</i> designation	<i>D</i> 1 _{<i>f</i>}
ICSD	86398
Pearson symbol	oF48
Space group number	70
Space group symbol	<i>Fddd</i>
AFLOW prototype command	<code>afLOW --proto=AB2_oF48_70_e_ef-001 --params=a, b/a, c/a, x₁, x₂, y₃</code>

Other compounds with this structure

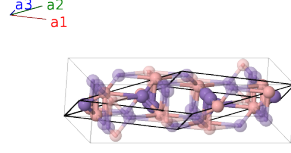
Cr₂B

- Early works, *e.g.* (Pearson, 1958), referred to this structure as Mn₄B, with the same space group and Wyckoff positions. The stoichiometry was fixed by assuming that the (16e) boron positions were only half-occupied. The (Tergenius, 1981) refinement of the structure showed that the (16e) sites were totally filled, fixing the stoichiometry to Mn₂B. A similar reanalysis showed that the similar structure known as Cr₄B also had composition Cr₂B.
- Tergenius gives the atomic positions using the first setting of space group *Fddd* #70. We have translated this into the second setting, where the origin is on an inversion site. As a part of this process the primitive axes were also rotated compared to Tergenius.

- Mn_2B ($D1_f$) and CuMg_2 (C_b) have the same AFLOW prototype label, AB2_oF48_70_e_ef. They are generated by the same symmetry operations with different sets of parameters (`--params`) specified in their corresponding CIF files.

Face-centered Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}}\end{aligned}$$



Basis vectors

	Lattice coordinates	Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= -(x_1 - \frac{1}{4})\mathbf{a}_1 + x_1\mathbf{a}_2 + x_1\mathbf{a}_3 =$	$ax_1\hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	B I
\mathbf{B}_2	$= x_1\mathbf{a}_1 - (x_1 - \frac{1}{4})\mathbf{a}_2 - (x_1 - \frac{1}{4})\mathbf{a}_3 =$	$-a(x_1 - \frac{1}{4})\hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	B I
\mathbf{B}_3	$= (x_1 + \frac{3}{4})\mathbf{a}_1 - x_1\mathbf{a}_2 - x_1\mathbf{a}_3 =$	$-ax_1\hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	B I
\mathbf{B}_4	$= -x_1\mathbf{a}_1 + (x_1 + \frac{3}{4})\mathbf{a}_2 + (x_1 + \frac{3}{4})\mathbf{a}_3 =$	$a(x_1 + \frac{3}{4})\hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	B I
\mathbf{B}_5	$= -(x_2 - \frac{1}{4})\mathbf{a}_1 + x_2\mathbf{a}_2 + x_2\mathbf{a}_3 =$	$ax_2\hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	Mn I
\mathbf{B}_6	$= x_2\mathbf{a}_1 - (x_2 - \frac{1}{4})\mathbf{a}_2 - (x_2 - \frac{1}{4})\mathbf{a}_3 =$	$-a(x_2 - \frac{1}{4})\hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	Mn I
\mathbf{B}_7	$= (x_2 + \frac{3}{4})\mathbf{a}_1 - x_2\mathbf{a}_2 - x_2\mathbf{a}_3 =$	$-ax_2\hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	Mn I
\mathbf{B}_8	$= -x_2\mathbf{a}_1 + (x_2 + \frac{3}{4})\mathbf{a}_2 + (x_2 + \frac{3}{4})\mathbf{a}_3 =$	$a(x_2 + \frac{3}{4})\hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	Mn I
\mathbf{B}_9	$= y_3\mathbf{a}_1 - (y_3 - \frac{1}{4})\mathbf{a}_2 + y_3\mathbf{a}_3 =$	$\frac{1}{8}a\hat{\mathbf{x}} + by_3\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16f)	Mn II
\mathbf{B}_{10}	$= -(y_3 - \frac{1}{4})\mathbf{a}_1 + y_3\mathbf{a}_2 - (y_3 - \frac{1}{4})\mathbf{a}_3 =$	$\frac{1}{8}a\hat{\mathbf{x}} - b(y_3 - \frac{1}{4})\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16f)	Mn II
\mathbf{B}_{11}	$= -y_3\mathbf{a}_1 + (y_3 + \frac{3}{4})\mathbf{a}_2 - y_3\mathbf{a}_3 =$	$\frac{3}{8}a\hat{\mathbf{x}} - by_3\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16f)	Mn II
\mathbf{B}_{12}	$= (y_3 + \frac{3}{4})\mathbf{a}_1 - y_3\mathbf{a}_2 + (y_3 + \frac{3}{4})\mathbf{a}_3 =$	$\frac{3}{8}a\hat{\mathbf{x}} + b(y_3 + \frac{3}{4})\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16f)	Mn II

References

- [1] L.-E. Tergenius, *Refinement of the crystal structure of orthorhombic Mn_2B (formerly denoted Mn_4B)*, J. Less-Common Met. **82**, 335–340 (1981), doi:10.1016/0022-5088(81)90236-8.
- [2] W. B. Pearson, *A Handbook of Lattice Spacings and Structures of Metals and Alloys*, no. N.R.C. No. 4303 in International Series of Monographs on Metal Physics and Physical Metallurgy (Pergamon Press, Oxford, London, Edinburgh, New York, Paris, Frankfurt, 1958), 1964 reprint with corrections edn.