

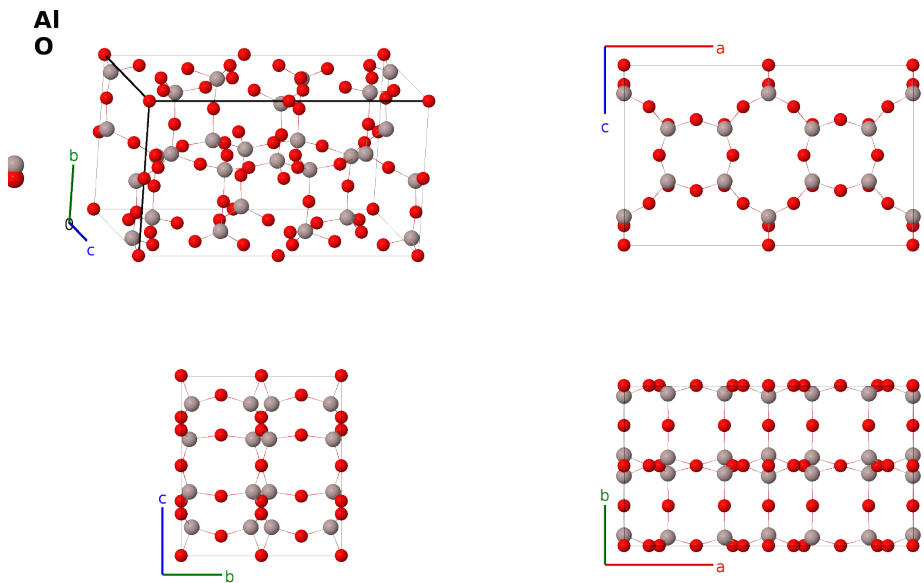
High-Temperature AlPO_4 -25 Structure: AB2_oC72_67_mo_cgilno-001

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<https://aflow.org/prototype-encyclopedia/E8FK>

https://aflow.org/prototype-encyclopedia/AB2_oC72_67_mo_cgilno-001



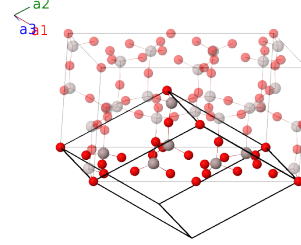
Prototype	AlO_4P
AFLOW prototype label	AB2_oC72_67_mo_cgilno-001
ICSD	108832
CCDC	1666476
Pearson symbol	oC72
Space group number	67
Space group symbol	$Cmme$
AFLOW prototype command	<code>aflow --proto=AB2_oC72_67_mo_cgilno-001</code> <code>--params=a, b/a, c/a, z2, x3, z4, y5, z5, x6, z6, x7, y7, z7, x8, y8, z8</code>

- Calcinated (heated below the melting temperature) AlPO_4 -21 loses its water molecules and accompanying embedded materials and transforms into the AlPO_4 -25 phase, with a structure in space group $Ibam$ #72 that (Richardson, 1990) were unable to resolve.
- Above 530K the structure transforms into this high-temperature structure, with a conventional unit cell half the size of the low-temperature cell.

- (Richardson, 1990) give the structure in the *Acm* setting of space group #67. AFLOW transforms this to the standard *Cmme* setting. Enforcing the AFLOW label convention then shifts the first oxygen atom from the (4e) to the (4c) Wyckoff position, with corresponding shifts in other Wyckoff positions.
- The metallic (8n) and (16o) sites randomly occupied by aluminum and phosphorous atoms. We arbitrarily chose aluminum to represent these sites.
- More information about AlPO_4 and related structures can be found on the silica and aluminum phosphate page.

Base-centered Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}b \hat{\mathbf{y}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$=$	0	$=$	0	(4c) O I
$\mathbf{B}_2$	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2}a \hat{\mathbf{x}}$	(4c) O I
$\mathbf{B}_3$	$=$	$\frac{3}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + z_2 \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{4}b \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(4g) O II
$\mathbf{B}_4$	$=$	$\frac{1}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - z_2 \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{4}b \hat{\mathbf{y}} - cz_2 \hat{\mathbf{z}}$	(4g) O II
$\mathbf{B}_5$	$=$	$x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8i) O III
$\mathbf{B}_6$	$=$	$-(x_3 - \frac{1}{2}) \mathbf{a}_1 - (x_3 - \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-a(x_3 - \frac{1}{2}) \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8i) O III
$\mathbf{B}_7$	$=$	$-x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8i) O III
$\mathbf{B}_8$	$=$	$(x_3 + \frac{1}{2}) \mathbf{a}_1 + (x_3 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$a(x_3 + \frac{1}{2}) \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8i) O III
$\mathbf{B}_9$	$=$	$\frac{1}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + z_4 \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + cz_4 \hat{\mathbf{z}}$	(8l) O IV
$\mathbf{B}_{10}$	$=$	$\frac{1}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 - z_4 \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} - cz_4 \hat{\mathbf{z}}$	(8l) O IV
$\mathbf{B}_{11}$	$=$	$\frac{3}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - z_4 \mathbf{a}_3$	$=$	$\frac{3}{4}a \hat{\mathbf{x}} - cz_4 \hat{\mathbf{z}}$	(8l) O IV
$\mathbf{B}_{12}$	$=$	$\frac{3}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + z_4 \mathbf{a}_3$	$=$	$\frac{3}{4}a \hat{\mathbf{x}} + cz_4 \hat{\mathbf{z}}$	(8l) O IV
$\mathbf{B}_{13}$	$=$	$-y_5 \mathbf{a}_1 + y_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(8m) Al I
$\mathbf{B}_{14}$	$=$	$(y_5 + \frac{1}{2}) \mathbf{a}_1 - (y_5 - \frac{1}{2}) \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(8m) Al I
$\mathbf{B}_{15}$	$=$	$-(y_5 - \frac{1}{2}) \mathbf{a}_1 + (y_5 + \frac{1}{2}) \mathbf{a}_2 - z_5 \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}}$	(8m) Al I
$\mathbf{B}_{16}$	$=$	$y_5 \mathbf{a}_1 - y_5 \mathbf{a}_2 - z_5 \mathbf{a}_3$	$=$	$-by_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}}$	(8m) Al I
$\mathbf{B}_{17}$	$=$	$(x_6 + \frac{3}{4}) \mathbf{a}_1 + (x_6 + \frac{1}{4}) \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$a(x_6 + \frac{1}{2}) \hat{\mathbf{x}} - \frac{1}{4}b \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(8n) O V
$\mathbf{B}_{18}$	$=$	$-(x_6 - \frac{3}{4}) \mathbf{a}_1 - (x_6 - \frac{1}{4}) \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$-a(x_6 - \frac{1}{2}) \hat{\mathbf{x}} - \frac{1}{4}b \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(8n) O V
$\mathbf{B}_{19}$	$=$	$-(x_6 - \frac{1}{4}) \mathbf{a}_1 - (x_6 - \frac{3}{4}) \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$-a(x_6 - \frac{1}{2}) \hat{\mathbf{x}} + \frac{1}{4}b \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(8n) O V
$\mathbf{B}_{20}$	$=$	$(x_6 + \frac{1}{4}) \mathbf{a}_1 + (x_6 + \frac{3}{4}) \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$a(x_6 + \frac{1}{2}) \hat{\mathbf{x}} + \frac{1}{4}b \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(8n) O V

$$\begin{aligned}
\mathbf{B}_{21} &= \begin{matrix} (x_7 - y_7) \mathbf{a}_1 + (x_7 + y_7) \mathbf{a}_2 + \\ z_7 \mathbf{a}_3 \end{matrix} = ax_7 \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (16o) & \text{Al II} \\
\mathbf{B}_{22} &= \begin{matrix} (-x_7 + y_7 + \frac{1}{2}) \mathbf{a}_1 - \\ (x_7 + y_7 - \frac{1}{2}) \mathbf{a}_2 + z_7 \mathbf{a}_3 \end{matrix} = -a(x_7 - \frac{1}{2}) \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (16o) & \text{Al II} \\
\mathbf{B}_{23} &= \begin{matrix} -(x_7 + y_7 - \frac{1}{2}) \mathbf{a}_1 + \\ (-x_7 + y_7 + \frac{1}{2}) \mathbf{a}_2 - z_7 \mathbf{a}_3 \end{matrix} = -a(x_7 - \frac{1}{2}) \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (16o) & \text{Al II} \\
\mathbf{B}_{24} &= \begin{matrix} (x_7 + y_7) \mathbf{a}_1 + (x_7 - y_7) \mathbf{a}_2 - \\ z_7 \mathbf{a}_3 \end{matrix} = ax_7 \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (16o) & \text{Al II} \\
\mathbf{B}_{25} &= \begin{matrix} -(x_7 - y_7) \mathbf{a}_1 - (x_7 + y_7) \mathbf{a}_2 - \\ z_7 \mathbf{a}_3 \end{matrix} = -ax_7 \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (16o) & \text{Al II} \\
\mathbf{B}_{26} &= \begin{matrix} (x_7 - y_7 + \frac{1}{2}) \mathbf{a}_1 + \\ (x_7 + y_7 + \frac{1}{2}) \mathbf{a}_2 - z_7 \mathbf{a}_3 \end{matrix} = a(x_7 + \frac{1}{2}) \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (16o) & \text{Al II} \\
\mathbf{B}_{27} &= \begin{matrix} (x_7 + y_7 + \frac{1}{2}) \mathbf{a}_1 + \\ (x_7 - y_7 + \frac{1}{2}) \mathbf{a}_2 + z_7 \mathbf{a}_3 \end{matrix} = a(x_7 + \frac{1}{2}) \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (16o) & \text{Al II} \\
\mathbf{B}_{28} &= \begin{matrix} -(x_7 + y_7) \mathbf{a}_1 - (x_7 - y_7) \mathbf{a}_2 + \\ z_7 \mathbf{a}_3 \end{matrix} = -ax_7 \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (16o) & \text{Al II} \\
\mathbf{B}_{29} &= \begin{matrix} (x_8 - y_8) \mathbf{a}_1 + (x_8 + y_8) \mathbf{a}_2 + \\ z_8 \mathbf{a}_3 \end{matrix} = ax_8 \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}} & (16o) & \text{O VI} \\
\mathbf{B}_{30} &= \begin{matrix} (-x_8 + y_8 + \frac{1}{2}) \mathbf{a}_1 - \\ (x_8 + y_8 - \frac{1}{2}) \mathbf{a}_2 + z_8 \mathbf{a}_3 \end{matrix} = -a(x_8 - \frac{1}{2}) \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}} & (16o) & \text{O VI} \\
\mathbf{B}_{31} &= \begin{matrix} -(x_8 + y_8 - \frac{1}{2}) \mathbf{a}_1 + \\ (-x_8 + y_8 + \frac{1}{2}) \mathbf{a}_2 - z_8 \mathbf{a}_3 \end{matrix} = -a(x_8 - \frac{1}{2}) \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}} & (16o) & \text{O VI} \\
\mathbf{B}_{32} &= \begin{matrix} (x_8 + y_8) \mathbf{a}_1 + (x_8 - y_8) \mathbf{a}_2 - \\ z_8 \mathbf{a}_3 \end{matrix} = ax_8 \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}} & (16o) & \text{O VI} \\
\mathbf{B}_{33} &= \begin{matrix} -(x_8 - y_8) \mathbf{a}_1 - (x_8 + y_8) \mathbf{a}_2 - \\ z_8 \mathbf{a}_3 \end{matrix} = -ax_8 \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}} & (16o) & \text{O VI} \\
\mathbf{B}_{34} &= \begin{matrix} (x_8 - y_8 + \frac{1}{2}) \mathbf{a}_1 + \\ (x_8 + y_8 + \frac{1}{2}) \mathbf{a}_2 - z_8 \mathbf{a}_3 \end{matrix} = a(x_8 + \frac{1}{2}) \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}} & (16o) & \text{O VI} \\
\mathbf{B}_{35} &= \begin{matrix} (x_8 + y_8 + \frac{1}{2}) \mathbf{a}_1 + \\ (x_8 - y_8 + \frac{1}{2}) \mathbf{a}_2 + z_8 \mathbf{a}_3 \end{matrix} = a(x_8 + \frac{1}{2}) \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}} & (16o) & \text{O VI} \\
\mathbf{B}_{36} &= \begin{matrix} -(x_8 + y_8) \mathbf{a}_1 - (x_8 - y_8) \mathbf{a}_2 + \\ z_8 \mathbf{a}_3 \end{matrix} = -ax_8 \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}} & (16o) & \text{O VI}
\end{aligned}$$

References

- [1] J. W. Richardson, J. V. Smith, and J. J. Pluth, *AlPO₄-25: framework topology, topotactic transformation from AlPO₄-21, and high-low displacive transition*, J. Phys. Chem. **94**, 3365–3367 (1990), doi:10.1021/j100372a002.

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