

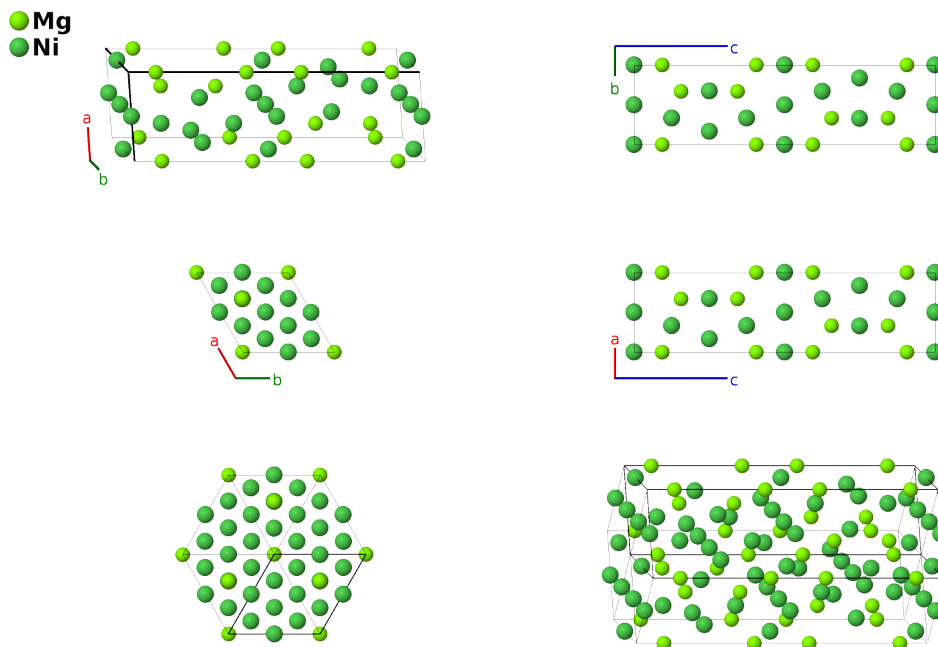
MgNi₂ Hexagonal Laves (C36) Structure: AB2_hP24_194_ef_fgh-001

This structure originally had the label AB2_hP24_194_ef_fgh. Calls to that address will be redirected here.

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<https://aflow.org/p/HV5V>

https://aflow.org/p/AB2_hP24_194_ef_fgh-001



Prototype	MgNi ₂
AFLOW prototype label	AB2_hP24_194_ef_fgh-001
Strukturbericht designation	C36
ICSD	104838
Pearson symbol	hP24
Space group number	194
Space group symbol	<i>P</i> 6 ₃ / <i>mmc</i>
AFLOW prototype command	<code>aflow --proto=AB2_hP24_194_ef_fgh-001 --params=a, c/a, z₁, z₂, z₃, x₅</code>

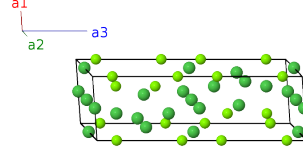
Other compounds with this structure

CdCu₂, HfCr₂, HfFe₂, HfMo₂ (HT), NbCo₂, NbZn₂, ScFe₂, ThMg₂ (LT), β -TiCo₂, UPt₂

- An AFLOW user, Mehdi Noori, identified an inconsistency with this entry and the original reference (Mehl, 2017): the z-value for Mg (I) 4e should have been 0.09400, not 0.04598. This entry has been corrected.

Hexagonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{2}a\hat{\mathbf{y}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{2}a\hat{\mathbf{y}} \\ \mathbf{a}_3 &= c\hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= z_1 \mathbf{a}_3$	$=$	$cz_1 \hat{\mathbf{z}}$	(4e)	Mg I
\mathbf{B}_2	$= (z_1 + \frac{1}{2}) \mathbf{a}_3$	$=$	$c(z_1 + \frac{1}{2}) \hat{\mathbf{z}}$	(4e)	Mg I
\mathbf{B}_3	$= -z_1 \mathbf{a}_3$	$=$	$-cz_1 \hat{\mathbf{z}}$	(4e)	Mg I
\mathbf{B}_4	$= -(z_1 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-c(z_1 - \frac{1}{2}) \hat{\mathbf{z}}$	(4e)	Mg I
\mathbf{B}_5	$= \frac{1}{3} \mathbf{a}_1 + \frac{2}{3} \mathbf{a}_2 + z_2 \mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} + cz_2\hat{\mathbf{z}}$	(4f)	Mg II
\mathbf{B}_6	$= \frac{2}{3} \mathbf{a}_1 + \frac{1}{3} \mathbf{a}_2 + (z_2 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} + c(z_2 + \frac{1}{2})\hat{\mathbf{z}}$	(4f)	Mg II
\mathbf{B}_7	$= \frac{2}{3} \mathbf{a}_1 + \frac{1}{3} \mathbf{a}_2 - z_2 \mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} - cz_2\hat{\mathbf{z}}$	(4f)	Mg II
\mathbf{B}_8	$= \frac{1}{3} \mathbf{a}_1 + \frac{2}{3} \mathbf{a}_2 - (z_2 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} - c(z_2 - \frac{1}{2})\hat{\mathbf{z}}$	(4f)	Mg II
\mathbf{B}_9	$= \frac{1}{3} \mathbf{a}_1 + \frac{2}{3} \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} + cz_3\hat{\mathbf{z}}$	(4f)	Ni I
\mathbf{B}_{10}	$= \frac{2}{3} \mathbf{a}_1 + \frac{1}{3} \mathbf{a}_2 + (z_3 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} + c(z_3 + \frac{1}{2})\hat{\mathbf{z}}$	(4f)	Ni I
\mathbf{B}_{11}	$= \frac{2}{3} \mathbf{a}_1 + \frac{1}{3} \mathbf{a}_2 - z_3 \mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} - cz_3\hat{\mathbf{z}}$	(4f)	Ni I
\mathbf{B}_{12}	$= \frac{1}{3} \mathbf{a}_1 + \frac{2}{3} \mathbf{a}_2 - (z_3 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} - c(z_3 - \frac{1}{2})\hat{\mathbf{z}}$	(4f)	Ni I
\mathbf{B}_{13}	$= \frac{1}{2} \mathbf{a}_1$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{4}a\hat{\mathbf{y}}$	(6g)	Ni II
\mathbf{B}_{14}	$= \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{4}a\hat{\mathbf{y}}$	(6g)	Ni II
\mathbf{B}_{15}	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2}a\hat{\mathbf{x}}$	(6g)	Ni II
\mathbf{B}_{16}	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{4}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$	(6g)	Ni II
\mathbf{B}_{17}	$= \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{4}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$	(6g)	Ni II
\mathbf{B}_{18}	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}c\hat{\mathbf{z}}$	(6g)	Ni II
\mathbf{B}_{19}	$= x_5 \mathbf{a}_1 + 2x_5 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{3}{2}ax_5\hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_5\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(6h)	Ni III
\mathbf{B}_{20}	$= -2x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$-\frac{3}{2}ax_5\hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_5\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(6h)	Ni III
\mathbf{B}_{21}	$= x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$-\sqrt{3}ax_5\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(6h)	Ni III
\mathbf{B}_{22}	$= -x_5 \mathbf{a}_1 - 2x_5 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$-\frac{3}{2}ax_5\hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_5\hat{\mathbf{y}} + \frac{3}{4}c\hat{\mathbf{z}}$	(6h)	Ni III
\mathbf{B}_{23}	$= 2x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{3}{2}ax_5\hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_5\hat{\mathbf{y}} + \frac{3}{4}c\hat{\mathbf{z}}$	(6h)	Ni III
\mathbf{B}_{24}	$= -x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\sqrt{3}ax_5\hat{\mathbf{y}} + \frac{3}{4}c\hat{\mathbf{z}}$	(6h)	Ni III

References

- [1] Y. Komura and K. Tokunaga, *Structural studies of stacking variants in Mg-base Friauf-Laves phases*, Acta Crystallogr. Sect. B **36**, 1548–1554 (1980), doi:10.1107/S0567740880006565.
- [2] M. J. Mehl, D. Hicks, C. Toher, O. Levy, R. M. Hanson, G. Hart, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 1*, Comput. Mater. Sci. **136**, S1–S828 (2017), doi:10.1016/j.commatsci.2017.01.017.