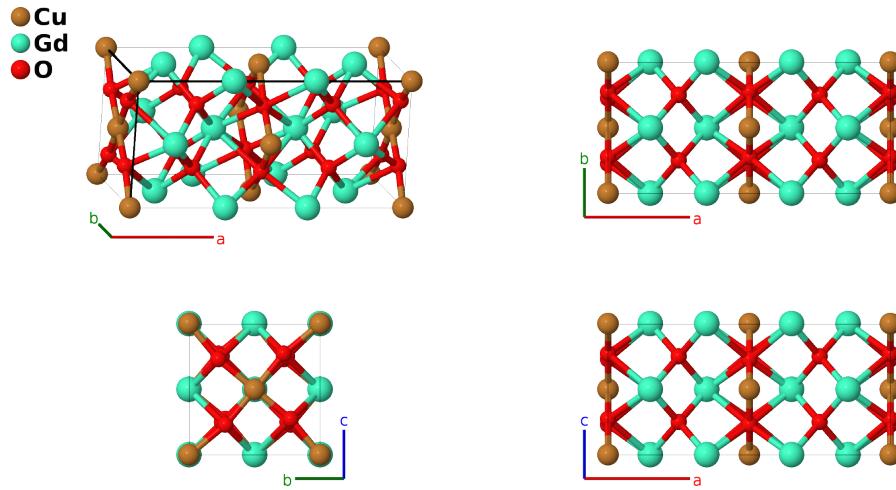


Gd₂CuO₄ Structure: AB2C4_oC28_64_a_d_ef-001

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<https://aflow.org/p/UBCB>

https://aflow.org/p/AB2C4_oC28_64_a_d_ef-001



Prototype CuGd₂O₄

AFLOW prototype label AB2C4_oC28_64_a_d_ef-001

ICSD 75425

Pearson symbol oC28

Space group number 64

Space group symbol *Cmce*

AFLOW prototype command `aflow --proto=AB2C4_oC28_64_a_d_ef-001
--params=a, b/a, c/a, x2, y3, y4, z4`

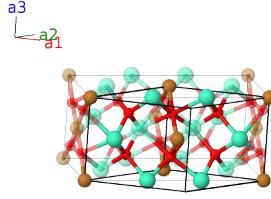
Other compounds with this structure

Eu₂CuO₄

- This is a slight orthorhombic distortion of the Nd₂CuO₄ structure, and there is some evidence that both Gd₂CuO₄ and Eu₂CuO₄ transform to the Nd₂CuO₄ structure at higher temperatures.
- We did not find an ICSD from (Luo, 1999), so we use the one from the earlier work of (Braden, 1994).

Base-centered Orthorhombic primitive vectors

$$\begin{aligned}
\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}b\hat{\mathbf{y}} \\
\mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}} \\
\mathbf{a}_3 &= c\hat{\mathbf{z}}
\end{aligned}$$



Basis vectors

	Lattice coordinates	Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	= 0	= 0	(4a)	Cu I
\mathbf{B}_2	= $\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	= $\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}c\hat{\mathbf{z}}$	(4a)	Cu I
\mathbf{B}_3	= $x_2\mathbf{a}_1 + x_2\mathbf{a}_2$	= $ax_2\hat{\mathbf{x}}$	(8d)	Gd I
\mathbf{B}_4	= $-(x_2 - \frac{1}{2})\mathbf{a}_1 - (x_2 - \frac{1}{2})\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	= $-a(x_2 - \frac{1}{2})\hat{\mathbf{x}} + \frac{1}{2}c\hat{\mathbf{z}}$	(8d)	Gd I
\mathbf{B}_5	= $-x_2\mathbf{a}_1 - x_2\mathbf{a}_2$	= $-ax_2\hat{\mathbf{x}}$	(8d)	Gd I
\mathbf{B}_6	= $(x_2 + \frac{1}{2})\mathbf{a}_1 + (x_2 + \frac{1}{2})\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	= $a(x_2 + \frac{1}{2})\hat{\mathbf{x}} + \frac{1}{2}c\hat{\mathbf{z}}$	(8d)	Gd I
\mathbf{B}_7	= $-(y_3 - \frac{1}{4})\mathbf{a}_1 + (y_3 + \frac{1}{4})\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$	= $\frac{1}{4}a\hat{\mathbf{x}} + by_3\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(8e)	O I
\mathbf{B}_8	= $(y_3 + \frac{1}{4})\mathbf{a}_1 - (y_3 - \frac{1}{4})\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$	= $\frac{1}{4}a\hat{\mathbf{x}} - by_3\hat{\mathbf{y}} + \frac{3}{4}c\hat{\mathbf{z}}$	(8e)	O I
\mathbf{B}_9	= $(y_3 + \frac{3}{4})\mathbf{a}_1 - (y_3 - \frac{3}{4})\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$	= $\frac{3}{4}a\hat{\mathbf{x}} - by_3\hat{\mathbf{y}} + \frac{3}{4}c\hat{\mathbf{z}}$	(8e)	O I
\mathbf{B}_{10}	= $-(y_3 - \frac{3}{4})\mathbf{a}_1 + (y_3 + \frac{3}{4})\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$	= $\frac{3}{4}a\hat{\mathbf{x}} + by_3\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(8e)	O I
\mathbf{B}_{11}	= $-y_4\mathbf{a}_1 + y_4\mathbf{a}_2 + z_4\mathbf{a}_3$	= $by_4\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(8f)	O II
\mathbf{B}_{12}	= $(y_4 + \frac{1}{2})\mathbf{a}_1 - (y_4 - \frac{1}{2})\mathbf{a}_2 + (z_4 + \frac{1}{2})\mathbf{a}_3$	= $\frac{1}{2}a\hat{\mathbf{x}} - by_4\hat{\mathbf{y}} + c(z_4 + \frac{1}{2})\hat{\mathbf{z}}$	(8f)	O II
\mathbf{B}_{13}	= $-(y_4 - \frac{1}{2})\mathbf{a}_1 + (y_4 + \frac{1}{2})\mathbf{a}_2 - (z_4 - \frac{1}{2})\mathbf{a}_3$	= $\frac{1}{2}a\hat{\mathbf{x}} + by_4\hat{\mathbf{y}} - c(z_4 - \frac{1}{2})\hat{\mathbf{z}}$	(8f)	O II
\mathbf{B}_{14}	= $y_4\mathbf{a}_1 - y_4\mathbf{a}_2 - z_4\mathbf{a}_3$	= $-by_4\hat{\mathbf{y}} - cz_4\hat{\mathbf{z}}$	(8f)	O II

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