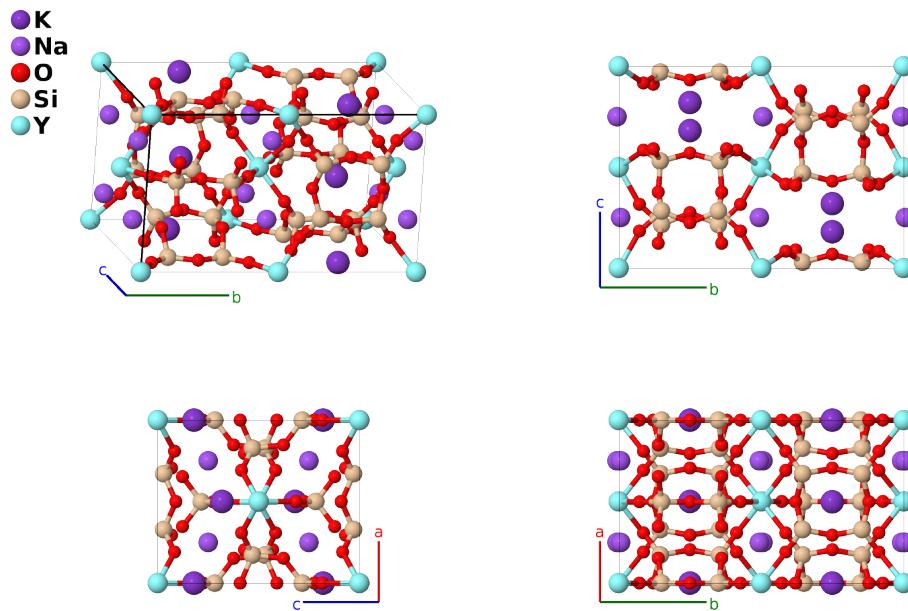


Moskvinit (Na₂KYSi₆O₁₅) Structure: AB₂C₁₅D₆E_oI100_74_e_g_e2hi2j_hj_a-001

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<https://aflow.org/p/F0JR>

https://aflow.org/p/AB2C15D6E_oI100_74_e_g_e2hi2j_hj_a-001

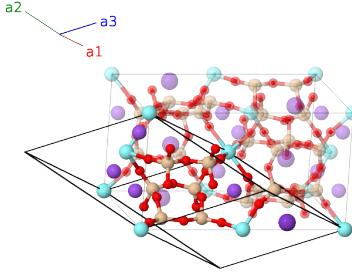


Prototype	KNa ₂ O ₁₅ Si ₆ Y
AFLOW prototype label	AB ₂ C ₁₅ D ₆ E_oI100_74_e_g_e2hi2j_hj_a-001
Mineral name	moskvinit
ICSD	97289
Pearson symbol	oI100
Space group number	74
Space group symbol	<i>Imma</i>
AFLOW prototype command	<pre>aflow --proto=AB2C15D6E_oI100_74_e_g_e2hi2j_hj_a-001 --params=a,b/a,c/a,z₂,z₃,y₄,y₅,z₅,y₆,z₆,y₇,z₇,x₈,z₈,x₉,y₉,z₉,x₁₀,y₁₀,z₁₀,x₁₁, y₁₁,z₁₁</pre>

- This is technically named moskvinit-(Y). The yttrium on the (4a) site can be replaced rare-earth elements. The composition of this sample is actually Na_{2.06}K_{0.95}(Y_{0.77}Dy_{0.09}Gd_{0.04}Er_{0.04}Ho_{0.02}Sm_{0.02}Nd_{0.01}Tb_{0.01})_{Σ1.00}Si₆O₁₅.
- (Sokolova, 2003) give the data for this structure in the *Ibmm* setting of space group #74. We used FINDSYM to shift this to the standard *Imma* setting. This involved rotation of the axes and shifting the Y-I atom from (1/4 1/4 1/4) to the origin.

Body-centered Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}} - \frac{1}{2}c\hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates	=	Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	0	=	0	(4a)	Y I
\mathbf{B}_2	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{2}b\hat{\mathbf{y}}$	(4a)	Y I
\mathbf{B}_3	$(z_2 + \frac{1}{4})\mathbf{a}_1 + z_2\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$	=	$\frac{1}{4}b\hat{\mathbf{y}} + cz_2\hat{\mathbf{z}}$	(4e)	K I
\mathbf{B}_4	$-(z_2 - \frac{3}{4})\mathbf{a}_1 - z_2\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$	=	$\frac{3}{4}b\hat{\mathbf{y}} - cz_2\hat{\mathbf{z}}$	(4e)	K I
\mathbf{B}_5	$(z_3 + \frac{1}{4})\mathbf{a}_1 + z_3\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$	=	$\frac{1}{4}b\hat{\mathbf{y}} + cz_3\hat{\mathbf{z}}$	(4e)	O I
\mathbf{B}_6	$-(z_3 - \frac{3}{4})\mathbf{a}_1 - z_3\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$	=	$\frac{3}{4}b\hat{\mathbf{y}} - cz_3\hat{\mathbf{z}}$	(4e)	O I
\mathbf{B}_7	$(y_4 + \frac{1}{4})\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2 + (y_4 + \frac{1}{4})\mathbf{a}_3$	=	$\frac{1}{4}a\hat{\mathbf{x}} + by_4\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(8g)	Na I
\mathbf{B}_8	$-(y_4 - \frac{3}{4})\mathbf{a}_1 - (y_4 - \frac{1}{4})\mathbf{a}_3$	=	$-\frac{1}{4}a\hat{\mathbf{x}} - b(y_4 - \frac{1}{2})\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(8g)	Na I
\mathbf{B}_9	$-(y_4 - \frac{3}{4})\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2 - (y_4 - \frac{3}{4})\mathbf{a}_3$	=	$\frac{1}{4}a\hat{\mathbf{x}} - b(y_4 - \frac{1}{2})\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(8g)	Na I
\mathbf{B}_{10}	$(y_4 + \frac{1}{4})\mathbf{a}_1 + (y_4 + \frac{3}{4})\mathbf{a}_3$	=	$\frac{1}{4}a\hat{\mathbf{x}} + b(y_4 + \frac{1}{2})\hat{\mathbf{y}} - \frac{1}{4}c\hat{\mathbf{z}}$	(8g)	Na I
\mathbf{B}_{11}	$(y_5 + z_5)\mathbf{a}_1 + z_5\mathbf{a}_2 + y_5\mathbf{a}_3$	=	$by_5\hat{\mathbf{y}} + cz_5\hat{\mathbf{z}}$	(8h)	O II
\mathbf{B}_{12}	$(-y_5 + z_5 + \frac{1}{2})\mathbf{a}_1 + z_5\mathbf{a}_2 - (y_5 - \frac{1}{2})\mathbf{a}_3$	=	$-b(y_5 - \frac{1}{2})\hat{\mathbf{y}} + cz_5\hat{\mathbf{z}}$	(8h)	O II
\mathbf{B}_{13}	$(y_5 - z_5 + \frac{1}{2})\mathbf{a}_1 - z_5\mathbf{a}_2 + (y_5 + \frac{1}{2})\mathbf{a}_3$	=	$b(y_5 + \frac{1}{2})\hat{\mathbf{y}} - cz_5\hat{\mathbf{z}}$	(8h)	O II
\mathbf{B}_{14}	$-(y_5 + z_5)\mathbf{a}_1 - z_5\mathbf{a}_2 - y_5\mathbf{a}_3$	=	$-by_5\hat{\mathbf{y}} - cz_5\hat{\mathbf{z}}$	(8h)	O II
\mathbf{B}_{15}	$(y_6 + z_6)\mathbf{a}_1 + z_6\mathbf{a}_2 + y_6\mathbf{a}_3$	=	$by_6\hat{\mathbf{y}} + cz_6\hat{\mathbf{z}}$	(8h)	O III
\mathbf{B}_{16}	$(-y_6 + z_6 + \frac{1}{2})\mathbf{a}_1 + z_6\mathbf{a}_2 - (y_6 - \frac{1}{2})\mathbf{a}_3$	=	$-b(y_6 - \frac{1}{2})\hat{\mathbf{y}} + cz_6\hat{\mathbf{z}}$	(8h)	O III
\mathbf{B}_{17}	$(y_6 - z_6 + \frac{1}{2})\mathbf{a}_1 - z_6\mathbf{a}_2 + (y_6 + \frac{1}{2})\mathbf{a}_3$	=	$b(y_6 + \frac{1}{2})\hat{\mathbf{y}} - cz_6\hat{\mathbf{z}}$	(8h)	O III
\mathbf{B}_{18}	$-(y_6 + z_6)\mathbf{a}_1 - z_6\mathbf{a}_2 - y_6\mathbf{a}_3$	=	$-by_6\hat{\mathbf{y}} - cz_6\hat{\mathbf{z}}$	(8h)	O III
\mathbf{B}_{19}	$(y_7 + z_7)\mathbf{a}_1 + z_7\mathbf{a}_2 + y_7\mathbf{a}_3$	=	$by_7\hat{\mathbf{y}} + cz_7\hat{\mathbf{z}}$	(8h)	Si I
\mathbf{B}_{20}	$(-y_7 + z_7 + \frac{1}{2})\mathbf{a}_1 + z_7\mathbf{a}_2 - (y_7 - \frac{1}{2})\mathbf{a}_3$	=	$-b(y_7 - \frac{1}{2})\hat{\mathbf{y}} + cz_7\hat{\mathbf{z}}$	(8h)	Si I
\mathbf{B}_{21}	$(y_7 - z_7 + \frac{1}{2})\mathbf{a}_1 - z_7\mathbf{a}_2 + (y_7 + \frac{1}{2})\mathbf{a}_3$	=	$b(y_7 + \frac{1}{2})\hat{\mathbf{y}} - cz_7\hat{\mathbf{z}}$	(8h)	Si I
\mathbf{B}_{22}	$-(y_7 + z_7)\mathbf{a}_1 - z_7\mathbf{a}_2 - y_7\mathbf{a}_3$	=	$-by_7\hat{\mathbf{y}} - cz_7\hat{\mathbf{z}}$	(8h)	Si I
\mathbf{B}_{23}	$(z_8 + \frac{1}{4})\mathbf{a}_1 + (x_8 + z_8)\mathbf{a}_2 + (x_8 + \frac{1}{4})\mathbf{a}_3$	=	$ax_8\hat{\mathbf{x}} + \frac{1}{4}b\hat{\mathbf{y}} + cz_8\hat{\mathbf{z}}$	(8i)	O IV

\mathbf{B}_{24}	$=$	$(z_8 + \frac{1}{4}) \mathbf{a}_1 - (x_8 - z_8) \mathbf{a}_2 -$ $(x_8 - \frac{1}{4}) \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} + \frac{1}{4}b \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(8i)	O IV
\mathbf{B}_{25}	$=$	$-(z_8 - \frac{3}{4}) \mathbf{a}_1 - (x_8 + z_8) \mathbf{a}_2 -$ $(x_8 - \frac{3}{4}) \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} + \frac{3}{4}b \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	(8i)	O IV
\mathbf{B}_{26}	$=$	$-(z_8 - \frac{3}{4}) \mathbf{a}_1 + (x_8 - z_8) \mathbf{a}_2 +$ $(x_8 + \frac{3}{4}) \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} + \frac{3}{4}b \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	(8i)	O IV
\mathbf{B}_{27}	$=$	$(y_9 + z_9) \mathbf{a}_1 + (x_9 + z_9) \mathbf{a}_2 +$ $(x_9 + y_9) \mathbf{a}_3$	$=$	$ax_9 \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(16j)	O V
\mathbf{B}_{28}	$=$	$(-y_9 + z_9 + \frac{1}{2}) \mathbf{a}_1 -$ $(x_9 - z_9) \mathbf{a}_2 - (x_9 + y_9 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-ax_9 \hat{\mathbf{x}} - b(y_9 - \frac{1}{2}) \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(16j)	O V
\mathbf{B}_{29}	$=$	$(y_9 - z_9 + \frac{1}{2}) \mathbf{a}_1 - (x_9 + z_9) \mathbf{a}_2 +$ $(-x_9 + y_9 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-ax_9 \hat{\mathbf{x}} + b(y_9 + \frac{1}{2}) \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}}$	(16j)	O V
\mathbf{B}_{30}	$=$	$-(y_9 + z_9) \mathbf{a}_1 + (x_9 - z_9) \mathbf{a}_2 +$ $(x_9 - y_9) \mathbf{a}_3$	$=$	$ax_9 \hat{\mathbf{x}} - by_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}}$	(16j)	O V
\mathbf{B}_{31}	$=$	$-(y_9 + z_9) \mathbf{a}_1 - (x_9 + z_9) \mathbf{a}_2 -$ $(x_9 + y_9) \mathbf{a}_3$	$=$	$-ax_9 \hat{\mathbf{x}} - by_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}}$	(16j)	O V
\mathbf{B}_{32}	$=$	$(y_9 - z_9 + \frac{1}{2}) \mathbf{a}_1 +$ $(x_9 - z_9) \mathbf{a}_2 + (x_9 + y_9 + \frac{1}{2}) \mathbf{a}_3$	$=$	$ax_9 \hat{\mathbf{x}} + b(y_9 + \frac{1}{2}) \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}}$	(16j)	O V
\mathbf{B}_{33}	$=$	$(-y_9 + z_9 + \frac{1}{2}) \mathbf{a}_1 +$ $(x_9 + z_9) \mathbf{a}_2 + (x_9 - y_9 + \frac{1}{2}) \mathbf{a}_3$	$=$	$ax_9 \hat{\mathbf{x}} - b(y_9 - \frac{1}{2}) \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(16j)	O V
\mathbf{B}_{34}	$=$	$(y_9 + z_9) \mathbf{a}_1 - (x_9 - z_9) \mathbf{a}_2 -$ $(x_9 - y_9) \mathbf{a}_3$	$=$	$-ax_9 \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(16j)	O V
\mathbf{B}_{35}	$=$	$(y_{10} + z_{10}) \mathbf{a}_1 + (x_{10} + z_{10}) \mathbf{a}_2 +$ $(x_{10} + y_{10}) \mathbf{a}_3$	$=$	$ax_{10} \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}}$	(16j)	O VI
\mathbf{B}_{36}	$=$	$(-y_{10} + z_{10} + \frac{1}{2}) \mathbf{a}_1 -$ $(x_{10} - z_{10}) \mathbf{a}_2 -$ $(x_{10} + y_{10} - \frac{1}{2}) \mathbf{a}_3$	$=$	$-ax_{10} \hat{\mathbf{x}} - b(y_{10} - \frac{1}{2}) \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}}$	(16j)	O VI
\mathbf{B}_{37}	$=$	$(y_{10} - z_{10} + \frac{1}{2}) \mathbf{a}_1 -$ $(x_{10} + z_{10}) \mathbf{a}_2 +$ $(-x_{10} + y_{10} + \frac{1}{2}) \mathbf{a}_3$	$=$	$-ax_{10} \hat{\mathbf{x}} + b(y_{10} + \frac{1}{2}) \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}}$	(16j)	O VI
\mathbf{B}_{38}	$=$	$-(y_{10} + z_{10}) \mathbf{a}_1 +$ $(x_{10} - z_{10}) \mathbf{a}_2 + (x_{10} - y_{10}) \mathbf{a}_3$	$=$	$ax_{10} \hat{\mathbf{x}} - by_{10} \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}}$	(16j)	O VI
\mathbf{B}_{39}	$=$	$-(y_{10} + z_{10}) \mathbf{a}_1 -$ $(x_{10} + z_{10}) \mathbf{a}_2 - (x_{10} + y_{10}) \mathbf{a}_3$	$=$	$-ax_{10} \hat{\mathbf{x}} - by_{10} \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}}$	(16j)	O VI
\mathbf{B}_{40}	$=$	$(y_{10} - z_{10} + \frac{1}{2}) \mathbf{a}_1 +$ $(x_{10} - z_{10}) \mathbf{a}_2 +$ $(x_{10} + y_{10} + \frac{1}{2}) \mathbf{a}_3$	$=$	$ax_{10} \hat{\mathbf{x}} + b(y_{10} + \frac{1}{2}) \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}}$	(16j)	O VI
\mathbf{B}_{41}	$=$	$(-y_{10} + z_{10} + \frac{1}{2}) \mathbf{a}_1 +$ $(x_{10} + z_{10}) \mathbf{a}_2 +$ $(x_{10} - y_{10} + \frac{1}{2}) \mathbf{a}_3$	$=$	$ax_{10} \hat{\mathbf{x}} - b(y_{10} - \frac{1}{2}) \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}}$	(16j)	O VI
\mathbf{B}_{42}	$=$	$(y_{10} + z_{10}) \mathbf{a}_1 - (x_{10} - z_{10}) \mathbf{a}_2 -$ $(x_{10} - y_{10}) \mathbf{a}_3$	$=$	$-ax_{10} \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}}$	(16j)	O VI
\mathbf{B}_{43}	$=$	$(y_{11} + z_{11}) \mathbf{a}_1 + (x_{11} + z_{11}) \mathbf{a}_2 +$ $(x_{11} + y_{11}) \mathbf{a}_3$	$=$	$ax_{11} \hat{\mathbf{x}} + by_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}}$	(16j)	Si II
\mathbf{B}_{44}	$=$	$(-y_{11} + z_{11} + \frac{1}{2}) \mathbf{a}_1 -$ $(x_{11} - z_{11}) \mathbf{a}_2 -$ $(x_{11} + y_{11} - \frac{1}{2}) \mathbf{a}_3$	$=$	$-ax_{11} \hat{\mathbf{x}} - b(y_{11} - \frac{1}{2}) \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}}$	(16j)	Si II

$$\begin{aligned}
\mathbf{B}_{45} &= \left(y_{11} - z_{11} + \frac{1}{2} \right) \mathbf{a}_1 - \left(x_{11} + z_{11} \right) \mathbf{a}_2 + \left(-x_{11} + y_{11} + \frac{1}{2} \right) \mathbf{a}_3 & = & -ax_{11} \hat{\mathbf{x}} + b \left(y_{11} + \frac{1}{2} \right) \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} & (16j) & \text{Si II} \\
\mathbf{B}_{46} &= - \left(y_{11} + z_{11} \right) \mathbf{a}_1 + \left(x_{11} - z_{11} \right) \mathbf{a}_2 + \left(x_{11} - y_{11} \right) \mathbf{a}_3 & = & ax_{11} \hat{\mathbf{x}} - by_{11} \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} & (16j) & \text{Si II} \\
\mathbf{B}_{47} &= - \left(y_{11} + z_{11} \right) \mathbf{a}_1 - \left(x_{11} + z_{11} \right) \mathbf{a}_2 - \left(x_{11} + y_{11} \right) \mathbf{a}_3 & = & -ax_{11} \hat{\mathbf{x}} - by_{11} \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} & (16j) & \text{Si II} \\
\mathbf{B}_{48} &= \left(y_{11} - z_{11} + \frac{1}{2} \right) \mathbf{a}_1 + \left(x_{11} - z_{11} \right) \mathbf{a}_2 + \left(x_{11} + y_{11} + \frac{1}{2} \right) \mathbf{a}_3 & = & ax_{11} \hat{\mathbf{x}} + b \left(y_{11} + \frac{1}{2} \right) \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} & (16j) & \text{Si II} \\
\mathbf{B}_{49} &= \left(-y_{11} + z_{11} + \frac{1}{2} \right) \mathbf{a}_1 + \left(x_{11} + z_{11} \right) \mathbf{a}_2 + \left(x_{11} - y_{11} + \frac{1}{2} \right) \mathbf{a}_3 & = & ax_{11} \hat{\mathbf{x}} - b \left(y_{11} - \frac{1}{2} \right) \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} & (16j) & \text{Si II} \\
\mathbf{B}_{50} &= \left(y_{11} + z_{11} \right) \mathbf{a}_1 - \left(x_{11} - z_{11} \right) \mathbf{a}_2 - \left(x_{11} - y_{11} \right) \mathbf{a}_3 & = & -ax_{11} \hat{\mathbf{x}} + by_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} & (16j) & \text{Si II}
\end{aligned}$$

References

- [1] E. Sokolova, F. C. Hawthorne, A. A. Agakhanov, and L. A. Pautov, *The crystal structure of Moskvinit-(Y), Na₂K(Y,REE)[Si₆O₁₅], a new silicate mineral with [Si₆O₁₅] three-membered double rings from the Dara-I-Pioz Moraine, Tien-Shan Mountains, Tajikistan*, Can. Mineral. **41**, 513–520 (2003), doi:10.2113/gscanmin.41.2.513.