

NaAlB₁₄ Structure:

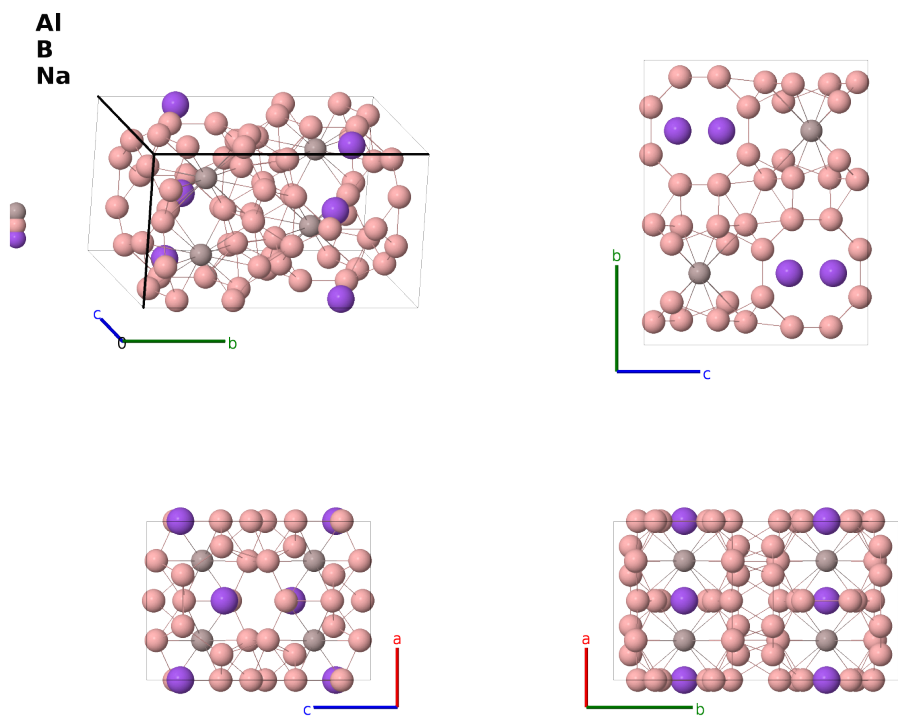
AB14C_oI64_74_c_3h2j_e-001

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- D. Hicks, M. J. Mehl, M. Esters, C. Osos, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/prototype-encyclopedia/XE01>

https://aflow.org/prototype-encyclopedia/AB14C_oI64_74_c_3h2j_e-001

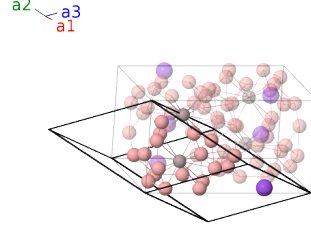


Prototype	AlB ₁₄ Na
AFLOW prototype label	AB14C_oI64_74_c_3h2j_e-001
ICSD	152701
CCDC	1669426
Pearson symbol	oI64
Space group number	74
Space group symbol	<i>Imma</i>
AFLOW prototype command	<code>aflow --proto=AB14C_oI64_74_c_3h2j_e-001</code> <code>--params=a, b/a, c/a, z₂, y₃, z₃, y₄, z₄, y₅, z₅, x₆, y₆, z₆, x₇, y₇, z₇</code>

- The stoichiometry of this sample is given as $\text{Na}_{0.95}\text{Al}_{0.94}\text{B}_{14}$, indicating vacancies on the sodium and aluminum sites.
- (Okada, 2005) say that this is isomorphous to MgAlB_{14} , but our published version of that structure has the Mg site split, rather than a single Na site.
- The AFLOW prototype label protocol swaps the a and b lattice constants, and moves the origin by $1/4 a \hat{x} + 1/4 b \hat{y} + 1/4 c \hat{z}$, moving the aluminum atom from the published (4b) Wyckoff position to (4c).

Body-centered Orthorhombic primitive vectors

$$\begin{aligned} \mathbf{a}_1 &= -\frac{1}{2}a \hat{x} + \frac{1}{2}b \hat{y} + \frac{1}{2}c \hat{z} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{x} - \frac{1}{2}b \hat{y} + \frac{1}{2}c \hat{z} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{x} + \frac{1}{2}b \hat{y} - \frac{1}{2}c \hat{z} \end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{x} + \frac{1}{4}b \hat{y} + \frac{1}{4}c \hat{z}$	(4c)	Al I
$\mathbf{B}_2$	$= \frac{1}{2} \mathbf{a}_1$	$=$	$-\frac{1}{4}a \hat{x} + \frac{1}{4}b \hat{y} + \frac{1}{4}c \hat{z}$	(4c)	Al I
$\mathbf{B}_3$	$= (z_2 + \frac{1}{4}) \mathbf{a}_1 + z_2 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{4}b \hat{y} + cz_2 \hat{z}$	(4e)	Na I
$\mathbf{B}_4$	$= -(z_2 - \frac{3}{4}) \mathbf{a}_1 - z_2 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{3}{4}b \hat{y} - cz_2 \hat{z}$	(4e)	Na I
$\mathbf{B}_5$	$= (y_3 + z_3) \mathbf{a}_1 + z_3 \mathbf{a}_2 + y_3 \mathbf{a}_3$	$=$	$by_3 \hat{y} + cz_3 \hat{z}$	(8h)	B I
$\mathbf{B}_6$	$= (-y_3 + z_3 + \frac{1}{2}) \mathbf{a}_1 + z_3 \mathbf{a}_2 - (y_3 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-b(y_3 - \frac{1}{2}) \hat{y} + cz_3 \hat{z}$	(8h)	B I
$\mathbf{B}_7$	$= (y_3 - z_3 + \frac{1}{2}) \mathbf{a}_1 - z_3 \mathbf{a}_2 + (y_3 + \frac{1}{2}) \mathbf{a}_3$	$=$	$b(y_3 + \frac{1}{2}) \hat{y} - cz_3 \hat{z}$	(8h)	B I
$\mathbf{B}_8$	$= -(y_3 + z_3) \mathbf{a}_1 - z_3 \mathbf{a}_2 - y_3 \mathbf{a}_3$	$=$	$-by_3 \hat{y} - cz_3 \hat{z}$	(8h)	B I
$\mathbf{B}_9$	$= (y_4 + z_4) \mathbf{a}_1 + z_4 \mathbf{a}_2 + y_4 \mathbf{a}_3$	$=$	$by_4 \hat{y} + cz_4 \hat{z}$	(8h)	B II
$\mathbf{B}_{10}$	$= (-y_4 + z_4 + \frac{1}{2}) \mathbf{a}_1 + z_4 \mathbf{a}_2 - (y_4 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-b(y_4 - \frac{1}{2}) \hat{y} + cz_4 \hat{z}$	(8h)	B II
$\mathbf{B}_{11}$	$= (y_4 - z_4 + \frac{1}{2}) \mathbf{a}_1 - z_4 \mathbf{a}_2 + (y_4 + \frac{1}{2}) \mathbf{a}_3$	$=$	$b(y_4 + \frac{1}{2}) \hat{y} - cz_4 \hat{z}$	(8h)	B II
$\mathbf{B}_{12}$	$= -(y_4 + z_4) \mathbf{a}_1 - z_4 \mathbf{a}_2 - y_4 \mathbf{a}_3$	$=$	$-by_4 \hat{y} - cz_4 \hat{z}$	(8h)	B II
$\mathbf{B}_{13}$	$= (y_5 + z_5) \mathbf{a}_1 + z_5 \mathbf{a}_2 + y_5 \mathbf{a}_3$	$=$	$by_5 \hat{y} + cz_5 \hat{z}$	(8h)	B III
$\mathbf{B}_{14}$	$= (-y_5 + z_5 + \frac{1}{2}) \mathbf{a}_1 + z_5 \mathbf{a}_2 - (y_5 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-b(y_5 - \frac{1}{2}) \hat{y} + cz_5 \hat{z}$	(8h)	B III
$\mathbf{B}_{15}$	$= (y_5 - z_5 + \frac{1}{2}) \mathbf{a}_1 - z_5 \mathbf{a}_2 + (y_5 + \frac{1}{2}) \mathbf{a}_3$	$=$	$b(y_5 + \frac{1}{2}) \hat{y} - cz_5 \hat{z}$	(8h)	B III
$\mathbf{B}_{16}$	$= -(y_5 + z_5) \mathbf{a}_1 - z_5 \mathbf{a}_2 - y_5 \mathbf{a}_3$	$=$	$-by_5 \hat{y} - cz_5 \hat{z}$	(8h)	B III
$\mathbf{B}_{17}$	$= (y_6 + z_6) \mathbf{a}_1 + (x_6 + z_6) \mathbf{a}_2 + (x_6 + y_6) \mathbf{a}_3$	$=$	$ax_6 \hat{x} + by_6 \hat{y} + cz_6 \hat{z}$	(16j)	B IV

$$\begin{aligned}
\mathbf{B}_{18} &= \begin{pmatrix} -y_6 + z_6 + \frac{1}{2} \\ x_6 - z_6 \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} x_6 + y_6 - \frac{1}{2} \\ -x_6 + y_6 + \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= & -ax_6 \hat{\mathbf{x}} - b(y_6 - \frac{1}{2}) \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} & (16j) & \text{B IV} \\
\mathbf{B}_{19} &= \begin{pmatrix} y_6 - z_6 + \frac{1}{2} \\ -x_6 + y_6 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} x_6 + z_6 \\ x_6 + y_6 \end{pmatrix} \mathbf{a}_2 + &= & -ax_6 \hat{\mathbf{x}} + b(y_6 + \frac{1}{2}) \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} & (16j) & \text{B IV} \\
\mathbf{B}_{20} &= -\begin{pmatrix} y_6 + z_6 \\ x_6 - y_6 \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} x_6 - z_6 \\ x_6 + y_6 \end{pmatrix} \mathbf{a}_2 + &= & ax_6 \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} & (16j) & \text{B IV} \\
\mathbf{B}_{21} &= -\begin{pmatrix} y_6 + z_6 \\ x_6 + y_6 \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} x_6 + z_6 \\ x_6 + y_6 \end{pmatrix} \mathbf{a}_2 - &= & -ax_6 \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} & (16j) & \text{B IV} \\
\mathbf{B}_{22} &= \begin{pmatrix} y_6 - z_6 + \frac{1}{2} \\ x_6 - z_6 \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} x_6 + y_6 + \frac{1}{2} \\ x_6 + y_6 + \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= & ax_6 \hat{\mathbf{x}} + b(y_6 + \frac{1}{2}) \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} & (16j) & \text{B IV} \\
\mathbf{B}_{23} &= \begin{pmatrix} -y_6 + z_6 + \frac{1}{2} \\ x_6 + z_6 \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} x_6 - y_6 + \frac{1}{2} \\ x_6 - y_6 + \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= & ax_6 \hat{\mathbf{x}} - b(y_6 - \frac{1}{2}) \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} & (16j) & \text{B IV} \\
\mathbf{B}_{24} &= \begin{pmatrix} y_6 + z_6 \\ x_6 - y_6 \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} x_6 - z_6 \\ x_6 - y_6 \end{pmatrix} \mathbf{a}_2 - &= & -ax_6 \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} & (16j) & \text{B IV} \\
\mathbf{B}_{25} &= \begin{pmatrix} y_7 + z_7 \\ x_7 + y_7 \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} x_7 + z_7 \\ x_7 + y_7 \end{pmatrix} \mathbf{a}_2 + &= & ax_7 \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (16j) & \text{B V} \\
\mathbf{B}_{26} &= \begin{pmatrix} -y_7 + z_7 + \frac{1}{2} \\ x_7 - z_7 \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} x_7 + y_7 - \frac{1}{2} \\ -x_7 + y_7 + \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= & -ax_7 \hat{\mathbf{x}} - b(y_7 - \frac{1}{2}) \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (16j) & \text{B V} \\
\mathbf{B}_{27} &= \begin{pmatrix} y_7 - z_7 + \frac{1}{2} \\ -x_7 + y_7 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} x_7 + z_7 \\ x_7 + y_7 \end{pmatrix} \mathbf{a}_2 + &= & -ax_7 \hat{\mathbf{x}} + b(y_7 + \frac{1}{2}) \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (16j) & \text{B V} \\
\mathbf{B}_{28} &= -\begin{pmatrix} y_7 + z_7 \\ x_7 - y_7 \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} x_7 - z_7 \\ x_7 - y_7 \end{pmatrix} \mathbf{a}_2 + &= & ax_7 \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (16j) & \text{B V} \\
\mathbf{B}_{29} &= -\begin{pmatrix} y_7 + z_7 \\ x_7 + y_7 \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} x_7 + z_7 \\ x_7 + y_7 \end{pmatrix} \mathbf{a}_2 - &= & -ax_7 \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (16j) & \text{B V} \\
\mathbf{B}_{30} &= \begin{pmatrix} y_7 - z_7 + \frac{1}{2} \\ x_7 - z_7 \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} x_7 + y_7 + \frac{1}{2} \\ x_7 + y_7 + \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= & ax_7 \hat{\mathbf{x}} + b(y_7 + \frac{1}{2}) \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (16j) & \text{B V} \\
\mathbf{B}_{31} &= \begin{pmatrix} -y_7 + z_7 + \frac{1}{2} \\ x_7 + z_7 \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} x_7 - y_7 + \frac{1}{2} \\ x_7 - y_7 + \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= & ax_7 \hat{\mathbf{x}} - b(y_7 - \frac{1}{2}) \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (16j) & \text{B V} \\
\mathbf{B}_{32} &= \begin{pmatrix} y_7 + z_7 \\ x_7 - y_7 \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} x_7 - z_7 \\ x_7 - y_7 \end{pmatrix} \mathbf{a}_2 - &= & -ax_7 \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (16j) & \text{B V}
\end{aligned}$$

References

- [1] S. Okada, T. Tanaka, A. Sato, T. Shishido, K. Kudou, K. Nakajima, and T. Lundström, *Crystal growth and structure refinement of a new higher boride NaAlB₁₄*, J. Alloys Compd. **395**, 231–235 (2005), doi:10.1016/j.jallcom.2004.10.057.

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