

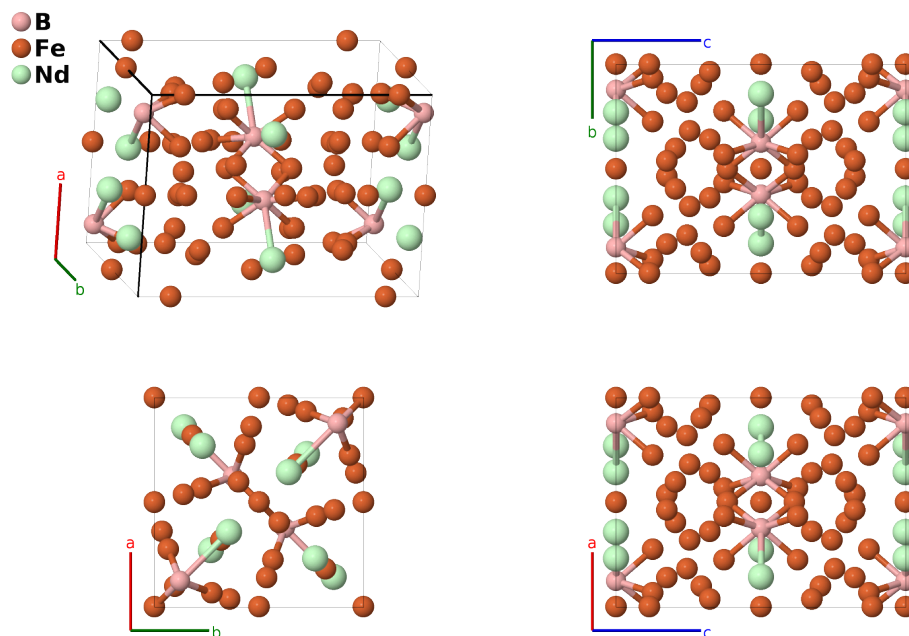
Nd₂Fe₁₄B Structure: AB14C2_tP68_136_f_ce2j2k_fg-001

This structure originally had the label AB14C2.tP68.136.f.ce2j2k.fg. Calls to that address will be redirected here.

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<https://afLOW.org/p/FUR0>

https://afLOW.org/p/AB14C2_tP68_136_f_ce2j2k_fg-001



Prototype	BFe ₁₄ Nd ₂
AFLOW prototype label	AB14C2_tP68_136_f_ce2j2k_fg-001
ICSD	67224
Pearson symbol	tP68
Space group number	136
Space group symbol	$P4_2/mnm$
AFLOW prototype command	<code>afLOW --proto=AB14C2_tP68_136_f_ce2j2k_fg-001 --params=a, c/a, z₂, x₃, x₄, x₅, x₆, z₆, x₇, z₇, x₈, y₈, z₈, x₉, y₉, z₉</code>

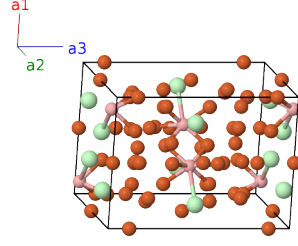
Other compounds with this structure

Gd₂Co₁₄B, Gd₂Co₁₄C, Gd₂Fe₁₄B, Gd₂Fe₁₄C, Ho₂Fe₁₄B, Ho₂Fe₁₄C, La₂Fe₁₄B, La₂Fe₁₄C, Lu₂Fe₁₄B, Lu₂Fe₁₄C, Nd₂Co₁₄B, Pr₂Co₁₄B, Pr₂Fe₁₄B, Pr₂Fe₁₄C, Sm₂Co₁₄B, Sm₂Fe₁₄B, Sm₂Fe₁₄C, Tb₂Co₁₄B, Tb₂Fe₁₄B, Tb₂Fe₁₄C, Th₂Fe₁₄B, Tm₂Fe₁₄B, Tm₂Fe₁₄C, Y₂Co₁₄B, Y₂Fe₁₄B, Gd₂(Co₁₀Mn₄)B, Gd₂(Co₇Fe₇)B, La₂(Co₇Fe₇)B, Nd₂(Co₇Fe₇)B, Pr₂(Co₇Fe₇)B, Tm₂(Fe₁₀Mn₄)B, Y₂(Fe₁₀Mn₄)B, (GdNd)Fe₁₄B, (HoNd)Fe₁₄B, (NdPr)Fe₁₄B, (NdTb)Co₁₄B, (NdTb)Fe₁₄B, (NdY)Co₁₄B, (NdY)Fe₁₄B, (ThY)Fe₁₄B

- In many cases the boron site can be partially occupied with boron or carbon, or have a mixture of boron and carbon.

Simple Tetragonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= a \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2} a \hat{\mathbf{y}}$	(4c)	Fe I
\mathbf{B}_2	$= \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4c)	Fe I
\mathbf{B}_3	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4c)	Fe I
\mathbf{B}_4	$= \frac{1}{2} \mathbf{a}_1$	$=$	$\frac{1}{2} a \hat{\mathbf{x}}$	(4c)	Fe I
\mathbf{B}_5	$= z_2 \mathbf{a}_3$	$=$	$c z_2 \hat{\mathbf{z}}$	(4e)	Fe II
\mathbf{B}_6	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + (z_2 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + c (z_2 + \frac{1}{2}) \hat{\mathbf{z}}$	(4e)	Fe II
\mathbf{B}_7	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 - (z_2 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} - c (z_2 - \frac{1}{2}) \hat{\mathbf{z}}$	(4e)	Fe II
\mathbf{B}_8	$= -z_2 \mathbf{a}_3$	$=$	$-c z_2 \hat{\mathbf{z}}$	(4e)	Fe II
\mathbf{B}_9	$= x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2$	$=$	$a x_3 \hat{\mathbf{x}} + a x_3 \hat{\mathbf{y}}$	(4f)	B I
\mathbf{B}_{10}	$= -x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2$	$=$	$-a x_3 \hat{\mathbf{x}} - a x_3 \hat{\mathbf{y}}$	(4f)	B I
\mathbf{B}_{11}	$= -(x_3 - \frac{1}{2}) \mathbf{a}_1 + (x_3 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-a (x_3 - \frac{1}{2}) \hat{\mathbf{x}} + a (x_3 + \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4f)	B I
\mathbf{B}_{12}	$= (x_3 + \frac{1}{2}) \mathbf{a}_1 - (x_3 - \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$a (x_3 + \frac{1}{2}) \hat{\mathbf{x}} - a (x_3 - \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4f)	B I
\mathbf{B}_{13}	$= x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2$	$=$	$a x_4 \hat{\mathbf{x}} + a x_4 \hat{\mathbf{y}}$	(4f)	Nd I
\mathbf{B}_{14}	$= -x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2$	$=$	$-a x_4 \hat{\mathbf{x}} - a x_4 \hat{\mathbf{y}}$	(4f)	Nd I
\mathbf{B}_{15}	$= -(x_4 - \frac{1}{2}) \mathbf{a}_1 + (x_4 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-a (x_4 - \frac{1}{2}) \hat{\mathbf{x}} + a (x_4 + \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4f)	Nd I
\mathbf{B}_{16}	$= (x_4 + \frac{1}{2}) \mathbf{a}_1 - (x_4 - \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$a (x_4 + \frac{1}{2}) \hat{\mathbf{x}} - a (x_4 - \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4f)	Nd I
\mathbf{B}_{17}	$= x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2$	$=$	$a x_5 \hat{\mathbf{x}} - a x_5 \hat{\mathbf{y}}$	(4g)	Nd II
\mathbf{B}_{18}	$= -x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2$	$=$	$-a x_5 \hat{\mathbf{x}} + a x_5 \hat{\mathbf{y}}$	(4g)	Nd II
\mathbf{B}_{19}	$= (x_5 + \frac{1}{2}) \mathbf{a}_1 + (x_5 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$a (x_5 + \frac{1}{2}) \hat{\mathbf{x}} + a (x_5 + \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4g)	Nd II
\mathbf{B}_{20}	$= -(x_5 - \frac{1}{2}) \mathbf{a}_1 - (x_5 - \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-a (x_5 - \frac{1}{2}) \hat{\mathbf{x}} - a (x_5 - \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4g)	Nd II
\mathbf{B}_{21}	$= x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$a x_6 \hat{\mathbf{x}} + a x_6 \hat{\mathbf{y}} + c z_6 \hat{\mathbf{z}}$	(8j)	Fe III
\mathbf{B}_{22}	$= -x_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$-a x_6 \hat{\mathbf{x}} - a x_6 \hat{\mathbf{y}} + c z_6 \hat{\mathbf{z}}$	(8j)	Fe III
\mathbf{B}_{23}	$= -(x_6 - \frac{1}{2}) \mathbf{a}_1 + (x_6 + \frac{1}{2}) \mathbf{a}_2 + (z_6 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-a (x_6 - \frac{1}{2}) \hat{\mathbf{x}} + a (x_6 + \frac{1}{2}) \hat{\mathbf{y}} + c (z_6 + \frac{1}{2}) \hat{\mathbf{z}}$	(8j)	Fe III
\mathbf{B}_{24}	$= (x_6 + \frac{1}{2}) \mathbf{a}_1 - (x_6 - \frac{1}{2}) \mathbf{a}_2 + (z_6 + \frac{1}{2}) \mathbf{a}_3$	$=$	$a (x_6 + \frac{1}{2}) \hat{\mathbf{x}} - a (x_6 - \frac{1}{2}) \hat{\mathbf{y}} + c (z_6 + \frac{1}{2}) \hat{\mathbf{z}}$	(8j)	Fe III
\mathbf{B}_{25}	$= -(x_6 - \frac{1}{2}) \mathbf{a}_1 + (x_6 + \frac{1}{2}) \mathbf{a}_2 - (z_6 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-a (x_6 - \frac{1}{2}) \hat{\mathbf{x}} + a (x_6 + \frac{1}{2}) \hat{\mathbf{y}} - c (z_6 - \frac{1}{2}) \hat{\mathbf{z}}$	(8j)	Fe III

$$\begin{aligned}
\mathbf{B}_{56} &= \begin{pmatrix} (y_9 + \frac{1}{2}) \mathbf{a}_1 - (x_9 - \frac{1}{2}) \mathbf{a}_2 + \\ (z_9 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = a (y_9 + \frac{1}{2}) \hat{\mathbf{x}} - a (x_9 - \frac{1}{2}) \hat{\mathbf{y}} + c (z_9 + \frac{1}{2}) \hat{\mathbf{z}} & (16k) & \text{Fe VI} \\
\mathbf{B}_{57} &= - \begin{pmatrix} (x_9 - \frac{1}{2}) \mathbf{a}_1 + (y_9 + \frac{1}{2}) \mathbf{a}_2 - \\ (z_9 - \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = -a (x_9 - \frac{1}{2}) \hat{\mathbf{x}} + a (y_9 + \frac{1}{2}) \hat{\mathbf{y}} - c (z_9 - \frac{1}{2}) \hat{\mathbf{z}} & (16k) & \text{Fe VI} \\
\mathbf{B}_{58} &= \begin{pmatrix} (x_9 + \frac{1}{2}) \mathbf{a}_1 - (y_9 - \frac{1}{2}) \mathbf{a}_2 - \\ (z_9 - \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = a (x_9 + \frac{1}{2}) \hat{\mathbf{x}} - a (y_9 - \frac{1}{2}) \hat{\mathbf{y}} - c (z_9 - \frac{1}{2}) \hat{\mathbf{z}} & (16k) & \text{Fe VI} \\
\mathbf{B}_{59} &= y_9 \mathbf{a}_1 + x_9 \mathbf{a}_2 - z_9 \mathbf{a}_3 = ay_9 \hat{\mathbf{x}} + ax_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}} & (16k) & \text{Fe VI} \\
\mathbf{B}_{60} &= -y_9 \mathbf{a}_1 - x_9 \mathbf{a}_2 - z_9 \mathbf{a}_3 = -ay_9 \hat{\mathbf{x}} - ax_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}} & (16k) & \text{Fe VI} \\
\mathbf{B}_{61} &= -x_9 \mathbf{a}_1 - y_9 \mathbf{a}_2 - z_9 \mathbf{a}_3 = -ax_9 \hat{\mathbf{x}} - ay_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}} & (16k) & \text{Fe VI} \\
\mathbf{B}_{62} &= x_9 \mathbf{a}_1 + y_9 \mathbf{a}_2 - z_9 \mathbf{a}_3 = ax_9 \hat{\mathbf{x}} + ay_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}} & (16k) & \text{Fe VI} \\
\mathbf{B}_{63} &= \begin{pmatrix} (y_9 + \frac{1}{2}) \mathbf{a}_1 - (x_9 - \frac{1}{2}) \mathbf{a}_2 - \\ (z_9 - \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = a (y_9 + \frac{1}{2}) \hat{\mathbf{x}} - a (x_9 - \frac{1}{2}) \hat{\mathbf{y}} - c (z_9 - \frac{1}{2}) \hat{\mathbf{z}} & (16k) & \text{Fe VI} \\
\mathbf{B}_{64} &= - \begin{pmatrix} (y_9 - \frac{1}{2}) \mathbf{a}_1 + (x_9 + \frac{1}{2}) \mathbf{a}_2 - \\ (z_9 - \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = -a (y_9 - \frac{1}{2}) \hat{\mathbf{x}} + a (x_9 + \frac{1}{2}) \hat{\mathbf{y}} - c (z_9 - \frac{1}{2}) \hat{\mathbf{z}} & (16k) & \text{Fe VI} \\
\mathbf{B}_{65} &= \begin{pmatrix} (x_9 + \frac{1}{2}) \mathbf{a}_1 - (y_9 - \frac{1}{2}) \mathbf{a}_2 + \\ (z_9 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = a (x_9 + \frac{1}{2}) \hat{\mathbf{x}} - a (y_9 - \frac{1}{2}) \hat{\mathbf{y}} + c (z_9 + \frac{1}{2}) \hat{\mathbf{z}} & (16k) & \text{Fe VI} \\
\mathbf{B}_{66} &= - \begin{pmatrix} (x_9 - \frac{1}{2}) \mathbf{a}_1 + (y_9 + \frac{1}{2}) \mathbf{a}_2 + \\ (z_9 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = -a (x_9 - \frac{1}{2}) \hat{\mathbf{x}} + a (y_9 + \frac{1}{2}) \hat{\mathbf{y}} + c (z_9 + \frac{1}{2}) \hat{\mathbf{z}} & (16k) & \text{Fe VI} \\
\mathbf{B}_{67} &= -y_9 \mathbf{a}_1 - x_9 \mathbf{a}_2 + z_9 \mathbf{a}_3 = -ay_9 \hat{\mathbf{x}} - ax_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}} & (16k) & \text{Fe VI} \\
\mathbf{B}_{68} &= y_9 \mathbf{a}_1 + x_9 \mathbf{a}_2 + z_9 \mathbf{a}_3 = ay_9 \hat{\mathbf{x}} + ax_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}} & (16k) & \text{Fe VI}
\end{aligned}$$

References

- [1] D. Givord, H. S. Li, and J. M. Moreau, *Magnetic properties and crystal structure of Nd₂Fe₁₄B*, Solid State Commun. **50**, 497–499 (1984), doi:10.1016/0038-1098(84)90315-6.