

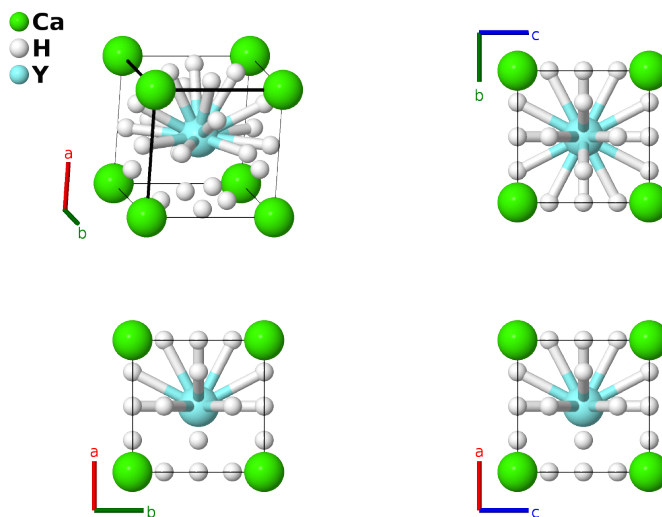
# Predicted High-Pressure YCaH<sub>12</sub> Structure: AB12C\_cP14\_221\_a\_h\_b-001

This structure originally had the label AB12C\_cP14\_221\_a\_h\_b. Calls to that address will be redirected here.

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<https://aflow.org/p/SQ16>

[https://aflow.org/p/AB12C\\_cP14\\_221\\_a\\_h\\_b-001](https://aflow.org/p/AB12C_cP14_221_a_h_b-001)



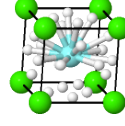
|                         |   |
|-------------------------|---|
| Prototype               | CaH <sub>12</sub> Y   |
| AFLOW prototype label   | AB12C_cP14_221_a_h_b-001  |
| ICSD                    | 686726  |
| Pearson symbol          | cP14  |
| Space group number      | 221   |
| Space group symbol      | $Pm\bar{3}m$  |
| AFLOW prototype command | <code>aflow --proto=AB12C_cP14_221_a_h_b-001<br/>--params=a, x<sub>3</sub></code> |

- This structure was determined by *ab initio* methods and is predicted to be stable in the pressure range 180-257GPa, with  $T_c = 230\text{K}$  at 180GPa. We show the predicted structure at 200GPa.
- The ICSD entry is from the calculations of (Liang, 2019).

## Simple Cubic primitive vectors

a1  
a3  
a2

$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= a \hat{\mathbf{y}} \\ \mathbf{a}_3 &= a \hat{\mathbf{z}}\end{aligned}$$




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## Basis vectors

|                   | Lattice coordinates |  | Cartesian coordinates | Wyckoff position   | Atom type |
|-------------------|---------------------|--|-----------------------|--|-----------|
| $\mathbf{B}_1$    | $=$                 | $0$  | $=$                   | $0$  | (1a) Ca I |
| $\mathbf{B}_2$    | $=$                 | $\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$ | $=$                   | $\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$ | (1b) Y I  |
| $\mathbf{B}_3$    | $=$                 | $x_3 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$                                    | $=$                   | $ax_3 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}}$   | (12h) H I |
| $\mathbf{B}_4$    | $=$                 | $-x_3 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$                                   | $=$                   | $-ax_3 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}}$  | (12h) H I |
| $\mathbf{B}_5$    | $=$                 | $x_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$                                    | $=$                   | $ax_3 \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$   | (12h) H I |
| $\mathbf{B}_6$    | $=$                 | $-x_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$                                   | $=$                   | $-ax_3 \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$  | (12h) H I |
| $\mathbf{B}_7$    | $=$                 | $\frac{1}{2} \mathbf{a}_1 + x_3 \mathbf{a}_3$                                    | $=$                   | $\frac{1}{2} a \hat{\mathbf{x}} + ax_3 \hat{\mathbf{z}}$   | (12h) H I |
| $\mathbf{B}_8$    | $=$                 | $\frac{1}{2} \mathbf{a}_1 - x_3 \mathbf{a}_3$                                    | $=$                   | $\frac{1}{2} a \hat{\mathbf{x}} - ax_3 \hat{\mathbf{z}}$   | (12h) H I |
| $\mathbf{B}_9$    | $=$                 | $\frac{1}{2} \mathbf{a}_1 + x_3 \mathbf{a}_2$                                    | $=$                   | $\frac{1}{2} a \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}}$   | (12h) H I |
| $\mathbf{B}_{10}$ | $=$                 | $\frac{1}{2} \mathbf{a}_1 - x_3 \mathbf{a}_2$                                    | $=$                   | $\frac{1}{2} a \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}}$   | (12h) H I |
| $\mathbf{B}_{11}$ | $=$                 | $x_3 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$                                    | $=$                   | $ax_3 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{z}}$   | (12h) H I |
| $\mathbf{B}_{12}$ | $=$                 | $-x_3 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$                                   | $=$                   | $-ax_3 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{z}}$  | (12h) H I |
| $\mathbf{B}_{13}$ | $=$                 | $\frac{1}{2} \mathbf{a}_2 - x_3 \mathbf{a}_3$                                    | $=$                   | $\frac{1}{2} a \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$   | (12h) H I |
| $\mathbf{B}_{14}$ | $=$                 | $\frac{1}{2} \mathbf{a}_2 + x_3 \mathbf{a}_3$                                    | $=$                   | $\frac{1}{2} a \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$   | (12h) H I |

## References

- [1] H. Xie, D. Duan, Z. Shao, H. Song, Y. Wang, X. Xiao, D. Li, F. Tian, B. Liu, and T. Cui, *High-temperature superconductivity in ternary clathrate  $YCaH_{12}$  under high pressures*, J. Phys.: Condens. Matter **31**, 245404 (2019), doi:10.1088/1361-648X/ab09b4.
- [2] X. Liang, A. Bergara, L. Wang, B. Wen, Z. Zhao, X.-F. Zhou, J. He, G. Gao, and Y. Tian, *Potential high- $T_c$  superconductivity in  $CaYH_{12}$  under pressure*, Phys. Rev. B **99**, 100505(R) (2019), doi:10.1103/PhysRevB.99.100505.