

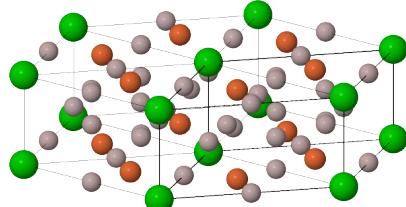
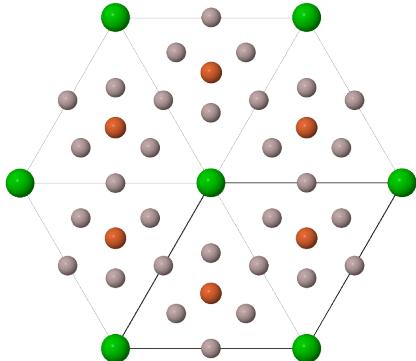
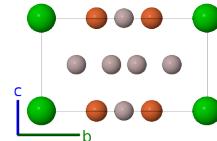
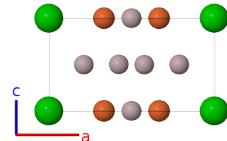
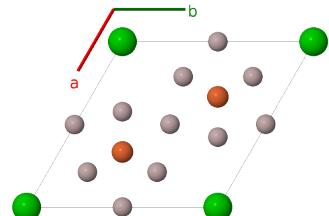
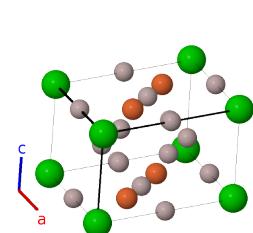
# BaFe<sub>2</sub>Al<sub>9</sub> Structure: A9BC2\_hP12\_191\_fm\_a\_c-001

Cite this page as: H. Eckert, S. Divilov, A. Zettel, M. J. Mehl, D. Hicks, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*. In preparation.

<https://aflow.org/p/CSJ8>

[https://aflow.org/p/A9BC2\\_hP12\\_191\\_fm\\_a\\_c-001](https://aflow.org/p/A9BC2_hP12_191_fm_a_c-001)

● Al  
● Ba  
● Fe



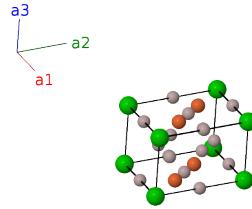
Prototype	Al <sub>9</sub> BaFe <sub>2</sub>
AFLOW prototype label	A9BC2_hP12_191_fm_a_c-001
ICSD	57518
Pearson symbol	hP12
Space group number	191
Space group symbol	$P6/mmm$
AFLOW prototype command	<code>aflow --proto=A9BC2_hP12_191_fm_a_c-001 --params=a, c/a, x4</code>

## Other compounds with this structure

BaFe<sub>2</sub>Al<sub>9</sub>, BaIr<sub>2</sub>In<sub>9</sub>, BaNi<sub>2</sub>Al<sub>9</sub>, CaCo<sub>2</sub>Al<sub>9</sub>, SrCo<sub>2</sub>Al<sub>9</sub>

## Hexagonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{2}a\hat{\mathbf{y}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{2}a\hat{\mathbf{y}} \\ \mathbf{a}_3 &= c\hat{\mathbf{z}}\end{aligned}$$



## Basis vectors

	Lattice coordinates	=	Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	0	=	0	(1a)	Ba I
$\mathbf{B}_2$	$\frac{1}{3}\mathbf{a}_1 + \frac{2}{3}\mathbf{a}_2$	=	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a\hat{\mathbf{y}}$	(2c)	Fe I
$\mathbf{B}_3$	$\frac{2}{3}\mathbf{a}_1 + \frac{1}{3}\mathbf{a}_2$	=	$\frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a\hat{\mathbf{y}}$	(2c)	Fe I
$\mathbf{B}_4$	$\frac{1}{2}\mathbf{a}_1$	=	$\frac{1}{4}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{4}a\hat{\mathbf{y}}$	(3f)	Al I
$\mathbf{B}_5$	$\frac{1}{2}\mathbf{a}_2$	=	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{4}a\hat{\mathbf{y}}$	(3f)	Al I
$\mathbf{B}_6$	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2$	=	$\frac{1}{2}a\hat{\mathbf{x}}$	(3f)	Al I
$\mathbf{B}_7$	$x_4\mathbf{a}_1 + 2x_4\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$\frac{3}{2}ax_4\hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_4\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$	(6m)	Al II
$\mathbf{B}_8$	$-2x_4\mathbf{a}_1 - x_4\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$-\frac{3}{2}ax_4\hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_4\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$	(6m)	Al II
$\mathbf{B}_9$	$x_4\mathbf{a}_1 - x_4\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$-\sqrt{3}ax_4\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$	(6m)	Al II
$\mathbf{B}_{10}$	$-x_4\mathbf{a}_1 - 2x_4\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$-\frac{3}{2}ax_4\hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_4\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$	(6m)	Al II
$\mathbf{B}_{11}$	$2x_4\mathbf{a}_1 + x_4\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$\frac{3}{2}ax_4\hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_4\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$	(6m)	Al II
$\mathbf{B}_{12}$	$-x_4\mathbf{a}_1 + x_4\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$\sqrt{3}ax_4\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$	(6m)	Al II

## References

- [1] K. Turban and H. Schäfer, *Zur Kenntnis des BaFe<sub>2</sub>Al<sub>9</sub>-Strukturtyps: Ternäre Aluminide mit A = Ba, Sr und T = Fe, Co, Ni*, J. Less-Common Met. **40**, 91–96 (1975), doi:10.1016/0022-5088(75)90184-8.

## Found in

- [1] R. E. Gladyshevskii, K. Cenzual, and E. Parthé, *Y<sub>2</sub>Co<sub>3</sub>Al<sub>9</sub> with Y<sub>2</sub>Co<sub>3</sub>Ga<sub>9</sub> type structure: an intergrowth of CsCl- and Th<sub>3</sub>Pd<sub>5</sub>-type slabs*, J. Alloys Compd. **182**, 165–170 (1992), doi:10.1016/0925-8388(92)90584-V.