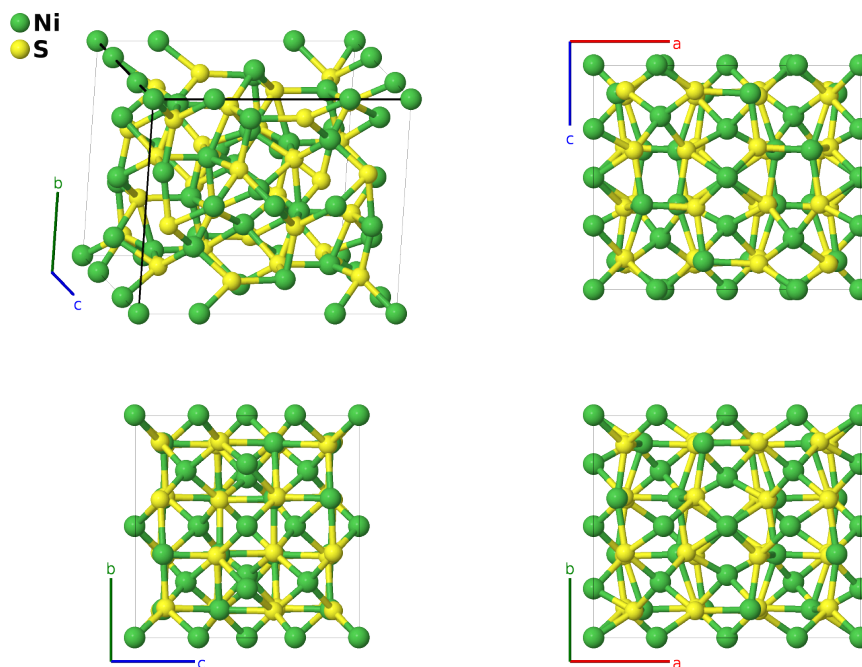


# Godlevskite ( $\text{Ni}_9\text{S}_8$ ) Structure: A9B8\_oC68\_21\_acehik2l\_4l-001

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<https://afLOW.org/p/L6M4>

[https://afLOW.org/p/A9B8\\_oC68\\_21\\_acehik2l\\_4l-001](https://afLOW.org/p/A9B8_oC68_21_acehik2l_4l-001)

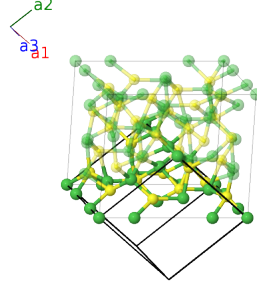


<b>Prototype</b>	$\text{Ni}_9\text{S}_8$
<b>AFLOW prototype label</b>	A9B8_oC68_21_acehik2l_4l-001
<b>Mineral name</b>	godlevskite
<b>ICSD</b>	63080
<b>Pearson symbol</b>	oC68
<b>Space group number</b>	21
<b>Space group symbol</b>	$C222$
<b>AFLOW prototype command</b>	<code>afLOW --proto=A9B8_oC68_21_acehik2l_4l-001 --params=a, b/a, c/a, x3, y4, z5, z6, x7, y7, z7, x8, y8, z8, x9, y9, z9, x10, y10, z10, x11, y11, z11, x12, y12, z12</code>

- (Fleet, 1987) says that the actual composition of the sample is  $(\text{Ni}_{8.7}\text{Fe}_{0.3})\text{S}_8$  with no information about where the iron atoms are located, although the associated ICSD entry states that our Ni-II (2c) (Fleet's (2b)) site is half nickel and half iron.

## Base-centered Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}b \hat{\mathbf{y}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}}\end{aligned}$$



## Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$0$	$=$	$0$	(2a)	Ni I
$\mathbf{B}_2$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(2c)	Ni II
$\mathbf{B}_3$	$x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2$	$=$	$ax_3 \hat{\mathbf{x}}$	(4e)	Ni III
$\mathbf{B}_4$	$-x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2$	$=$	$-ax_3 \hat{\mathbf{x}}$	(4e)	Ni III
$\mathbf{B}_5$	$-y_4 \mathbf{a}_1 + y_4 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$by_4 \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(4h)	Ni IV
$\mathbf{B}_6$	$y_4 \mathbf{a}_1 - y_4 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-by_4 \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(4h)	Ni IV
$\mathbf{B}_7$	$z_5 \mathbf{a}_3$	$=$	$cz_5 \hat{\mathbf{z}}$	(4i)	Ni V
$\mathbf{B}_8$	$-z_5 \mathbf{a}_3$	$=$	$-cz_5 \hat{\mathbf{z}}$	(4i)	Ni V
$\mathbf{B}_9$	$\frac{1}{2} \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + \frac{1}{4}b \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(4k)	Ni VI
$\mathbf{B}_{10}$	$\frac{1}{2} \mathbf{a}_1 - z_6 \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} - \frac{1}{4}b \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(4k)	Ni VI
$\mathbf{B}_{11}$	$(x_7 - y_7) \mathbf{a}_1 + (x_7 + y_7) \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(8l)	Ni VII
$\mathbf{B}_{12}$	$-(x_7 - y_7) \mathbf{a}_1 - (x_7 + y_7) \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(8l)	Ni VII
$\mathbf{B}_{13}$	$-(x_7 + y_7) \mathbf{a}_1 - (x_7 - y_7) \mathbf{a}_2 - z_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(8l)	Ni VII
$\mathbf{B}_{14}$	$(x_7 + y_7) \mathbf{a}_1 + (x_7 - y_7) \mathbf{a}_2 - z_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(8l)	Ni VII
$\mathbf{B}_{15}$	$(x_8 - y_8) \mathbf{a}_1 + (x_8 + y_8) \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(8l)	Ni VIII
$\mathbf{B}_{16}$	$-(x_8 - y_8) \mathbf{a}_1 - (x_8 + y_8) \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(8l)	Ni VIII
$\mathbf{B}_{17}$	$-(x_8 + y_8) \mathbf{a}_1 - (x_8 - y_8) \mathbf{a}_2 - z_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	(8l)	Ni VIII
$\mathbf{B}_{18}$	$(x_8 + y_8) \mathbf{a}_1 + (x_8 - y_8) \mathbf{a}_2 - z_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	(8l)	Ni VIII
$\mathbf{B}_{19}$	$(x_9 - y_9) \mathbf{a}_1 + (x_9 + y_9) \mathbf{a}_2 + z_9 \mathbf{a}_3$	$=$	$ax_9 \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(8l)	S I
$\mathbf{B}_{20}$	$-(x_9 - y_9) \mathbf{a}_1 - (x_9 + y_9) \mathbf{a}_2 + z_9 \mathbf{a}_3$	$=$	$-ax_9 \hat{\mathbf{x}} - by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(8l)	S I
$\mathbf{B}_{21}$	$-(x_9 + y_9) \mathbf{a}_1 - (x_9 - y_9) \mathbf{a}_2 - z_9 \mathbf{a}_3$	$=$	$-ax_9 \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}}$	(8l)	S I

$$\begin{aligned}
\mathbf{B}_{22} &= \begin{matrix} (x_9 + y_9) \mathbf{a}_1 + (x_9 - y_9) \mathbf{a}_2 - \\ z_9 \mathbf{a}_3 \end{matrix} = ax_9 \hat{\mathbf{x}} - by_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}} & (81) & \text{S I} \\
\mathbf{B}_{23} &= \begin{matrix} (x_{10} - y_{10}) \mathbf{a}_1 + \\ (x_{10} + y_{10}) \mathbf{a}_2 + z_{10} \mathbf{a}_3 \end{matrix} = ax_{10} \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} & (81) & \text{S II} \\
\mathbf{B}_{24} &= \begin{matrix} -(x_{10} - y_{10}) \mathbf{a}_1 - \\ (x_{10} + y_{10}) \mathbf{a}_2 + z_{10} \mathbf{a}_3 \end{matrix} = -ax_{10} \hat{\mathbf{x}} - by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} & (81) & \text{S II} \\
\mathbf{B}_{25} &= \begin{matrix} -(x_{10} + y_{10}) \mathbf{a}_1 - \\ (x_{10} - y_{10}) \mathbf{a}_2 - z_{10} \mathbf{a}_3 \end{matrix} = -ax_{10} \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}} & (81) & \text{S II} \\
\mathbf{B}_{26} &= \begin{matrix} (x_{10} + y_{10}) \mathbf{a}_1 + \\ (x_{10} - y_{10}) \mathbf{a}_2 - z_{10} \mathbf{a}_3 \end{matrix} = ax_{10} \hat{\mathbf{x}} - by_{10} \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}} & (81) & \text{S II} \\
\mathbf{B}_{27} &= \begin{matrix} (x_{11} - y_{11}) \mathbf{a}_1 + \\ (x_{11} + y_{11}) \mathbf{a}_2 + z_{11} \mathbf{a}_3 \end{matrix} = ax_{11} \hat{\mathbf{x}} + by_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} & (81) & \text{S III} \\
\mathbf{B}_{28} &= \begin{matrix} -(x_{11} - y_{11}) \mathbf{a}_1 - \\ (x_{11} + y_{11}) \mathbf{a}_2 + z_{11} \mathbf{a}_3 \end{matrix} = -ax_{11} \hat{\mathbf{x}} - by_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} & (81) & \text{S III} \\
\mathbf{B}_{29} &= \begin{matrix} -(x_{11} + y_{11}) \mathbf{a}_1 - \\ (x_{11} - y_{11}) \mathbf{a}_2 - z_{11} \mathbf{a}_3 \end{matrix} = -ax_{11} \hat{\mathbf{x}} + by_{11} \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} & (81) & \text{S III} \\
\mathbf{B}_{30} &= \begin{matrix} (x_{11} + y_{11}) \mathbf{a}_1 + \\ (x_{11} - y_{11}) \mathbf{a}_2 - z_{11} \mathbf{a}_3 \end{matrix} = ax_{11} \hat{\mathbf{x}} - by_{11} \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} & (81) & \text{S III} \\
\mathbf{B}_{31} &= \begin{matrix} (x_{12} - y_{12}) \mathbf{a}_1 + \\ (x_{12} + y_{12}) \mathbf{a}_2 + z_{12} \mathbf{a}_3 \end{matrix} = ax_{12} \hat{\mathbf{x}} + by_{12} \hat{\mathbf{y}} + cz_{12} \hat{\mathbf{z}} & (81) & \text{S IV} \\
\mathbf{B}_{32} &= \begin{matrix} -(x_{12} - y_{12}) \mathbf{a}_1 - \\ (x_{12} + y_{12}) \mathbf{a}_2 + z_{12} \mathbf{a}_3 \end{matrix} = -ax_{12} \hat{\mathbf{x}} - by_{12} \hat{\mathbf{y}} + cz_{12} \hat{\mathbf{z}} & (81) & \text{S IV} \\
\mathbf{B}_{33} &= \begin{matrix} -(x_{12} + y_{12}) \mathbf{a}_1 - \\ (x_{12} - y_{12}) \mathbf{a}_2 - z_{12} \mathbf{a}_3 \end{matrix} = -ax_{12} \hat{\mathbf{x}} + by_{12} \hat{\mathbf{y}} - cz_{12} \hat{\mathbf{z}} & (81) & \text{S IV} \\
\mathbf{B}_{34} &= \begin{matrix} (x_{12} + y_{12}) \mathbf{a}_1 + \\ (x_{12} - y_{12}) \mathbf{a}_2 - z_{12} \mathbf{a}_3 \end{matrix} = ax_{12} \hat{\mathbf{x}} - by_{12} \hat{\mathbf{y}} - cz_{12} \hat{\mathbf{z}} & (81) & \text{S IV}
\end{aligned}$$

## References

- [1] M. E. Fleet, *Structure of Godlevskite, Ni<sub>9</sub>S<sub>8</sub>*, Acta Crystallogr. Sect. C **43**, 2255–2257 (1987), doi:10.1107/S0108270187088176.

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- [1] P. Villars, H. Okamoto, and K. Cenzual, eds., *ASM Alloy Phase Diagram Database* (ASM International, 2018), chap. Nickel-Sulfur Binary Phase Diagram (1990 Singleton M.). Copyright ©2006-2018 ASM International.