

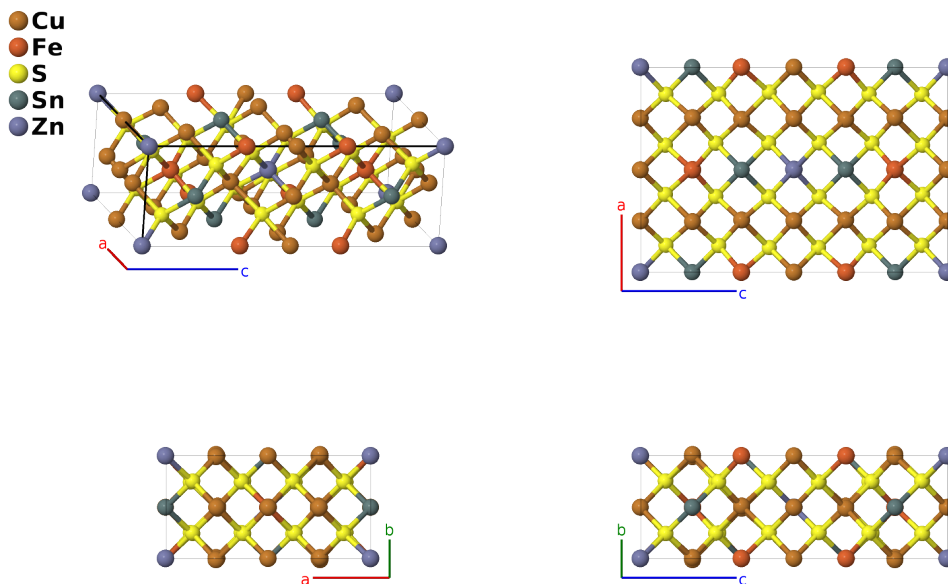
Stannoidite ($\text{Cu}_8(\text{Fe,Zn})_3\text{Sn}_2\text{S}_{12}$) Structure: A8B2C12D2E_oI50_23_acgk_e_3k_f_b-001

This structure originally had the label A8B2C12D2E_oI50_23_bcfk_i_3k_j_a. Calls to that address will be redirected here.

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<https://afLOW.org/p/7NS2>

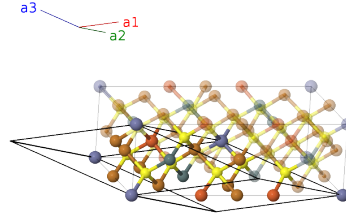
https://afLOW.org/p/A8B2C12D2E_oI50_23_acgk_e_3k_f_b-001



Prototype	$\text{Cu}_8\text{Fe}_2\text{S}_{12}\text{Sn}_2\text{Zn}$
AFLOW prototype label	A8B2C12D2E_oI50_23_acgk_e_3k_f_b-001
Mineral name	stannoidite
ICSD	41894
Pearson symbol	oI50
Space group number	23
Space group symbol	$I222$
AFLOW prototype command	<pre>afLOW --proto=A8B2C12D2E_oI50_23_acgk_e_3k_f_b-001 --params=a, b/a, c/a, x4, x5, y6, x7, y7, z7, x8, y8, z8, x9, y9, z9, x10, y10, z10</pre>

- The composition of the Zn (2a) site is actually $\text{Zn}_{0.85}\text{Fe}_{0.15}$. Here we assume that it is purely zinc.

Body-centered Orthorhombic primitive vectors



$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}}\end{aligned}$$

Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	0	$=$	0	(2a)	Cu I
\mathbf{B}_2	$\frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}}$	(2b)	Zn I
\mathbf{B}_3	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2}c \hat{\mathbf{z}}$	(2c)	Cu II
\mathbf{B}_4	$x_4 \mathbf{a}_2 + x_4 \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}}$	(4e)	Fe I
\mathbf{B}_5	$-x_4 \mathbf{a}_2 - x_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}}$	(4e)	Fe I
\mathbf{B}_6	$\frac{1}{2} \mathbf{a}_1 + (x_5 + \frac{1}{2}) \mathbf{a}_2 + x_5 \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(4f)	Sn I
\mathbf{B}_7	$\frac{1}{2} \mathbf{a}_1 - (x_5 - \frac{1}{2}) \mathbf{a}_2 - x_5 \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(4f)	Sn I
\mathbf{B}_8	$y_6 \mathbf{a}_1 + y_6 \mathbf{a}_3$	$=$	$by_6 \hat{\mathbf{y}}$	(4g)	Cu III
\mathbf{B}_9	$-y_6 \mathbf{a}_1 - y_6 \mathbf{a}_3$	$=$	$-by_6 \hat{\mathbf{y}}$	(4g)	Cu III
\mathbf{B}_{10}	$(y_7 + z_7) \mathbf{a}_1 + (x_7 + z_7) \mathbf{a}_2 + (x_7 + y_7) \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(8k)	Cu IV
\mathbf{B}_{11}	$-(y_7 - z_7) \mathbf{a}_1 - (x_7 - z_7) \mathbf{a}_2 - (x_7 + y_7) \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(8k)	Cu IV
\mathbf{B}_{12}	$(y_7 - z_7) \mathbf{a}_1 - (x_7 + z_7) \mathbf{a}_2 - (x_7 - y_7) \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(8k)	Cu IV
\mathbf{B}_{13}	$-(y_7 + z_7) \mathbf{a}_1 + (x_7 - z_7) \mathbf{a}_2 + (x_7 - y_7) \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(8k)	Cu IV
\mathbf{B}_{14}	$(y_8 + z_8) \mathbf{a}_1 + (x_8 + z_8) \mathbf{a}_2 + (x_8 + y_8) \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(8k)	S I
\mathbf{B}_{15}	$-(y_8 - z_8) \mathbf{a}_1 - (x_8 - z_8) \mathbf{a}_2 - (x_8 + y_8) \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(8k)	S I
\mathbf{B}_{16}	$(y_8 - z_8) \mathbf{a}_1 - (x_8 + z_8) \mathbf{a}_2 - (x_8 - y_8) \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	(8k)	S I
\mathbf{B}_{17}	$-(y_8 + z_8) \mathbf{a}_1 + (x_8 - z_8) \mathbf{a}_2 + (x_8 - y_8) \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	(8k)	S I
\mathbf{B}_{18}	$(y_9 + z_9) \mathbf{a}_1 + (x_9 + z_9) \mathbf{a}_2 + (x_9 + y_9) \mathbf{a}_3$	$=$	$ax_9 \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(8k)	S II
\mathbf{B}_{19}	$-(y_9 - z_9) \mathbf{a}_1 - (x_9 - z_9) \mathbf{a}_2 - (x_9 + y_9) \mathbf{a}_3$	$=$	$-ax_9 \hat{\mathbf{x}} - by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(8k)	S II
\mathbf{B}_{20}	$(y_9 - z_9) \mathbf{a}_1 - (x_9 + z_9) \mathbf{a}_2 - (x_9 - y_9) \mathbf{a}_3$	$=$	$-ax_9 \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}}$	(8k)	S II
\mathbf{B}_{21}	$-(y_9 + z_9) \mathbf{a}_1 + (x_9 - z_9) \mathbf{a}_2 + (x_9 - y_9) \mathbf{a}_3$	$=$	$ax_9 \hat{\mathbf{x}} - by_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}}$	(8k)	S II
\mathbf{B}_{22}	$(y_{10} + z_{10}) \mathbf{a}_1 + (x_{10} + z_{10}) \mathbf{a}_2 + (x_{10} + y_{10}) \mathbf{a}_3$	$=$	$ax_{10} \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}}$	(8k)	S III

$$\mathbf{B}_{23} = \begin{matrix} -(y_{10} - z_{10}) \mathbf{a}_1 - \\ (x_{10} - z_{10}) \mathbf{a}_2 - (x_{10} + y_{10}) \mathbf{a}_3 \end{matrix} = -ax_{10} \hat{\mathbf{x}} - by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} \quad (8k) \quad \text{S III}$$

$$\mathbf{B}_{24} = \begin{matrix} (y_{10} - z_{10}) \mathbf{a}_1 - (x_{10} + z_{10}) \mathbf{a}_2 - \\ (x_{10} - y_{10}) \mathbf{a}_3 \end{matrix} = -ax_{10} \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}} \quad (8k) \quad \text{S III}$$

$$\mathbf{B}_{25} = \begin{matrix} -(y_{10} + z_{10}) \mathbf{a}_1 + \\ (x_{10} - z_{10}) \mathbf{a}_2 + (x_{10} - y_{10}) \mathbf{a}_3 \end{matrix} = ax_{10} \hat{\mathbf{x}} - by_{10} \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}} \quad (8k) \quad \text{S III}$$

References

- [1] Y. Kudoh and Y. Takéuchi, *The superstructure of stannoidite*, Z. Kristallogr. **144**, 145–160 (1976), doi:10.1524/zkri.1976.144.16.145.

Found in

- [1] R. T. Downs and M. Hall-Wallace, *The American Mineralogist Crystal Structure Database*, Am. Mineral. **88**, 247–250 (2003).