

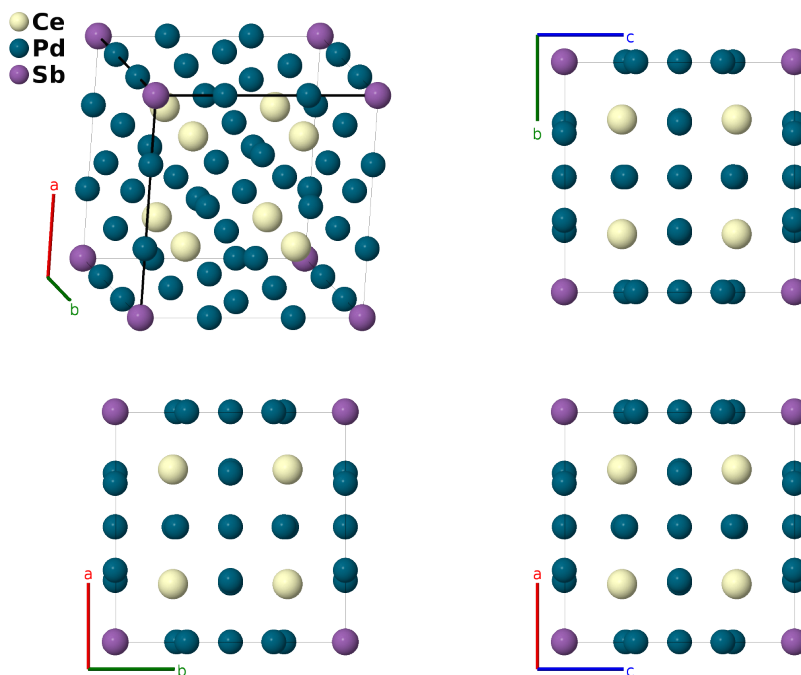
Ce₈Pd₂₄Sb Structure:

A8B24C_cP33_221_g_efh_a-001

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<https://aflow.org/p/CLMU>

https://aflow.org/p/A8B24C_cP33_221_g_efh_a-001

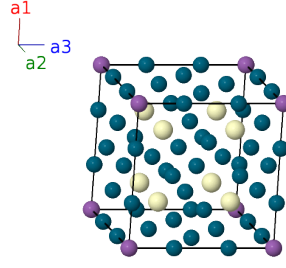


Prototype	Ce ₈ Pd ₂₄ Sb
AFLOW prototype label	A8B24C_cP33_221_g_efh_a-001
ICSD	83378
Pearson symbol	cP33
Space group number	221
Space group symbol	$Pm\bar{3}m$
AFLOW prototype command	<code>aflow --proto=A8B24C_cP33_221_g_efh_a-001 --params=a, x₂, x₃, x₄, x₅</code>

- CePd₃ forms in the $L1_2$ Cu₃Au Structure. Adding antimony at some octahedral sites gives this structure. Alternatively, this can be viewed as a cubic perovskite ($E2_1$) structure with 7/8 of the B atoms removed in an ordered manner.

Simple Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= a \hat{\mathbf{y}} \\ \mathbf{a}_3 &= a \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$=$	0	$=$	0	(1a) Sb I
\mathbf{B}_2	$=$	$x_2 \mathbf{a}_1$	$=$	$ax_2 \hat{\mathbf{x}}$	(6e) Pd I
\mathbf{B}_3	$=$	$-x_2 \mathbf{a}_1$	$=$	$-ax_2 \hat{\mathbf{x}}$	(6e) Pd I
\mathbf{B}_4	$=$	$x_2 \mathbf{a}_2$	$=$	$ax_2 \hat{\mathbf{y}}$	(6e) Pd I
\mathbf{B}_5	$=$	$-x_2 \mathbf{a}_2$	$=$	$-ax_2 \hat{\mathbf{y}}$	(6e) Pd I
\mathbf{B}_6	$=$	$x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{z}}$	(6e) Pd I
\mathbf{B}_7	$=$	$-x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{z}}$	(6e) Pd I
\mathbf{B}_8	$=$	$x_3 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6f) Pd II
\mathbf{B}_9	$=$	$-x_3 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6f) Pd II
\mathbf{B}_{10}	$=$	$\frac{1}{2} \mathbf{a}_1 + x_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6f) Pd II
\mathbf{B}_{11}	$=$	$\frac{1}{2} \mathbf{a}_1 - x_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6f) Pd II
\mathbf{B}_{12}	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + x_3 \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(6f) Pd II
\mathbf{B}_{13}	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 - x_3 \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(6f) Pd II
\mathbf{B}_{14}	$=$	$x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + x_4 \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}}$	(8g) Ce I
\mathbf{B}_{15}	$=$	$-x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 + x_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}}$	(8g) Ce I
\mathbf{B}_{16}	$=$	$-x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 - x_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}}$	(8g) Ce I
\mathbf{B}_{17}	$=$	$x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 - x_4 \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}}$	(8g) Ce I
\mathbf{B}_{18}	$=$	$x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 - x_4 \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}}$	(8g) Ce I
\mathbf{B}_{19}	$=$	$-x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 - x_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}}$	(8g) Ce I
\mathbf{B}_{20}	$=$	$x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 + x_4 \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}}$	(8g) Ce I
\mathbf{B}_{21}	$=$	$-x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + x_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}}$	(8g) Ce I
\mathbf{B}_{22}	$=$	$x_5 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$ax_5 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}}$	(12h) Pd III
\mathbf{B}_{23}	$=$	$-x_5 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$-ax_5 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}}$	(12h) Pd III
\mathbf{B}_{24}	$=$	$x_5 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(12h) Pd III
\mathbf{B}_{25}	$=$	$-x_5 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(12h) Pd III
\mathbf{B}_{26}	$=$	$\frac{1}{2} \mathbf{a}_1 + x_5 \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + ax_5 \hat{\mathbf{z}}$	(12h) Pd III
\mathbf{B}_{27}	$=$	$\frac{1}{2} \mathbf{a}_1 - x_5 \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - ax_5 \hat{\mathbf{z}}$	(12h) Pd III
\mathbf{B}_{28}	$=$	$\frac{1}{2} \mathbf{a}_1 + x_5 \mathbf{a}_2$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}}$	(12h) Pd III
\mathbf{B}_{29}	$=$	$\frac{1}{2} \mathbf{a}_1 - x_5 \mathbf{a}_2$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}}$	(12h) Pd III
\mathbf{B}_{30}	$=$	$x_5 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{z}}$	(12h) Pd III

$$\mathbf{B}_{31} = -x_5 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3 = -ax_5 \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{z}} \quad (12h) \quad \text{Pd III}$$

$$\mathbf{B}_{32} = \frac{1}{2} \mathbf{a}_2 - x_5 \mathbf{a}_3 = \frac{1}{2}a \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}} \quad (12h) \quad \text{Pd III}$$

$$\mathbf{B}_{33} = \frac{1}{2} \mathbf{a}_2 + x_5 \mathbf{a}_3 = \frac{1}{2}a \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}} \quad (12h) \quad \text{Pd III}$$

References

- [1] R. A. Gordon and F. J. DiSalvo, *Crystal Structure and Magnetic Susceptibility of $Ce_8Pd_{24}Sb$* , Z. Naturforsch. B **51**, 52–56 (1996), doi:10.1515/znb-1996-0112.