

RbNO₃ (III) Structure:

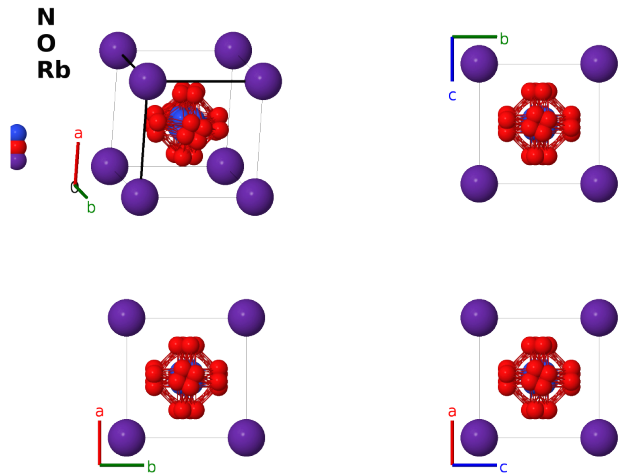
A8B24C_cP33_207_g_k_a-001

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- D. Hicks, M. J. Mehl, M. Esters, C. Oses, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/prototype-encyclopedia/2SP7>

https://aflow.org/prototype-encyclopedia/A8B24C_cP33_207_g_k_a-001



Prototype	NO ₃ Rb
AFLOW prototype label	A8B24C_cP33_207_g_k_a-001
ICSD	60966
CCDC	1624521
Pearson symbol	cP33
Space group number	207
Space group symbol	<i>P</i> 432
AFLOW prototype command	<code>aflow --proto=A8B24C_cP33_207_g_k_a-001</code> <code>--params=<i>a</i>, <i>x</i>₂, <i>x</i>₃, <i>y</i>₃, <i>z</i>₃</code>

- RbNO₃ takes on four distinct phases with increasing temperature (Shamsuzzoha, 1988):
 - Phase IV is the ground state, stable up to 437K.
 - Phase III, stable in the range 437-492K, is in this disordered cubic structure, where the NO₃ ions are centered on the halide site in the cesium chloride (*B2*) structure.
 - Phase II, stable up to 564K, is possibly a body-centered cubic structure with up to eight formula units in the conventional unit cell.
 - Phase I, stable up to the melting point, is thought to be a sodium chloride (*B1*) structure, with NO₃ again playing the role of chlorine.

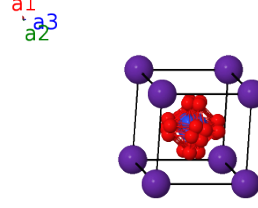
- The nitrogen and oxygen sites are filled 12.5% of the time, so that only one nitrogen and three oxygens appear on any given halide site.
- Prior to 2023 this was the only ICSD entry for space group $P432$ #207.

Simple Cubic primitive vectors

$$\mathbf{a}_1 = a \hat{\mathbf{x}}$$

$$\mathbf{a}_2 = a \hat{\mathbf{y}}$$

$$\mathbf{a}_3 = a \hat{\mathbf{z}}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$=$	0	$=$	0	(1a) Rb I
$\mathbf{B}_2$	$=$	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$	(8g) N I
$\mathbf{B}_3$	$=$	$-x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$	(8g) N I
$\mathbf{B}_4$	$=$	$-x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$	(8g) N I
$\mathbf{B}_5$	$=$	$x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$	(8g) N I
$\mathbf{B}_6$	$=$	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$	(8g) N I
$\mathbf{B}_7$	$=$	$-x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$	(8g) N I
$\mathbf{B}_8$	$=$	$x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$	(8g) N I
$\mathbf{B}_9$	$=$	$-x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$	(8g) N I
$\mathbf{B}_{10}$	$=$	$x_3 \mathbf{a}_1 + y_3 \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + ay_3 \hat{\mathbf{y}} + az_3 \hat{\mathbf{z}}$	(24k) O I
$\mathbf{B}_{11}$	$=$	$-x_3 \mathbf{a}_1 - y_3 \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} - ay_3 \hat{\mathbf{y}} + az_3 \hat{\mathbf{z}}$	(24k) O I
$\mathbf{B}_{12}$	$=$	$-x_3 \mathbf{a}_1 + y_3 \mathbf{a}_2 - z_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} + ay_3 \hat{\mathbf{y}} - az_3 \hat{\mathbf{z}}$	(24k) O I
$\mathbf{B}_{13}$	$=$	$x_3 \mathbf{a}_1 - y_3 \mathbf{a}_2 - z_3 \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} - ay_3 \hat{\mathbf{y}} - az_3 \hat{\mathbf{z}}$	(24k) O I
$\mathbf{B}_{14}$	$=$	$z_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + y_3 \mathbf{a}_3$	$=$	$az_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + ay_3 \hat{\mathbf{z}}$	(24k) O I
$\mathbf{B}_{15}$	$=$	$z_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 - y_3 \mathbf{a}_3$	$=$	$az_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - ay_3 \hat{\mathbf{z}}$	(24k) O I
$\mathbf{B}_{16}$	$=$	$-z_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 + y_3 \mathbf{a}_3$	$=$	$-az_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + ay_3 \hat{\mathbf{z}}$	(24k) O I
$\mathbf{B}_{17}$	$=$	$-z_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 - y_3 \mathbf{a}_3$	$=$	$-az_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} - ay_3 \hat{\mathbf{z}}$	(24k) O I
$\mathbf{B}_{18}$	$=$	$y_3 \mathbf{a}_1 + z_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	$=$	$ay_3 \hat{\mathbf{x}} + az_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(24k) O I
$\mathbf{B}_{19}$	$=$	$-y_3 \mathbf{a}_1 + z_3 \mathbf{a}_2 - x_3 \mathbf{a}_3$	$=$	$-ay_3 \hat{\mathbf{x}} + az_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(24k) O I
$\mathbf{B}_{20}$	$=$	$y_3 \mathbf{a}_1 - z_3 \mathbf{a}_2 - x_3 \mathbf{a}_3$	$=$	$ay_3 \hat{\mathbf{x}} - az_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(24k) O I
$\mathbf{B}_{21}$	$=$	$-y_3 \mathbf{a}_1 - z_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	$=$	$-ay_3 \hat{\mathbf{x}} - az_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(24k) O I
$\mathbf{B}_{22}$	$=$	$y_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 - z_3 \mathbf{a}_3$	$=$	$ay_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} - az_3 \hat{\mathbf{z}}$	(24k) O I
$\mathbf{B}_{23}$	$=$	$-y_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 - z_3 \mathbf{a}_3$	$=$	$-ay_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - az_3 \hat{\mathbf{z}}$	(24k) O I
$\mathbf{B}_{24}$	$=$	$y_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$ay_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + az_3 \hat{\mathbf{z}}$	(24k) O I
$\mathbf{B}_{25}$	$=$	$-y_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$-ay_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + az_3 \hat{\mathbf{z}}$	(24k) O I

$$\begin{aligned}
\mathbf{B}_{26} &= x_3 \mathbf{a}_1 + z_3 \mathbf{a}_2 - y_3 \mathbf{a}_3 &= ax_3 \hat{\mathbf{x}} + az_3 \hat{\mathbf{y}} - ay_3 \hat{\mathbf{z}} & (24k) & \text{O I} \\
\mathbf{B}_{27} &= -x_3 \mathbf{a}_1 + z_3 \mathbf{a}_2 + y_3 \mathbf{a}_3 &= -ax_3 \hat{\mathbf{x}} + az_3 \hat{\mathbf{y}} + ay_3 \hat{\mathbf{z}} & (24k) & \text{O I} \\
\mathbf{B}_{28} &= -x_3 \mathbf{a}_1 - z_3 \mathbf{a}_2 - y_3 \mathbf{a}_3 &= -ax_3 \hat{\mathbf{x}} - az_3 \hat{\mathbf{y}} - ay_3 \hat{\mathbf{z}} & (24k) & \text{O I} \\
\mathbf{B}_{29} &= x_3 \mathbf{a}_1 - z_3 \mathbf{a}_2 + y_3 \mathbf{a}_3 &= ax_3 \hat{\mathbf{x}} - az_3 \hat{\mathbf{y}} + ay_3 \hat{\mathbf{z}} & (24k) & \text{O I} \\
\mathbf{B}_{30} &= z_3 \mathbf{a}_1 + y_3 \mathbf{a}_2 - x_3 \mathbf{a}_3 &= az_3 \hat{\mathbf{x}} + ay_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}} & (24k) & \text{O I} \\
\mathbf{B}_{31} &= z_3 \mathbf{a}_1 - y_3 \mathbf{a}_2 + x_3 \mathbf{a}_3 &= az_3 \hat{\mathbf{x}} - ay_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}} & (24k) & \text{O I} \\
\mathbf{B}_{32} &= -z_3 \mathbf{a}_1 + y_3 \mathbf{a}_2 + x_3 \mathbf{a}_3 &= -az_3 \hat{\mathbf{x}} + ay_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}} & (24k) & \text{O I} \\
\mathbf{B}_{33} &= -z_3 \mathbf{a}_1 - y_3 \mathbf{a}_2 - x_3 \mathbf{a}_3 &= -az_3 \hat{\mathbf{x}} - ay_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}} & (24k) & \text{O I}
\end{aligned}$$

References

- [1] M. Shamsuzzoh and B. W. Lucas, *Single-crystal (neutron) diffraction structure of III-rubidium nitrate*, Acta Crystallogr. Sect. B **43**, 385–388 (1987), doi:10.1107/S0108270187095660.
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Found in

- [1] *Inorganic Crystal Structure Database*. Entry 60966 [RbNO₃].

First cited in

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