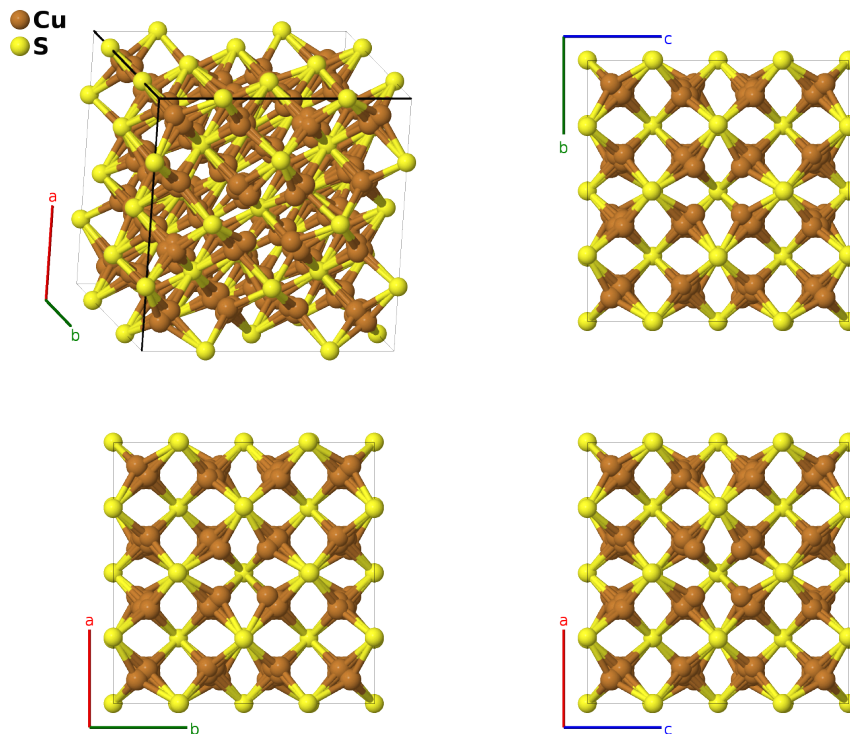


Intermediate Temperature Bornite ($\text{Cu}_{5/6}\text{Fe}_{1/6}$) $_3\text{S}_2$ Structure: A7B_cF256_225_f2k_ce-001

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<https://aflow.org/p/EMLR>

https://aflow.org/p/A7B_cF256_225_f2k_ce-001



Prototype	Cu_5FeS_4
AFLOW prototype label	A7B_cF256_225_f2k_ce-001
Mineral name	bornite
ICSD	200424
Pearson symbol	cF256
Space group number	225
Space group symbol	$Fm\bar{3}m$
AFLOW prototype command	<pre>aflow --proto=A7B_cF256_225_f2k_ce-001 --params=a, x2, x3, x4, z4, x5, z5</pre>

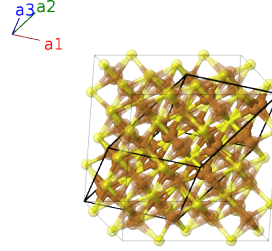
- Bornite can take on several forms at different temperatures (Martinelli, 2018).
 - At temperatures above 508K it is cubic with an “anti”-fluorite ($C1$) structure.
 - From 443K to 508K it becomes a a supercell of an anti-fluorite structure (this structure).
 - Below 443K it becomes orthorhombic, in the $Pbca$ #61 space group.

– As temperatures drop into the 50-70K range it transforms in to the non-centrosymmetric $Pca2_1$ #29 space group.

- In all of these cases the sulfur atoms form a face-centered or nearly face-centered cubic lattice.
- Data for this structure was taken at 458K. There is considerable disorder here. The site we labeled Cu-II is occupied 33% of the time with a mixture of copper and iron atoms. The Cu-I and Cu-III sites are occupied 31% and 7% of the time, respectively, and are purely copper. The sulfur atoms form a nearly cubic fcc lattice, with one of the tetrahedral sites is occupied by a copper or iron atom, and the other site is either filled by a copper atom or remains vacant. (Kanazawa, 1978)

Face-centered Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a \hat{y} + \frac{1}{2}a \hat{z} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{x} + \frac{1}{2}a \hat{z} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{x} + \frac{1}{2}a \hat{y}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= \frac{1}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{x} + \frac{1}{4}a \hat{y} + \frac{1}{4}a \hat{z}$	(8c)	S I
\mathbf{B}_2	$= \frac{3}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{3}{4}a \hat{x} + \frac{3}{4}a \hat{y} + \frac{3}{4}a \hat{z}$	(8c)	S I
\mathbf{B}_3	$= -x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{x}$	(24e)	S II
\mathbf{B}_4	$= x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{x}$	(24e)	S II
\mathbf{B}_5	$= x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{y}$	(24e)	S II
\mathbf{B}_6	$= -x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{y}$	(24e)	S II
\mathbf{B}_7	$= x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{z}$	(24e)	S II
\mathbf{B}_8	$= -x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{z}$	(24e)	S II
\mathbf{B}_9	$= x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	$=$	$ax_3 \hat{x} + ax_3 \hat{y} + ax_3 \hat{z}$	(32f)	Cu I
\mathbf{B}_{10}	$= x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 - 3x_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{x} - ax_3 \hat{y} + ax_3 \hat{z}$	(32f)	Cu I
\mathbf{B}_{11}	$= x_3 \mathbf{a}_1 - 3x_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{x} + ax_3 \hat{y} - ax_3 \hat{z}$	(32f)	Cu I
\mathbf{B}_{12}	$= -3x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	$=$	$ax_3 \hat{x} - ax_3 \hat{y} - ax_3 \hat{z}$	(32f)	Cu I
\mathbf{B}_{13}	$= -x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 + 3x_3 \mathbf{a}_3$	$=$	$ax_3 \hat{x} + ax_3 \hat{y} - ax_3 \hat{z}$	(32f)	Cu I
\mathbf{B}_{14}	$= -x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 - x_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{x} - ax_3 \hat{y} - ax_3 \hat{z}$	(32f)	Cu I
\mathbf{B}_{15}	$= -x_3 \mathbf{a}_1 + 3x_3 \mathbf{a}_2 - x_3 \mathbf{a}_3$	$=$	$ax_3 \hat{x} - ax_3 \hat{y} + ax_3 \hat{z}$	(32f)	Cu I
\mathbf{B}_{16}	$= 3x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 - x_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{x} + ax_3 \hat{y} + ax_3 \hat{z}$	(32f)	Cu I
\mathbf{B}_{17}	$= z_4 \mathbf{a}_1 + z_4 \mathbf{a}_2 + (2x_4 - z_4) \mathbf{a}_3$	$=$	$ax_4 \hat{x} + ax_4 \hat{y} + az_4 \hat{z}$	(96k)	Cu II
\mathbf{B}_{18}	$= z_4 \mathbf{a}_1 + z_4 \mathbf{a}_2 - (2x_4 + z_4) \mathbf{a}_3$	$=$	$-ax_4 \hat{x} - ax_4 \hat{y} + az_4 \hat{z}$	(96k)	Cu II
\mathbf{B}_{19}	$= (2x_4 - z_4) \mathbf{a}_1 - (2x_4 + z_4) \mathbf{a}_2 + z_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{x} + ax_4 \hat{y} - az_4 \hat{z}$	(96k)	Cu II
\mathbf{B}_{20}	$= -(2x_4 + z_4) \mathbf{a}_1 + (2x_4 - z_4) \mathbf{a}_2 + z_4 \mathbf{a}_3$	$=$	$ax_4 \hat{x} - ax_4 \hat{y} - az_4 \hat{z}$	(96k)	Cu II

$$\begin{aligned}
\mathbf{B}_{51} &= - (2x_5 + z_5) \mathbf{a}_1 + z_5 \mathbf{a}_2 + (2x_5 - z_5) \mathbf{a}_3 &= ax_5 \hat{\mathbf{x}} - az_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}} &(96k) &\text{Cu III} \\
\mathbf{B}_{52} &= (2x_5 - z_5) \mathbf{a}_1 + z_5 \mathbf{a}_2 - (2x_5 + z_5) \mathbf{a}_3 &= -ax_5 \hat{\mathbf{x}} - az_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}} &(96k) &\text{Cu III} \\
\mathbf{B}_{53} &= -z_5 \mathbf{a}_1 - z_5 \mathbf{a}_2 + (2x_5 + z_5) \mathbf{a}_3 &= ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - az_5 \hat{\mathbf{z}} &(96k) &\text{Cu III} \\
\mathbf{B}_{54} &= -z_5 \mathbf{a}_1 - z_5 \mathbf{a}_2 - (2x_5 - z_5) \mathbf{a}_3 &= -ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - az_5 \hat{\mathbf{z}} &(96k) &\text{Cu III} \\
\mathbf{B}_{55} &= - (2x_5 - z_5) \mathbf{a}_1 + (2x_5 + z_5) \mathbf{a}_2 - z_5 \mathbf{a}_3 &= ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} + az_5 \hat{\mathbf{z}} &(96k) &\text{Cu III} \\
\mathbf{B}_{56} &= (2x_5 + z_5) \mathbf{a}_1 - (2x_5 - z_5) \mathbf{a}_2 - z_5 \mathbf{a}_3 &= -ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} + az_5 \hat{\mathbf{z}} &(96k) &\text{Cu III} \\
\mathbf{B}_{57} &= - (2x_5 - z_5) \mathbf{a}_1 - z_5 \mathbf{a}_2 + (2x_5 + z_5) \mathbf{a}_3 &= ax_5 \hat{\mathbf{x}} + az_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}} &(96k) &\text{Cu III} \\
\mathbf{B}_{58} &= (2x_5 + z_5) \mathbf{a}_1 - z_5 \mathbf{a}_2 - (2x_5 - z_5) \mathbf{a}_3 &= -ax_5 \hat{\mathbf{x}} + az_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}} &(96k) &\text{Cu III} \\
\mathbf{B}_{59} &= -z_5 \mathbf{a}_1 - (2x_5 - z_5) \mathbf{a}_2 - z_5 \mathbf{a}_3 &= -ax_5 \hat{\mathbf{x}} - az_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}} &(96k) &\text{Cu III} \\
\mathbf{B}_{60} &= -z_5 \mathbf{a}_1 + (2x_5 + z_5) \mathbf{a}_2 - z_5 \mathbf{a}_3 &= ax_5 \hat{\mathbf{x}} - az_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}} &(96k) &\text{Cu III} \\
\mathbf{B}_{61} &= -z_5 \mathbf{a}_1 - (2x_5 - z_5) \mathbf{a}_2 + (2x_5 + z_5) \mathbf{a}_3 &= az_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}} &(96k) &\text{Cu III} \\
\mathbf{B}_{62} &= -z_5 \mathbf{a}_1 + (2x_5 + z_5) \mathbf{a}_2 - (2x_5 - z_5) \mathbf{a}_3 &= az_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}} &(96k) &\text{Cu III} \\
\mathbf{B}_{63} &= (2x_5 + z_5) \mathbf{a}_1 - z_5 \mathbf{a}_2 - z_5 \mathbf{a}_3 &= -az_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}} &(96k) &\text{Cu III} \\
\mathbf{B}_{64} &= - (2x_5 - z_5) \mathbf{a}_1 - z_5 \mathbf{a}_2 - z_5 \mathbf{a}_3 &= -az_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}} &(96k) &\text{Cu III}
\end{aligned}$$

References

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