

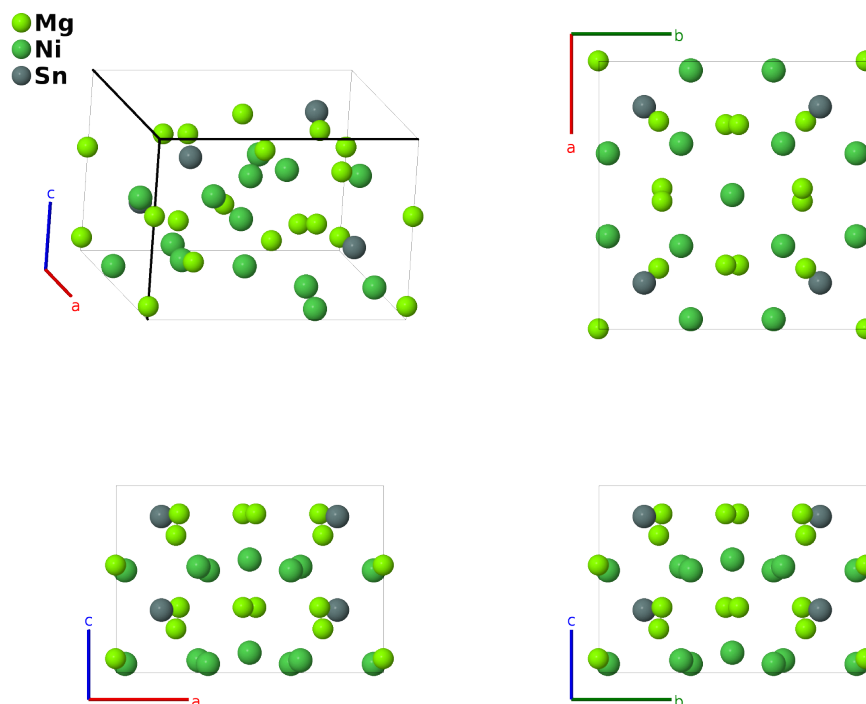
Y-MgNiSn Structure: A7B7C2_tP32_101_ade_bde_d-001

This structure originally had the label `A7B7C2_tP32_101_bde_ade_d`. Calls to that address will be redirected here.

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<https://aflow.org/p/LR8K>

https://aflow.org/p/A7B7C2_tP32_101_ade_bde_d-001



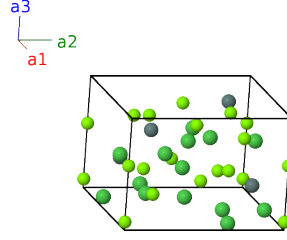
Prototype	MgNiSn
AFLOW prototype label	A7B7C2_tP32_101_ade_bde_d-001
ICSD	99208
Pearson symbol	tP32
Space group number	101
Space group symbol	$P4_2cm$
AFLOW prototype command	<code>aflow --proto=A7B7C2_tP32_101_ade_bde_d-001 --params=a, c/a, z1, z2, x3, z3, x4, z4, x5, z5, x6, y6, z6, x7, y7, z7</code>

- This is the Y-phase of the Mg-Ni-Sn ternary system. The (2b), (4d) and (8e) Wyckoff positions are partially occupied and are represented by the labels M-I, M-II, and M-III, respectively. Here, M-I is $Mg_{0.88}Ni_{0.12}$, which we label “Ni”, M-II is $Sn_{0.88}Mg_{0.12}$ labeled “Sn”, and M-III is $Mg_{0.95}Ni_{0.05}$, labeled “Ni”, with the supposed element names picked to highlight the different Wyckoff positions.

- We previously referred to this as the γ -phase, but Y-phase is the proper terminology (Boudard, 2004).

Simple Tetragonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= a \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates	=	Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= z_1 \mathbf{a}_3$	=	$c z_1 \hat{\mathbf{z}}$	(2a)	Mg I
\mathbf{B}_2	$= (z_1 + \frac{1}{2}) \mathbf{a}_3$	=	$c (z_1 + \frac{1}{2}) \hat{\mathbf{z}}$	(2a)	Mg I
\mathbf{B}_3	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + z_2 \mathbf{a}_3$	=	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + c z_2 \hat{\mathbf{z}}$	(2b)	Ni I
\mathbf{B}_4	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + (z_2 + \frac{1}{2}) \mathbf{a}_3$	=	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + c (z_2 + \frac{1}{2}) \hat{\mathbf{z}}$	(2b)	Ni I
\mathbf{B}_5	$= x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + z_3 \mathbf{a}_3$	=	$a x_3 \hat{\mathbf{x}} + a x_3 \hat{\mathbf{y}} + c z_3 \hat{\mathbf{z}}$	(4d)	Mg II
\mathbf{B}_6	$= -x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 + z_3 \mathbf{a}_3$	=	$-a x_3 \hat{\mathbf{x}} - a x_3 \hat{\mathbf{y}} + c z_3 \hat{\mathbf{z}}$	(4d)	Mg II
\mathbf{B}_7	$= -x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + (z_3 + \frac{1}{2}) \mathbf{a}_3$	=	$-a x_3 \hat{\mathbf{x}} + a x_3 \hat{\mathbf{y}} + c (z_3 + \frac{1}{2}) \hat{\mathbf{z}}$	(4d)	Mg II
\mathbf{B}_8	$= x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 + (z_3 + \frac{1}{2}) \mathbf{a}_3$	=	$a x_3 \hat{\mathbf{x}} - a x_3 \hat{\mathbf{y}} + c (z_3 + \frac{1}{2}) \hat{\mathbf{z}}$	(4d)	Mg II
\mathbf{B}_9	$= x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + z_4 \mathbf{a}_3$	=	$a x_4 \hat{\mathbf{x}} + a x_4 \hat{\mathbf{y}} + c z_4 \hat{\mathbf{z}}$	(4d)	Ni II
\mathbf{B}_{10}	$= -x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 + z_4 \mathbf{a}_3$	=	$-a x_4 \hat{\mathbf{x}} - a x_4 \hat{\mathbf{y}} + c z_4 \hat{\mathbf{z}}$	(4d)	Ni II
\mathbf{B}_{11}	$= -x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + (z_4 + \frac{1}{2}) \mathbf{a}_3$	=	$-a x_4 \hat{\mathbf{x}} + a x_4 \hat{\mathbf{y}} + c (z_4 + \frac{1}{2}) \hat{\mathbf{z}}$	(4d)	Ni II
\mathbf{B}_{12}	$= x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 + (z_4 + \frac{1}{2}) \mathbf{a}_3$	=	$a x_4 \hat{\mathbf{x}} - a x_4 \hat{\mathbf{y}} + c (z_4 + \frac{1}{2}) \hat{\mathbf{z}}$	(4d)	Ni II
\mathbf{B}_{13}	$= x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	=	$a x_5 \hat{\mathbf{x}} + a x_5 \hat{\mathbf{y}} + c z_5 \hat{\mathbf{z}}$	(4d)	Sn I
\mathbf{B}_{14}	$= -x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	=	$-a x_5 \hat{\mathbf{x}} - a x_5 \hat{\mathbf{y}} + c z_5 \hat{\mathbf{z}}$	(4d)	Sn I
\mathbf{B}_{15}	$= -x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + (z_5 + \frac{1}{2}) \mathbf{a}_3$	=	$-a x_5 \hat{\mathbf{x}} + a x_5 \hat{\mathbf{y}} + c (z_5 + \frac{1}{2}) \hat{\mathbf{z}}$	(4d)	Sn I
\mathbf{B}_{16}	$= x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + (z_5 + \frac{1}{2}) \mathbf{a}_3$	=	$a x_5 \hat{\mathbf{x}} - a x_5 \hat{\mathbf{y}} + c (z_5 + \frac{1}{2}) \hat{\mathbf{z}}$	(4d)	Sn I
\mathbf{B}_{17}	$= x_6 \mathbf{a}_1 + y_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	=	$a x_6 \hat{\mathbf{x}} + a y_6 \hat{\mathbf{y}} + c z_6 \hat{\mathbf{z}}$	(8e)	Mg III
\mathbf{B}_{18}	$= -x_6 \mathbf{a}_1 - y_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	=	$-a x_6 \hat{\mathbf{x}} - a y_6 \hat{\mathbf{y}} + c z_6 \hat{\mathbf{z}}$	(8e)	Mg III
\mathbf{B}_{19}	$= -y_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 + (z_6 + \frac{1}{2}) \mathbf{a}_3$	=	$-a y_6 \hat{\mathbf{x}} + a x_6 \hat{\mathbf{y}} + c (z_6 + \frac{1}{2}) \hat{\mathbf{z}}$	(8e)	Mg III
\mathbf{B}_{20}	$= y_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 + (z_6 + \frac{1}{2}) \mathbf{a}_3$	=	$a y_6 \hat{\mathbf{x}} - a x_6 \hat{\mathbf{y}} + c (z_6 + \frac{1}{2}) \hat{\mathbf{z}}$	(8e)	Mg III
\mathbf{B}_{21}	$= x_6 \mathbf{a}_1 - y_6 \mathbf{a}_2 + (z_6 + \frac{1}{2}) \mathbf{a}_3$	=	$a x_6 \hat{\mathbf{x}} - a y_6 \hat{\mathbf{y}} + c (z_6 + \frac{1}{2}) \hat{\mathbf{z}}$	(8e)	Mg III
\mathbf{B}_{22}	$= -x_6 \mathbf{a}_1 + y_6 \mathbf{a}_2 + (z_6 + \frac{1}{2}) \mathbf{a}_3$	=	$-a x_6 \hat{\mathbf{x}} + a y_6 \hat{\mathbf{y}} + c (z_6 + \frac{1}{2}) \hat{\mathbf{z}}$	(8e)	Mg III
\mathbf{B}_{23}	$= -y_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	=	$-a y_6 \hat{\mathbf{x}} - a x_6 \hat{\mathbf{y}} + c z_6 \hat{\mathbf{z}}$	(8e)	Mg III
\mathbf{B}_{24}	$= y_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	=	$a y_6 \hat{\mathbf{x}} + a x_6 \hat{\mathbf{y}} + c z_6 \hat{\mathbf{z}}$	(8e)	Mg III
\mathbf{B}_{25}	$= x_7 \mathbf{a}_1 + y_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	=	$a x_7 \hat{\mathbf{x}} + a y_7 \hat{\mathbf{y}} + c z_7 \hat{\mathbf{z}}$	(8e)	Ni III
\mathbf{B}_{26}	$= -x_7 \mathbf{a}_1 - y_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	=	$-a x_7 \hat{\mathbf{x}} - a y_7 \hat{\mathbf{y}} + c z_7 \hat{\mathbf{z}}$	(8e)	Ni III
\mathbf{B}_{27}	$= -y_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 + (z_7 + \frac{1}{2}) \mathbf{a}_3$	=	$-a y_7 \hat{\mathbf{x}} + a x_7 \hat{\mathbf{y}} + c (z_7 + \frac{1}{2}) \hat{\mathbf{z}}$	(8e)	Ni III

$$\begin{aligned}
\mathbf{B}_{28} &= y_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 + \left(z_7 + \frac{1}{2}\right) \mathbf{a}_3 &= ay_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} + c \left(z_7 + \frac{1}{2}\right) \hat{\mathbf{z}} & (8e) & \text{Ni III} \\
\mathbf{B}_{29} &= x_7 \mathbf{a}_1 - y_7 \mathbf{a}_2 + \left(z_7 + \frac{1}{2}\right) \mathbf{a}_3 &= ax_7 \hat{\mathbf{x}} - ay_7 \hat{\mathbf{y}} + c \left(z_7 + \frac{1}{2}\right) \hat{\mathbf{z}} & (8e) & \text{Ni III} \\
\mathbf{B}_{30} &= -x_7 \mathbf{a}_1 + y_7 \mathbf{a}_2 + \left(z_7 + \frac{1}{2}\right) \mathbf{a}_3 &= -ax_7 \hat{\mathbf{x}} + ay_7 \hat{\mathbf{y}} + c \left(z_7 + \frac{1}{2}\right) \hat{\mathbf{z}} & (8e) & \text{Ni III} \\
\mathbf{B}_{31} &= -y_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 + z_7 \mathbf{a}_3 &= -ay_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (8e) & \text{Ni III} \\
\mathbf{B}_{32} &= y_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 + z_7 \mathbf{a}_3 &= ay_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (8e) & \text{Ni III}
\end{aligned}$$

References

- [1] M. Boudard, P. Bordet, H. Vincent, and F. Audebert, *The structure of the Y-phase in the Mg-Ni-Sn system*, J. Alloys Compd. **372**, 121–128 (2004), doi:10.1016/j.jallcom.2003.09.142.

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