

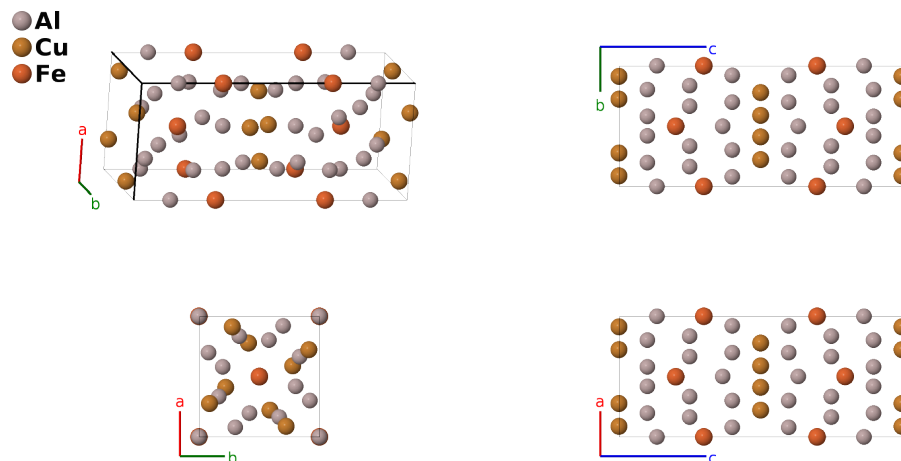
FeCu₂Al₇ (*E9_a*) Structure: A7B2C_tP40_128_egi_h_e-001

This structure originally had the label A7B2C_tP40_128_egi_h_e. Calls to that address will be redirected here.

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<https://aflow.org/p/YX16>

https://aflow.org/p/A7B2C_tP40_128_egi_h_e-001



Prototype	Al ₇ Cu ₂ Fe
AFLOW prototype label	A7B2C_tP40_128_egi_h_e-001
<i>Strukturbericht</i> designation	<i>E9_a</i>
ICSD	57677
Pearson symbol	tP40
Space group number	128
Space group symbol	<i>P4/mnc</i>
AFLOW prototype command	<code>aflow --proto=A7B2C_tP40_128_egi_h_e-001 --params=a, c/a, z₁, z₂, x₃, x₄, y₄, x₅, y₅, z₅</code>

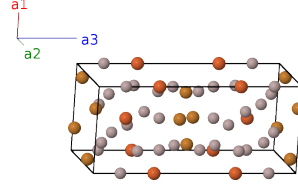
Other compounds with this structure

CoCu₂Al₇, NiCu₃Al₆, T(CoCuAl) – an alloy with approximate composition Co₂Cu_{4.9}Al_{17.7}

- Our original (Hicks, 2019) CIF for this structure has incorrect *z*-coordinates for the Al I and Fe I atoms. We have corrected the errors with this release.

Simple Tetragonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= a \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= z_1 \mathbf{a}_3$	$=$	$c z_1 \hat{\mathbf{z}}$	(4e)	Al I
\mathbf{B}_2	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 - (z_1 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} - c (z_1 - \frac{1}{2}) \hat{\mathbf{z}}$	(4e)	Al I
\mathbf{B}_3	$= -z_1 \mathbf{a}_3$	$=$	$-c z_1 \hat{\mathbf{z}}$	(4e)	Al I
\mathbf{B}_4	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + (z_1 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + c (z_1 + \frac{1}{2}) \hat{\mathbf{z}}$	(4e)	Al I
\mathbf{B}_5	$= z_2 \mathbf{a}_3$	$=$	$c z_2 \hat{\mathbf{z}}$	(4e)	Fe I
\mathbf{B}_6	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 - (z_2 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} - c (z_2 - \frac{1}{2}) \hat{\mathbf{z}}$	(4e)	Fe I
\mathbf{B}_7	$= -z_2 \mathbf{a}_3$	$=$	$-c z_2 \hat{\mathbf{z}}$	(4e)	Fe I
\mathbf{B}_8	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + (z_2 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + c (z_2 + \frac{1}{2}) \hat{\mathbf{z}}$	(4e)	Fe I
\mathbf{B}_9	$= x_3 \mathbf{a}_1 + (x_3 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$a x_3 \hat{\mathbf{x}} + a (x_3 + \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}}$	(8g)	Al II
\mathbf{B}_{10}	$= -x_3 \mathbf{a}_1 - (x_3 - \frac{1}{2}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$-a x_3 \hat{\mathbf{x}} - a (x_3 - \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}}$	(8g)	Al II
\mathbf{B}_{11}	$= -(x_3 - \frac{1}{2}) \mathbf{a}_1 + x_3 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$-a (x_3 - \frac{1}{2}) \hat{\mathbf{x}} + a x_3 \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}}$	(8g)	Al II
\mathbf{B}_{12}	$= (x_3 + \frac{1}{2}) \mathbf{a}_1 - x_3 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$a (x_3 + \frac{1}{2}) \hat{\mathbf{x}} - a x_3 \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}}$	(8g)	Al II
\mathbf{B}_{13}	$= -x_3 \mathbf{a}_1 - (x_3 - \frac{1}{2}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$-a x_3 \hat{\mathbf{x}} - a (x_3 - \frac{1}{2}) \hat{\mathbf{y}} + \frac{3}{4} c \hat{\mathbf{z}}$	(8g)	Al II
\mathbf{B}_{14}	$= x_3 \mathbf{a}_1 + (x_3 + \frac{1}{2}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$a x_3 \hat{\mathbf{x}} + a (x_3 + \frac{1}{2}) \hat{\mathbf{y}} + \frac{3}{4} c \hat{\mathbf{z}}$	(8g)	Al II
\mathbf{B}_{15}	$= (x_3 + \frac{1}{2}) \mathbf{a}_1 - x_3 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$a (x_3 + \frac{1}{2}) \hat{\mathbf{x}} - a x_3 \hat{\mathbf{y}} + \frac{3}{4} c \hat{\mathbf{z}}$	(8g)	Al II
\mathbf{B}_{16}	$= -(x_3 - \frac{1}{2}) \mathbf{a}_1 + x_3 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$-a (x_3 - \frac{1}{2}) \hat{\mathbf{x}} + a x_3 \hat{\mathbf{y}} + \frac{3}{4} c \hat{\mathbf{z}}$	(8g)	Al II
\mathbf{B}_{17}	$= x_4 \mathbf{a}_1 + y_4 \mathbf{a}_2$	$=$	$a x_4 \hat{\mathbf{x}} + a y_4 \hat{\mathbf{y}}$	(8h)	Cu I
\mathbf{B}_{18}	$= -x_4 \mathbf{a}_1 - y_4 \mathbf{a}_2$	$=$	$-a x_4 \hat{\mathbf{x}} - a y_4 \hat{\mathbf{y}}$	(8h)	Cu I
\mathbf{B}_{19}	$= -y_4 \mathbf{a}_1 + x_4 \mathbf{a}_2$	$=$	$-a y_4 \hat{\mathbf{x}} + a x_4 \hat{\mathbf{y}}$	(8h)	Cu I
\mathbf{B}_{20}	$= y_4 \mathbf{a}_1 - x_4 \mathbf{a}_2$	$=$	$a y_4 \hat{\mathbf{x}} - a x_4 \hat{\mathbf{y}}$	(8h)	Cu I
\mathbf{B}_{21}	$= -(x_4 - \frac{1}{2}) \mathbf{a}_1 + (y_4 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-a (x_4 - \frac{1}{2}) \hat{\mathbf{x}} + a (y_4 + \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(8h)	Cu I
\mathbf{B}_{22}	$= (x_4 + \frac{1}{2}) \mathbf{a}_1 - (y_4 - \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$a (x_4 + \frac{1}{2}) \hat{\mathbf{x}} - a (y_4 - \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(8h)	Cu I
\mathbf{B}_{23}	$= (y_4 + \frac{1}{2}) \mathbf{a}_1 + (x_4 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$a (y_4 + \frac{1}{2}) \hat{\mathbf{x}} + a (x_4 + \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(8h)	Cu I
\mathbf{B}_{24}	$= -(y_4 - \frac{1}{2}) \mathbf{a}_1 - (x_4 - \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-a (y_4 - \frac{1}{2}) \hat{\mathbf{x}} - a (x_4 - \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(8h)	Cu I
\mathbf{B}_{25}	$= x_5 \mathbf{a}_1 + y_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$a x_5 \hat{\mathbf{x}} + a y_5 \hat{\mathbf{y}} + c z_5 \hat{\mathbf{z}}$	(16i)	Al III
\mathbf{B}_{26}	$= -x_5 \mathbf{a}_1 - y_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$-a x_5 \hat{\mathbf{x}} - a y_5 \hat{\mathbf{y}} + c z_5 \hat{\mathbf{z}}$	(16i)	Al III
\mathbf{B}_{27}	$= -y_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$-a y_5 \hat{\mathbf{x}} + a x_5 \hat{\mathbf{y}} + c z_5 \hat{\mathbf{z}}$	(16i)	Al III
\mathbf{B}_{28}	$= y_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$a y_5 \hat{\mathbf{x}} - a x_5 \hat{\mathbf{y}} + c z_5 \hat{\mathbf{z}}$	(16i)	Al III
\mathbf{B}_{29}	$= -(x_5 - \frac{1}{2}) \mathbf{a}_1 + (y_5 + \frac{1}{2}) \mathbf{a}_2 - (z_5 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-a (x_5 - \frac{1}{2}) \hat{\mathbf{x}} + a (y_5 + \frac{1}{2}) \hat{\mathbf{y}} - c (z_5 - \frac{1}{2}) \hat{\mathbf{z}}$	(16i)	Al III

$$\begin{aligned}
\mathbf{B}_{30} &= \begin{pmatrix} x_5 + \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} y_5 - \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \mathbf{a}_2 - \mathbf{a}_3 &= a \left(x_5 + \frac{1}{2} \right) \hat{\mathbf{x}} - a \left(y_5 - \frac{1}{2} \right) \hat{\mathbf{y}} - c \left(z_5 - \frac{1}{2} \right) \hat{\mathbf{z}} & (16i) & \text{Al III} \\
\mathbf{B}_{31} &= \begin{pmatrix} y_5 + \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} x_5 + \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \mathbf{a}_2 - \mathbf{a}_3 &= a \left(y_5 + \frac{1}{2} \right) \hat{\mathbf{x}} + a \left(x_5 + \frac{1}{2} \right) \hat{\mathbf{y}} - c \left(z_5 - \frac{1}{2} \right) \hat{\mathbf{z}} & (16i) & \text{Al III} \\
\mathbf{B}_{32} &= - \begin{pmatrix} y_5 - \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} x_5 - \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \mathbf{a}_2 - \mathbf{a}_3 &= -a \left(y_5 - \frac{1}{2} \right) \hat{\mathbf{x}} - a \left(x_5 - \frac{1}{2} \right) \hat{\mathbf{y}} - c \left(z_5 - \frac{1}{2} \right) \hat{\mathbf{z}} & (16i) & \text{Al III} \\
\mathbf{B}_{33} &= -x_5 \mathbf{a}_1 - y_5 \mathbf{a}_2 - z_5 \mathbf{a}_3 &= -ax_5 \hat{\mathbf{x}} - ay_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}} & (16i) & \text{Al III} \\
\mathbf{B}_{34} &= x_5 \mathbf{a}_1 + y_5 \mathbf{a}_2 - z_5 \mathbf{a}_3 &= ax_5 \hat{\mathbf{x}} + ay_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}} & (16i) & \text{Al III} \\
\mathbf{B}_{35} &= y_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - z_5 \mathbf{a}_3 &= ay_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}} & (16i) & \text{Al III} \\
\mathbf{B}_{36} &= -y_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 - z_5 \mathbf{a}_3 &= -ay_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}} & (16i) & \text{Al III} \\
\mathbf{B}_{37} &= \begin{pmatrix} x_5 + \frac{1}{2} \\ z_5 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} y_5 - \frac{1}{2} \\ z_5 + \frac{1}{2} \end{pmatrix} \mathbf{a}_2 + \mathbf{a}_3 &= a \left(x_5 + \frac{1}{2} \right) \hat{\mathbf{x}} - a \left(y_5 - \frac{1}{2} \right) \hat{\mathbf{y}} + c \left(z_5 + \frac{1}{2} \right) \hat{\mathbf{z}} & (16i) & \text{Al III} \\
\mathbf{B}_{38} &= - \begin{pmatrix} x_5 - \frac{1}{2} \\ z_5 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} y_5 + \frac{1}{2} \\ z_5 + \frac{1}{2} \end{pmatrix} \mathbf{a}_2 + \mathbf{a}_3 &= -a \left(x_5 - \frac{1}{2} \right) \hat{\mathbf{x}} + a \left(y_5 + \frac{1}{2} \right) \hat{\mathbf{y}} + c \left(z_5 + \frac{1}{2} \right) \hat{\mathbf{z}} & (16i) & \text{Al III} \\
\mathbf{B}_{39} &= - \begin{pmatrix} y_5 - \frac{1}{2} \\ z_5 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} x_5 - \frac{1}{2} \\ z_5 + \frac{1}{2} \end{pmatrix} \mathbf{a}_2 + \mathbf{a}_3 &= -a \left(y_5 - \frac{1}{2} \right) \hat{\mathbf{x}} - a \left(x_5 - \frac{1}{2} \right) \hat{\mathbf{y}} + c \left(z_5 + \frac{1}{2} \right) \hat{\mathbf{z}} & (16i) & \text{Al III} \\
\mathbf{B}_{40} &= \begin{pmatrix} y_5 + \frac{1}{2} \\ z_5 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} x_5 + \frac{1}{2} \\ z_5 + \frac{1}{2} \end{pmatrix} \mathbf{a}_2 + \mathbf{a}_3 &= a \left(y_5 + \frac{1}{2} \right) \hat{\mathbf{x}} + a \left(x_5 + \frac{1}{2} \right) \hat{\mathbf{y}} + c \left(z_5 + \frac{1}{2} \right) \hat{\mathbf{z}} & (16i) & \text{Al III}
\end{aligned}$$

References

- [1] M. G. Bown and P. J. Brown, *The structure of FeCu₂Al₇ and T(CoCuAl)*, *Acta Cryst.* **9**, 911–914 (1956), doi:10.1107/S0365110X56002576.
- [2] D. Hicks, M. J. Mehl, E. Gossett, C. Toher, O. Levy, R. M. Hanson, G. Hart, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 2*, *Comput. Mater. Sci.* **161**, S1–S1011 (2019), doi:10.1016/j.commatsci.2018.10.043.