

# y-Y<sub>2</sub>Si<sub>2</sub>O<sub>7</sub> Structure:

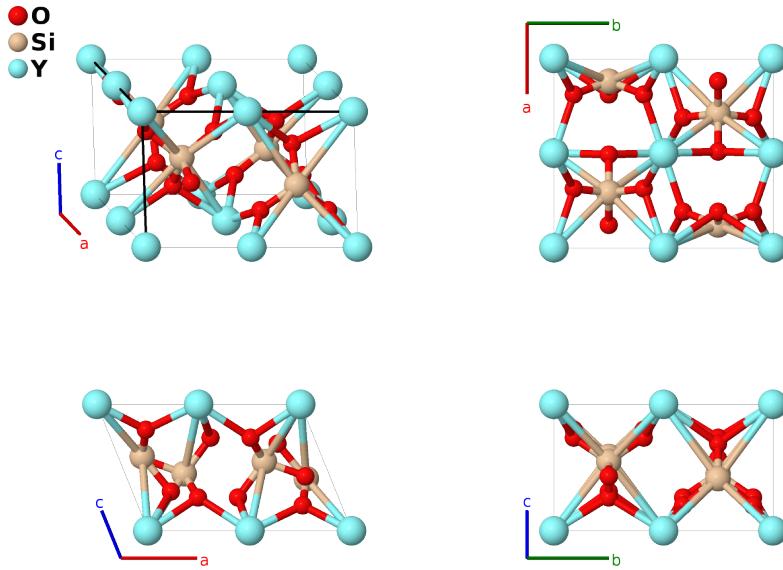
A7B2C2\_mP22\_11\_3e2f\_2e\_ab-001

This structure originally had the label A7B2C2\_mP22\_11\_3e2f\_2e\_ab. Calls to that address will be redirected here.

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<https://aflow.org/p/3RSG>

[https://aflow.org/p/A7B2C2\\_mP22\\_11\\_3e2f\\_2e\\_ab-001](https://aflow.org/p/A7B2C2_mP22_11_3e2f_2e_ab-001)



**Prototype** O<sub>7</sub>Si<sub>2</sub>Y<sub>2</sub>

**AFLOW prototype label** A7B2C2\_mP22\_11\_3e2f\_2e\_ab-001

**ICSD** 28004

**Pearson symbol** mP22

**Space group number** 11

**Space group symbol** P<sub>2</sub><sub>1</sub>/m

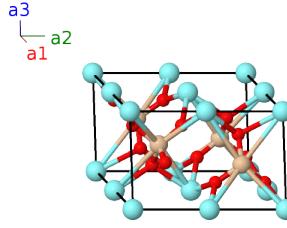
**AFLOW prototype command**

```
aflow --proto=A7B2C2_mP22_11_3e2f_2e_ab-001  
--params=a,b/a,c/a,\beta,x3,z3,x4,z4,x5,z5,x6,z6,x7,z7,x8,y8,z8,x9,y9,z9
```

- (Becerro, 2003) found that the NMR spectrum of y-Y<sub>2</sub>Si<sub>2</sub>O<sub>7</sub> showed only one peak for yttrium. If that is the case, then this crystal structure is incorrect.

**Simple Monoclinic primitive vectors**

$$\begin{aligned}
\mathbf{a}_1 &= a \hat{\mathbf{x}} \\
\mathbf{a}_2 &= b \hat{\mathbf{y}} \\
\mathbf{a}_3 &= c \cos \beta \hat{\mathbf{x}} + c \sin \beta \hat{\mathbf{z}}
\end{aligned}$$



## Basis vectors

|                   | Lattice coordinates   | Cartesian coordinates   | Wyckoff position | Atom type |
|-------------------|---|---|------------------|-----------|
| $\mathbf{B}_1$    | = 0   | = 0   | (2a)             | Y I       |
| $\mathbf{B}_2$    | = $\frac{1}{2} \mathbf{a}_2$  | = $\frac{1}{2} b \hat{\mathbf{y}}$  | (2a)             | Y I       |
| $\mathbf{B}_3$    | = $\frac{1}{2} \mathbf{a}_1$  | = $\frac{1}{2} a \hat{\mathbf{x}}$  | (2b)             | Y II      |
| $\mathbf{B}_4$    | = $\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$                     | = $\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} b \hat{\mathbf{y}}$   | (2b)             | Y II      |
| $\mathbf{B}_5$    | = $x_3 \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + z_3 \mathbf{a}_3$          | = $(ax_3 + cz_3 \cos \beta) \hat{\mathbf{x}} + \frac{1}{4} b \hat{\mathbf{y}} + cz_3 \sin \beta \hat{\mathbf{z}}$         | (2e)             | O I       |
| $\mathbf{B}_6$    | = $-x_3 \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - z_3 \mathbf{a}_3$         | = $-(ax_3 + cz_3 \cos \beta) \hat{\mathbf{x}} + \frac{3}{4} b \hat{\mathbf{y}} - cz_3 \sin \beta \hat{\mathbf{z}}$        | (2e)             | O I       |
| $\mathbf{B}_7$    | = $x_4 \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + z_4 \mathbf{a}_3$          | = $(ax_4 + cz_4 \cos \beta) \hat{\mathbf{x}} + \frac{1}{4} b \hat{\mathbf{y}} + cz_4 \sin \beta \hat{\mathbf{z}}$         | (2e)             | O II      |
| $\mathbf{B}_8$    | = $-x_4 \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - z_4 \mathbf{a}_3$         | = $-(ax_4 + cz_4 \cos \beta) \hat{\mathbf{x}} + \frac{3}{4} b \hat{\mathbf{y}} - cz_4 \sin \beta \hat{\mathbf{z}}$        | (2e)             | O II      |
| $\mathbf{B}_9$    | = $x_5 \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + z_5 \mathbf{a}_3$          | = $(ax_5 + cz_5 \cos \beta) \hat{\mathbf{x}} + \frac{1}{4} b \hat{\mathbf{y}} + cz_5 \sin \beta \hat{\mathbf{z}}$         | (2e)             | O III     |
| $\mathbf{B}_{10}$ | = $-x_5 \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - z_5 \mathbf{a}_3$         | = $-(ax_5 + cz_5 \cos \beta) \hat{\mathbf{x}} + \frac{3}{4} b \hat{\mathbf{y}} - cz_5 \sin \beta \hat{\mathbf{z}}$        | (2e)             | O III     |
| $\mathbf{B}_{11}$ | = $x_6 \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + z_6 \mathbf{a}_3$          | = $(ax_6 + cz_6 \cos \beta) \hat{\mathbf{x}} + \frac{1}{4} b \hat{\mathbf{y}} + cz_6 \sin \beta \hat{\mathbf{z}}$         | (2e)             | Si I      |
| $\mathbf{B}_{12}$ | = $-x_6 \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - z_6 \mathbf{a}_3$         | = $-(ax_6 + cz_6 \cos \beta) \hat{\mathbf{x}} + \frac{3}{4} b \hat{\mathbf{y}} - cz_6 \sin \beta \hat{\mathbf{z}}$        | (2e)             | Si I      |
| $\mathbf{B}_{13}$ | = $x_7 \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + z_7 \mathbf{a}_3$          | = $(ax_7 + cz_7 \cos \beta) \hat{\mathbf{x}} + \frac{1}{4} b \hat{\mathbf{y}} + cz_7 \sin \beta \hat{\mathbf{z}}$         | (2e)             | Si II     |
| $\mathbf{B}_{14}$ | = $-x_7 \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - z_7 \mathbf{a}_3$         | = $-(ax_7 + cz_7 \cos \beta) \hat{\mathbf{x}} + \frac{3}{4} b \hat{\mathbf{y}} - cz_7 \sin \beta \hat{\mathbf{z}}$        | (2e)             | Si II     |
| $\mathbf{B}_{15}$ | = $x_8 \mathbf{a}_1 + y_8 \mathbf{a}_2 + z_8 \mathbf{a}_3$                  | = $(ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} + cz_8 \sin \beta \hat{\mathbf{z}}$                  | (4f)             | O IV      |
| $\mathbf{B}_{16}$ | = $-x_8 \mathbf{a}_1 + (y_8 + \frac{1}{2}) \mathbf{a}_2 - z_8 \mathbf{a}_3$ | = $-(ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} + b(y_8 + \frac{1}{2}) \hat{\mathbf{y}} - cz_8 \sin \beta \hat{\mathbf{z}}$ | (4f)             | O IV      |
| $\mathbf{B}_{17}$ | = $-x_8 \mathbf{a}_1 - y_8 \mathbf{a}_2 - z_8 \mathbf{a}_3$                 | = $-(ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} - cz_8 \sin \beta \hat{\mathbf{z}}$                 | (4f)             | O IV      |
| $\mathbf{B}_{18}$ | = $x_8 \mathbf{a}_1 - (y_8 - \frac{1}{2}) \mathbf{a}_2 + z_8 \mathbf{a}_3$  | = $(ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} - b(y_8 - \frac{1}{2}) \hat{\mathbf{y}} + cz_8 \sin \beta \hat{\mathbf{z}}$  | (4f)             | O IV      |
| $\mathbf{B}_{19}$ | = $x_9 \mathbf{a}_1 + y_9 \mathbf{a}_2 + z_9 \mathbf{a}_3$                  | = $(ax_9 + cz_9 \cos \beta) \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} + cz_9 \sin \beta \hat{\mathbf{z}}$                  | (4f)             | O V       |
| $\mathbf{B}_{20}$ | = $-x_9 \mathbf{a}_1 + (y_9 + \frac{1}{2}) \mathbf{a}_2 - z_9 \mathbf{a}_3$ | = $-(ax_9 + cz_9 \cos \beta) \hat{\mathbf{x}} + b(y_9 + \frac{1}{2}) \hat{\mathbf{y}} - cz_9 \sin \beta \hat{\mathbf{z}}$ | (4f)             | O V       |
| $\mathbf{B}_{21}$ | = $-x_9 \mathbf{a}_1 - y_9 \mathbf{a}_2 - z_9 \mathbf{a}_3$                 | = $-(ax_9 + cz_9 \cos \beta) \hat{\mathbf{x}} - by_9 \hat{\mathbf{y}} - cz_9 \sin \beta \hat{\mathbf{z}}$                 | (4f)             | O V       |
| $\mathbf{B}_{22}$ | = $x_9 \mathbf{a}_1 - (y_9 - \frac{1}{2}) \mathbf{a}_2 + z_9 \mathbf{a}_3$  | = $(ax_9 + cz_9 \cos \beta) \hat{\mathbf{x}} - b(y_9 - \frac{1}{2}) \hat{\mathbf{y}} + cz_9 \sin \beta \hat{\mathbf{z}}$  | (4f)             | O V       |

## References

- [1] N. G. Batalieva and Y. A. Pyatenko, *Artificial yttrialite ("y-phase") - a representative of a new structure type in the rare earth diorthosilicate series*, Sov. Phys. Crystallogr. **16**, 786–789 (1972). Translation of N. G. Batalieva and Yu. A. Pyatenko, Kristallogr. 16, 905 (1971).

- [2] A. I. Becerro, A. Escudero, P. Florian, D. Massiot, and M. D. Alba, *Revisiting  $Y_2Si_2O_7$  and  $Y_2SiO_5$  polymorphic structures by  $^9Y$  MAS-NMR spectroscopy*, J. Solid State Chem. **177**, 2783–2789 (2004), doi:10.1016/j.jssc.2004.03.047.

#### Found in

- [1] A. I. Becerro and A. Escudero, *Revision of the crystallographic data of polymorphic  $Y_2Si_2O_7$  and  $Y_2SiO_5$  compounds*, Phase Transit. **77**, 1093–1102 (2004), doi:10.1080/01411590412331282814.