

Tb₁₁Si₄In₆ Structure:

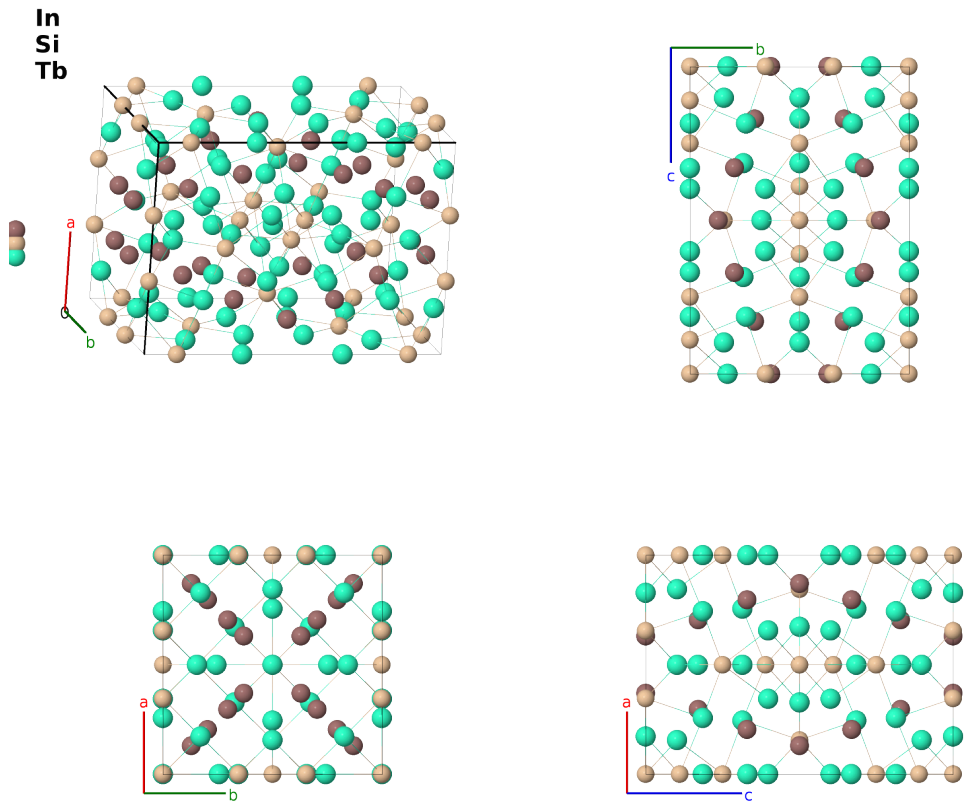
A6B4C11_tI84_139_hm_dei_eh2n-001

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<https://aflow.org/prototype-encyclopedia/0KJ3>

https://aflow.org/prototype-encyclopedia/A6B4C11_tI84_139_hm_dei_eh2n-001



Prototype	In ₆ Si ₄ Tb ₁₁
AFLOW prototype label	A6B4C11_tI84_139_hm_dei_eh2n-001
ICSD	184236
CCDC	1693480
Pearson symbol	tI84
Space group number	139
Space group symbol	<i>I4/mmm</i>
AFLOW prototype command	<code>aflow --proto=A6B4C11_tI84_139_hm_dei_eh2n-001</code> <code>--params=a, c/a, z₂, z₃, x₄, x₅, x₆, x₇, z₇, y₈, z₈, y₉, z₉</code>

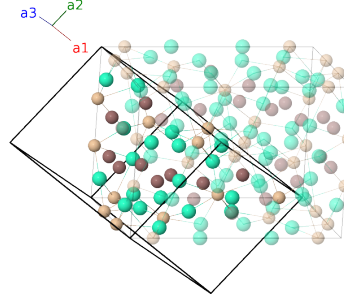
Other compounds with this structure

Dy₁₁Ge₄In₆, Dy₁₁Si₄In₆, Er₁₁Ge₄In₆, Er₁₁Si₄In₆, Gd₁₁Ge₄In₆, Gd₁₁Si₄In₆, Ho₁₁Ge₄In₆, Ho₁₁Si₄In₆, La₁₁Ge₄In₆, Tb₁₁Ge₄In₆, Y₁₁Ge₄In₆, Y₁₁Si₄In₆

- This is a ternary form of Ho₁₁Ge₁₀. The ICSD lists all these compounds using the Ho₁₁Ge₁₀ prototype. Tb₁₁Si₄In₆ is the first ICSD entry in the reference, so we use it as the ternary prototype.
- Sc₁₁Al₂Ge₈ is a second ternary form of Ho₁₁Ge₁₀.
- The AFLOW standard labeling algorithm shifts the origin by (0.5 a, 0.5 b, 0), moving the Si III atom from the published (8j) Wyckoff position to (8i).

Body-centered Tetragonal primitive vectors

$$\begin{aligned} \mathbf{a}_1 &= -\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} - \frac{1}{2}c\hat{\mathbf{z}} \end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= \frac{3}{4}\mathbf{a}_1 + \frac{1}{4}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(4d)	Si I
$\mathbf{B}_2$	$= \frac{1}{4}\mathbf{a}_1 + \frac{3}{4}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{4}c\hat{\mathbf{z}}$	(4d)	Si I
$\mathbf{B}_3$	$= z_2\mathbf{a}_1 + z_2\mathbf{a}_2$	$=$	$cz_2\hat{\mathbf{z}}$	(4e)	Si II
$\mathbf{B}_4$	$= -z_2\mathbf{a}_1 - z_2\mathbf{a}_2$	$=$	$-cz_2\hat{\mathbf{z}}$	(4e)	Si II
$\mathbf{B}_5$	$= z_3\mathbf{a}_1 + z_3\mathbf{a}_2$	$=$	$cz_3\hat{\mathbf{z}}$	(4e)	Tb I
$\mathbf{B}_6$	$= -z_3\mathbf{a}_1 - z_3\mathbf{a}_2$	$=$	$-cz_3\hat{\mathbf{z}}$	(4e)	Tb I
$\mathbf{B}_7$	$= x_4\mathbf{a}_1 + x_4\mathbf{a}_2 + 2x_4\mathbf{a}_3$	$=$	$ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}}$	(8h)	In I
$\mathbf{B}_8$	$= -x_4\mathbf{a}_1 - x_4\mathbf{a}_2 - 2x_4\mathbf{a}_3$	$=$	$-ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}}$	(8h)	In I
$\mathbf{B}_9$	$= x_4\mathbf{a}_1 - x_4\mathbf{a}_2$	$=$	$-ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}}$	(8h)	In I
$\mathbf{B}_{10}$	$= -x_4\mathbf{a}_1 + x_4\mathbf{a}_2$	$=$	$ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}}$	(8h)	In I
$\mathbf{B}_{11}$	$= x_5\mathbf{a}_1 + x_5\mathbf{a}_2 + 2x_5\mathbf{a}_3$	$=$	$ax_5\hat{\mathbf{x}} + ax_5\hat{\mathbf{y}}$	(8h)	Tb II
$\mathbf{B}_{12}$	$= -x_5\mathbf{a}_1 - x_5\mathbf{a}_2 - 2x_5\mathbf{a}_3$	$=$	$-ax_5\hat{\mathbf{x}} - ax_5\hat{\mathbf{y}}$	(8h)	Tb II
$\mathbf{B}_{13}$	$= x_5\mathbf{a}_1 - x_5\mathbf{a}_2$	$=$	$-ax_5\hat{\mathbf{x}} + ax_5\hat{\mathbf{y}}$	(8h)	Tb II
$\mathbf{B}_{14}$	$= -x_5\mathbf{a}_1 + x_5\mathbf{a}_2$	$=$	$ax_5\hat{\mathbf{x}} - ax_5\hat{\mathbf{y}}$	(8h)	Tb II
$\mathbf{B}_{15}$	$= x_6\mathbf{a}_2 + x_6\mathbf{a}_3$	$=$	$ax_6\hat{\mathbf{x}}$	(8i)	Si III
$\mathbf{B}_{16}$	$= -x_6\mathbf{a}_2 - x_6\mathbf{a}_3$	$=$	$-ax_6\hat{\mathbf{x}}$	(8i)	Si III
$\mathbf{B}_{17}$	$= x_6\mathbf{a}_1 + x_6\mathbf{a}_3$	$=$	$ax_6\hat{\mathbf{y}}$	(8i)	Si III
$\mathbf{B}_{18}$	$= -x_6\mathbf{a}_1 - x_6\mathbf{a}_3$	$=$	$-ax_6\hat{\mathbf{y}}$	(8i)	Si III

$\mathbf{B}_{19}$	$=$	$(x_7 + z_7) \mathbf{a}_1 + (x_7 + z_7) \mathbf{a}_2 +$	$=$	$ax_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(16m)	In II
		$2x_7 \mathbf{a}_3$				
$\mathbf{B}_{20}$	$=$	$-(x_7 - z_7) \mathbf{a}_1 - (x_7 - z_7) \mathbf{a}_2 -$	$=$	$-ax_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(16m)	In II
		$2x_7 \mathbf{a}_3$				
$\mathbf{B}_{21}$	$=$	$(x_7 + z_7) \mathbf{a}_1 - (x_7 - z_7) \mathbf{a}_2$	$=$	$-ax_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(16m)	In II
$\mathbf{B}_{22}$	$=$	$-(x_7 - z_7) \mathbf{a}_1 + (x_7 + z_7) \mathbf{a}_2$	$=$	$ax_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(16m)	In II
$\mathbf{B}_{23}$	$=$	$(x_7 - z_7) \mathbf{a}_1 - (x_7 + z_7) \mathbf{a}_2$	$=$	$-ax_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(16m)	In II
$\mathbf{B}_{24}$	$=$	$-(x_7 + z_7) \mathbf{a}_1 + (x_7 - z_7) \mathbf{a}_2$	$=$	$ax_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(16m)	In II
$\mathbf{B}_{25}$	$=$	$(x_7 - z_7) \mathbf{a}_1 + (x_7 - z_7) \mathbf{a}_2 +$	$=$	$ax_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(16m)	In II
		$2x_7 \mathbf{a}_3$				
$\mathbf{B}_{26}$	$=$	$-(x_7 + z_7) \mathbf{a}_1 - (x_7 + z_7) \mathbf{a}_2 -$	$=$	$-ax_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(16m)	In II
		$2x_7 \mathbf{a}_3$				
$\mathbf{B}_{27}$	$=$	$(y_8 + z_8) \mathbf{a}_1 + z_8 \mathbf{a}_2 + y_8 \mathbf{a}_3$	$=$	$ay_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(16n)	Tb III
$\mathbf{B}_{28}$	$=$	$-(y_8 - z_8) \mathbf{a}_1 + z_8 \mathbf{a}_2 - y_8 \mathbf{a}_3$	$=$	$-ay_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(16n)	Tb III
$\mathbf{B}_{29}$	$=$	$z_8 \mathbf{a}_1 - (y_8 - z_8) \mathbf{a}_2 - y_8 \mathbf{a}_3$	$=$	$-ay_8 \hat{\mathbf{x}} + cz_8 \hat{\mathbf{z}}$	(16n)	Tb III
$\mathbf{B}_{30}$	$=$	$z_8 \mathbf{a}_1 + (y_8 + z_8) \mathbf{a}_2 + y_8 \mathbf{a}_3$	$=$	$ay_8 \hat{\mathbf{x}} + cz_8 \hat{\mathbf{z}}$	(16n)	Tb III
$\mathbf{B}_{31}$	$=$	$(y_8 - z_8) \mathbf{a}_1 - z_8 \mathbf{a}_2 + y_8 \mathbf{a}_3$	$=$	$ay_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	(16n)	Tb III
$\mathbf{B}_{32}$	$=$	$-(y_8 + z_8) \mathbf{a}_1 - z_8 \mathbf{a}_2 - y_8 \mathbf{a}_3$	$=$	$-ay_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	(16n)	Tb III
$\mathbf{B}_{33}$	$=$	$-z_8 \mathbf{a}_1 + (y_8 - z_8) \mathbf{a}_2 + y_8 \mathbf{a}_3$	$=$	$ay_8 \hat{\mathbf{x}} - cz_8 \hat{\mathbf{z}}$	(16n)	Tb III
$\mathbf{B}_{34}$	$=$	$-z_8 \mathbf{a}_1 - (y_8 + z_8) \mathbf{a}_2 - y_8 \mathbf{a}_3$	$=$	$-ay_8 \hat{\mathbf{x}} - cz_8 \hat{\mathbf{z}}$	(16n)	Tb III
$\mathbf{B}_{35}$	$=$	$(y_9 + z_9) \mathbf{a}_1 + z_9 \mathbf{a}_2 + y_9 \mathbf{a}_3$	$=$	$ay_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(16n)	Tb IV
$\mathbf{B}_{36}$	$=$	$-(y_9 - z_9) \mathbf{a}_1 + z_9 \mathbf{a}_2 - y_9 \mathbf{a}_3$	$=$	$-ay_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(16n)	Tb IV
$\mathbf{B}_{37}$	$=$	$z_9 \mathbf{a}_1 - (y_9 - z_9) \mathbf{a}_2 - y_9 \mathbf{a}_3$	$=$	$-ay_9 \hat{\mathbf{x}} + cz_9 \hat{\mathbf{z}}$	(16n)	Tb IV
$\mathbf{B}_{38}$	$=$	$z_9 \mathbf{a}_1 + (y_9 + z_9) \mathbf{a}_2 + y_9 \mathbf{a}_3$	$=$	$ay_9 \hat{\mathbf{x}} + cz_9 \hat{\mathbf{z}}$	(16n)	Tb IV
$\mathbf{B}_{39}$	$=$	$(y_9 - z_9) \mathbf{a}_1 - z_9 \mathbf{a}_2 + y_9 \mathbf{a}_3$	$=$	$ay_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}}$	(16n)	Tb IV
$\mathbf{B}_{40}$	$=$	$-(y_9 + z_9) \mathbf{a}_1 - z_9 \mathbf{a}_2 - y_9 \mathbf{a}_3$	$=$	$-ay_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}}$	(16n)	Tb IV
$\mathbf{B}_{41}$	$=$	$-z_9 \mathbf{a}_1 + (y_9 - z_9) \mathbf{a}_2 + y_9 \mathbf{a}_3$	$=$	$ay_9 \hat{\mathbf{x}} - cz_9 \hat{\mathbf{z}}$	(16n)	Tb IV
$\mathbf{B}_{42}$	$=$	$-z_9 \mathbf{a}_1 - (y_9 + z_9) \mathbf{a}_2 - y_9 \mathbf{a}_3$	$=$	$-ay_9 \hat{\mathbf{x}} - cz_9 \hat{\mathbf{z}}$	(16n)	Tb IV

References

- [1] Y. Tyvanchuk, R. Duraj, T. Jaworska-Goław, S. Baran, Y. M. Kalychak, J. Przewoźnik, and A. Szytuła, *Structural chemistry and magnetic properties of $R_{11}M_4In_6$ ($R = Gd, Tb, Dy, Ho, Er, Y$; $M = Si, Ge$) compounds*, Intermetallics **25**, 18–26 (2012), doi:10.1016/j.intermet.2012.02.005.

Found in

- [1] *Inorganic Crystal Structure Database*. Entry 184236 (Tb11Si4In6).

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