

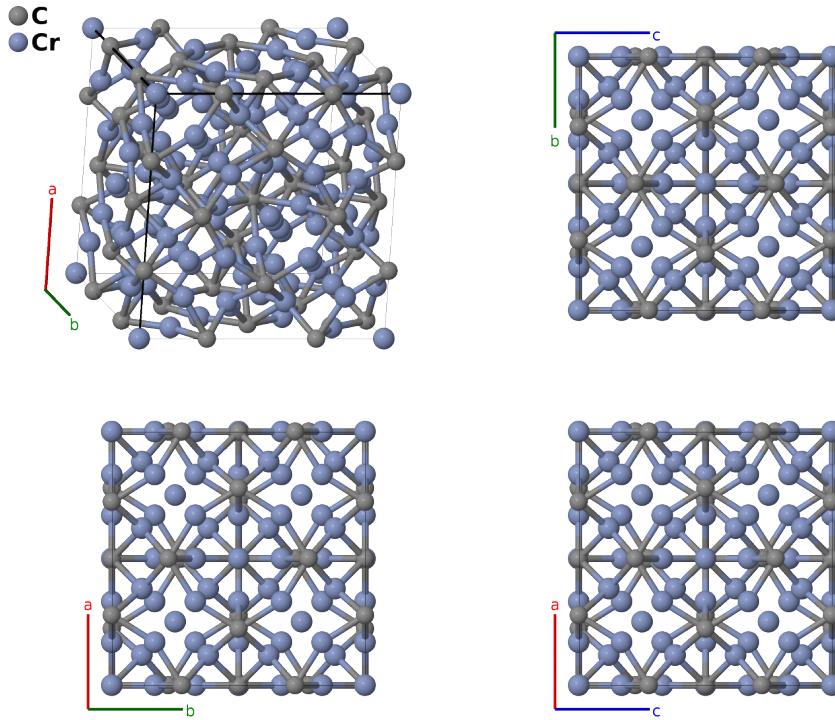
Cr_{23}C_6 ($D8_4$) Structure: A6B23_cF116_225_e_acfh-001

This structure originally had the label A6B23_cF116_225_e_acfh. Calls to that address will be redirected here.

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<https://aflow.org/p/EY4X>

https://aflow.org/p/A6B23_cF116_225_e_acfh-001



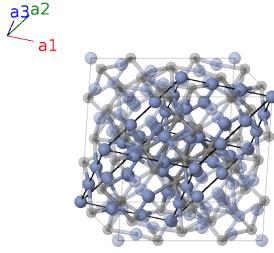
| | |
|------------------------------------|--|
| Prototype | C_6Cr_{23} |
| AFLOW prototype label | A6B23_cF116_225_e_acfh-001 |
| Strukturbericht designation | $D8_4$ |
| ICSD | 2837 |
| Pearson symbol | cF116 |
| Space group number | 225 |
| Space group symbol | $Fm\bar{3}m$ |
| AFLOW prototype command | <code>aflow --proto=A6B23_cF116_225_e_acfh-001 --params=a, x3, x4, y5</code> |

Other compounds with this structure

Mn₂₃C₆, Co₂₁Sn₂B₆, Fe₂₁Mo₂C₆, Fe₂₁W₂C₆, Ni₂₀Mg₃B₆, Ni₂₁In₂B₆, Ni₂₁Sn₂B₆

Face-centered Cubic primitive vectors

$$\begin{aligned}
 \mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}} \\
 \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{z}} \\
 \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}}
 \end{aligned}$$



Basis vectors

| | Lattice coordinates | Cartesian coordinates | Wyckoff position | Atom type |
|-------------------|---|--|------------------|-----------|
| \mathbf{B}_1 | = 0 | = 0 | (4a) | Cr I |
| \mathbf{B}_2 | = $\frac{1}{4}\mathbf{a}_1 + \frac{1}{4}\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$ | = $\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{4}a\hat{\mathbf{z}}$ | (8c) | Cr II |
| \mathbf{B}_3 | = $\frac{3}{4}\mathbf{a}_1 + \frac{3}{4}\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$ | = $\frac{3}{4}a\hat{\mathbf{x}} + \frac{3}{4}a\hat{\mathbf{y}} + \frac{3}{4}a\hat{\mathbf{z}}$ | (8c) | Cr II |
| \mathbf{B}_4 | = $-x_3\mathbf{a}_1 + x_3\mathbf{a}_2 + x_3\mathbf{a}_3$ | = $ax_3\hat{\mathbf{x}}$ | (24e) | C I |
| \mathbf{B}_5 | = $x_3\mathbf{a}_1 - x_3\mathbf{a}_2 - x_3\mathbf{a}_3$ | = $-ax_3\hat{\mathbf{x}}$ | (24e) | C I |
| \mathbf{B}_6 | = $x_3\mathbf{a}_1 - x_3\mathbf{a}_2 + x_3\mathbf{a}_3$ | = $ax_3\hat{\mathbf{y}}$ | (24e) | C I |
| \mathbf{B}_7 | = $-x_3\mathbf{a}_1 + x_3\mathbf{a}_2 - x_3\mathbf{a}_3$ | = $-ax_3\hat{\mathbf{y}}$ | (24e) | C I |
| \mathbf{B}_8 | = $x_3\mathbf{a}_1 + x_3\mathbf{a}_2 - x_3\mathbf{a}_3$ | = $ax_3\hat{\mathbf{z}}$ | (24e) | C I |
| \mathbf{B}_9 | = $-x_3\mathbf{a}_1 - x_3\mathbf{a}_2 + x_3\mathbf{a}_3$ | = $-ax_3\hat{\mathbf{z}}$ | (24e) | C I |
| \mathbf{B}_{10} | = $x_4\mathbf{a}_1 + x_4\mathbf{a}_2 + x_4\mathbf{a}_3$ | = $ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} + ax_4\hat{\mathbf{z}}$ | (32f) | Cr III |
| \mathbf{B}_{11} | = $x_4\mathbf{a}_1 + x_4\mathbf{a}_2 - 3x_4\mathbf{a}_3$ | = $-ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} + ax_4\hat{\mathbf{z}}$ | (32f) | Cr III |
| \mathbf{B}_{12} | = $x_4\mathbf{a}_1 - 3x_4\mathbf{a}_2 + x_4\mathbf{a}_3$ | = $-ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} - ax_4\hat{\mathbf{z}}$ | (32f) | Cr III |
| \mathbf{B}_{13} | = $-3x_4\mathbf{a}_1 + x_4\mathbf{a}_2 + x_4\mathbf{a}_3$ | = $ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} - ax_4\hat{\mathbf{z}}$ | (32f) | Cr III |
| \mathbf{B}_{14} | = $-x_4\mathbf{a}_1 - x_4\mathbf{a}_2 + 3x_4\mathbf{a}_3$ | = $ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} - ax_4\hat{\mathbf{z}}$ | (32f) | Cr III |
| \mathbf{B}_{15} | = $-x_4\mathbf{a}_1 - x_4\mathbf{a}_2 - x_4\mathbf{a}_3$ | = $-ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} - ax_4\hat{\mathbf{z}}$ | (32f) | Cr III |
| \mathbf{B}_{16} | = $-x_4\mathbf{a}_1 + 3x_4\mathbf{a}_2 - x_4\mathbf{a}_3$ | = $ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} + ax_4\hat{\mathbf{z}}$ | (32f) | Cr III |
| \mathbf{B}_{17} | = $3x_4\mathbf{a}_1 - x_4\mathbf{a}_2 - x_4\mathbf{a}_3$ | = $-ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} + ax_4\hat{\mathbf{z}}$ | (32f) | Cr III |
| \mathbf{B}_{18} | = $2y_5\mathbf{a}_1$ | = $ay_5\hat{\mathbf{y}} + ay_5\hat{\mathbf{z}}$ | (48h) | Cr IV |
| \mathbf{B}_{19} | = $2y_5\mathbf{a}_2 - 2y_5\mathbf{a}_3$ | = $-ay_5\hat{\mathbf{y}} + ay_5\hat{\mathbf{z}}$ | (48h) | Cr IV |
| \mathbf{B}_{20} | = $-2y_5\mathbf{a}_2 + 2y_5\mathbf{a}_3$ | = $ay_5\hat{\mathbf{y}} - ay_5\hat{\mathbf{z}}$ | (48h) | Cr IV |
| \mathbf{B}_{21} | = $-2y_5\mathbf{a}_1$ | = $-ay_5\hat{\mathbf{y}} - ay_5\hat{\mathbf{z}}$ | (48h) | Cr IV |
| \mathbf{B}_{22} | = $2y_5\mathbf{a}_2$ | = $ay_5\hat{\mathbf{x}} + ay_5\hat{\mathbf{z}}$ | (48h) | Cr IV |
| \mathbf{B}_{23} | = $-2y_5\mathbf{a}_1 + 2y_5\mathbf{a}_3$ | = $ay_5\hat{\mathbf{x}} - ay_5\hat{\mathbf{z}}$ | (48h) | Cr IV |
| \mathbf{B}_{24} | = $2y_5\mathbf{a}_1 - 2y_5\mathbf{a}_3$ | = $-ay_5\hat{\mathbf{x}} + ay_5\hat{\mathbf{z}}$ | (48h) | Cr IV |
| \mathbf{B}_{25} | = $-2y_5\mathbf{a}_2$ | = $-ay_5\hat{\mathbf{x}} - ay_5\hat{\mathbf{z}}$ | (48h) | Cr IV |
| \mathbf{B}_{26} | = $2y_5\mathbf{a}_3$ | = $ay_5\hat{\mathbf{x}} + ay_5\hat{\mathbf{y}}$ | (48h) | Cr IV |
| \mathbf{B}_{27} | = $2y_5\mathbf{a}_1 - 2y_5\mathbf{a}_2$ | = $-ay_5\hat{\mathbf{x}} + ay_5\hat{\mathbf{y}}$ | (48h) | Cr IV |
| \mathbf{B}_{28} | = $-2y_5\mathbf{a}_1 + 2y_5\mathbf{a}_2$ | = $ay_5\hat{\mathbf{x}} - ay_5\hat{\mathbf{y}}$ | (48h) | Cr IV |
| \mathbf{B}_{29} | = $-2y_5\mathbf{a}_3$ | = $-ay_5\hat{\mathbf{x}} - ay_5\hat{\mathbf{y}}$ | (48h) | Cr IV |

References

- [1] A. L. Bowman, G. P. Arnold, E. K. Storms, and N. G. Nereson, *The crystal structure of Cr₂₃C₆*, Acta Crystallogr. Sect. B **28**, 3102–3103 (1972), doi:10.1107/S0567740872007526.