

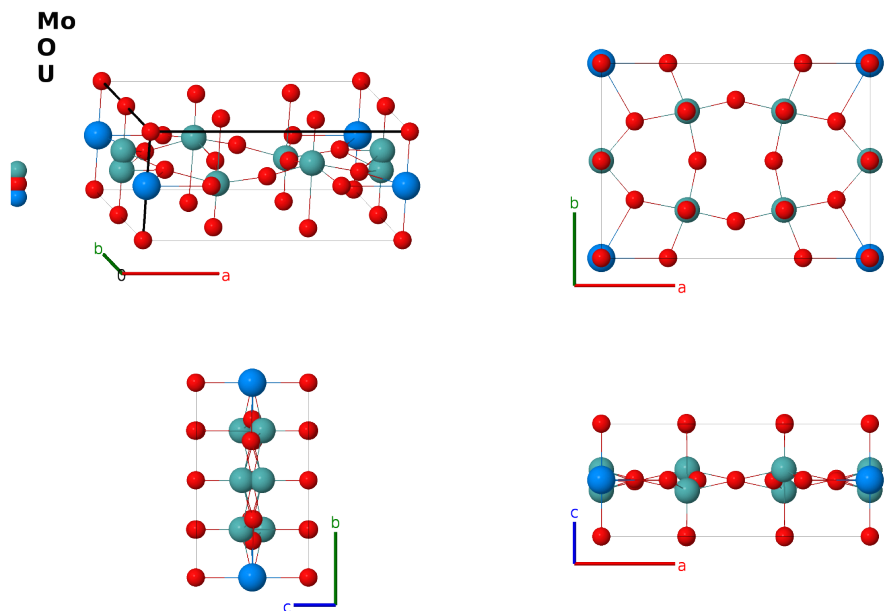
Orthorhombic $\text{UMo}_5\text{O}_{16}$ Structure: A6B16C_oP23_16_su_acjlp2u_d-001

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<https://aflow.org/prototype-encyclopedia/CAAV>

https://aflow.org/prototype-encyclopedia/A6B16C_oP23_16_su_acjlp2u_d-001



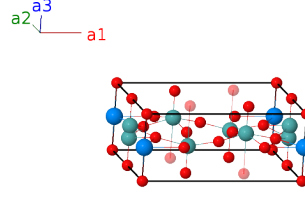
Prototype	$\text{Mo}_5\text{O}_{16}\text{U}$
AFLOW prototype label	A6B16C_oP23_16_su_acjlp2u_d-001
ICSD	80164
CCDC	1640388
Pearson symbol	oP23
Space group number	16
Space group symbol	$P222$
AFLOW prototype command	<pre>aflow --proto=A6B16C_oP23_16_su_acjlp2u_d-001 --params=a, b/a, c/a, x4, x5, y6, z7, x8, y8, z8, x9, y9, z9, x10, y10, z10</pre>

- The Mo-I (2s) site is occupied only 50% of the time. For first-principles calculations it may be possible to replace the atoms on the (2s) site by a single atom at the (1g) site.
- (Tabachenko, 1995) also found evidence of a $\text{U}_{0.75}\text{Mo}_5\text{O}_{16}$ structure, where the uranium (1d) site contains 25% vacancies, and the Mo-II (4u) site is split into two partially occupied (4u) sites.

- (Tabachenko, 1995) also found a monoclinic $\text{UMo}_5\text{O}_{16}$ structure, where the atoms are completely ordered.

Simple Orthorhombic primitive vectors

$$\begin{aligned} \mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= b \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}} \end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= 0$	$=$	0	(1a)	U I
$\mathbf{B}_2$	$= \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2} b \hat{\mathbf{y}}$	(1c)	O I
$\mathbf{B}_3$	$= \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} b \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(1g)	O II
$\mathbf{B}_4$	$= x_4 \mathbf{a}_1$	$=$	$a x_4 \hat{\mathbf{x}}$	(2i)	O III
$\mathbf{B}_5$	$= -x_4 \mathbf{a}_1$	$=$	$-a x_4 \hat{\mathbf{x}}$	(2i)	O III
$\mathbf{B}_6$	$= x_5 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	$=$	$a x_5 \hat{\mathbf{x}} + \frac{1}{2} c \hat{\mathbf{z}}$	(2j)	O IV
$\mathbf{B}_7$	$= -x_5 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	$=$	$-a x_5 \hat{\mathbf{x}} + \frac{1}{2} c \hat{\mathbf{z}}$	(2j)	O IV
$\mathbf{B}_8$	$= y_6 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$b y_6 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(2n)	Mo I
$\mathbf{B}_9$	$= -y_6 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-b y_6 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(2n)	Mo I
$\mathbf{B}_{10}$	$= \frac{1}{2} \mathbf{a}_1 + z_7 \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + c z_7 \hat{\mathbf{z}}$	(2r)	O V
$\mathbf{B}_{11}$	$= \frac{1}{2} \mathbf{a}_1 - z_7 \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - c z_7 \hat{\mathbf{z}}$	(2r)	O V
$\mathbf{B}_{12}$	$= x_8 \mathbf{a}_1 + y_8 \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$a x_8 \hat{\mathbf{x}} + b y_8 \hat{\mathbf{y}} + c z_8 \hat{\mathbf{z}}$	(4u)	Mo II
$\mathbf{B}_{13}$	$= -x_8 \mathbf{a}_1 - y_8 \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$-a x_8 \hat{\mathbf{x}} - b y_8 \hat{\mathbf{y}} + c z_8 \hat{\mathbf{z}}$	(4u)	Mo II
$\mathbf{B}_{14}$	$= -x_8 \mathbf{a}_1 + y_8 \mathbf{a}_2 - z_8 \mathbf{a}_3$	$=$	$-a x_8 \hat{\mathbf{x}} + b y_8 \hat{\mathbf{y}} - c z_8 \hat{\mathbf{z}}$	(4u)	Mo II
$\mathbf{B}_{15}$	$= x_8 \mathbf{a}_1 - y_8 \mathbf{a}_2 - z_8 \mathbf{a}_3$	$=$	$a x_8 \hat{\mathbf{x}} - b y_8 \hat{\mathbf{y}} - c z_8 \hat{\mathbf{z}}$	(4u)	Mo II
$\mathbf{B}_{16}$	$= x_9 \mathbf{a}_1 + y_9 \mathbf{a}_2 + z_9 \mathbf{a}_3$	$=$	$a x_9 \hat{\mathbf{x}} + b y_9 \hat{\mathbf{y}} + c z_9 \hat{\mathbf{z}}$	(4u)	O VI
$\mathbf{B}_{17}$	$= -x_9 \mathbf{a}_1 - y_9 \mathbf{a}_2 + z_9 \mathbf{a}_3$	$=$	$-a x_9 \hat{\mathbf{x}} - b y_9 \hat{\mathbf{y}} + c z_9 \hat{\mathbf{z}}$	(4u)	O VI
$\mathbf{B}_{18}$	$= -x_9 \mathbf{a}_1 + y_9 \mathbf{a}_2 - z_9 \mathbf{a}_3$	$=$	$-a x_9 \hat{\mathbf{x}} + b y_9 \hat{\mathbf{y}} - c z_9 \hat{\mathbf{z}}$	(4u)	O VI
$\mathbf{B}_{19}$	$= x_9 \mathbf{a}_1 - y_9 \mathbf{a}_2 - z_9 \mathbf{a}_3$	$=$	$a x_9 \hat{\mathbf{x}} - b y_9 \hat{\mathbf{y}} - c z_9 \hat{\mathbf{z}}$	(4u)	O VI
$\mathbf{B}_{20}$	$= x_{10} \mathbf{a}_1 + y_{10} \mathbf{a}_2 + z_{10} \mathbf{a}_3$	$=$	$a x_{10} \hat{\mathbf{x}} + b y_{10} \hat{\mathbf{y}} + c z_{10} \hat{\mathbf{z}}$	(4u)	O VII
$\mathbf{B}_{21}$	$= -x_{10} \mathbf{a}_1 - y_{10} \mathbf{a}_2 + z_{10} \mathbf{a}_3$	$=$	$-a x_{10} \hat{\mathbf{x}} - b y_{10} \hat{\mathbf{y}} + c z_{10} \hat{\mathbf{z}}$	(4u)	O VII
$\mathbf{B}_{22}$	$= -x_{10} \mathbf{a}_1 + y_{10} \mathbf{a}_2 - z_{10} \mathbf{a}_3$	$=$	$-a x_{10} \hat{\mathbf{x}} + b y_{10} \hat{\mathbf{y}} - c z_{10} \hat{\mathbf{z}}$	(4u)	O VII
$\mathbf{B}_{23}$	$= x_{10} \mathbf{a}_1 - y_{10} \mathbf{a}_2 - z_{10} \mathbf{a}_3$	$=$	$a x_{10} \hat{\mathbf{x}} - b y_{10} \hat{\mathbf{y}} - c z_{10} \hat{\mathbf{z}}$	(4u)	O VII

References

- [1] V. V. Tabachenko, O. G. D'yachenko, and M. Sundberg, *The crystal structures of $\text{UMo}_5\text{O}_{16}$ and $\text{U}_{0.75}\text{Mo}_5\text{O}_{16}$ studies by X-ray diffraction and high resolution electron microscopy*, Eur. J. Solid State Inorg. Chem. **32**, 1137–1149 (1995).

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