

# Rhombohedral Al<sub>5</sub>Mo Structure:

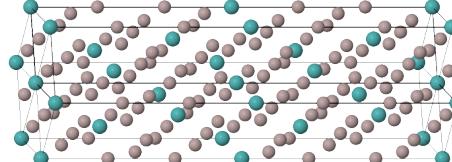
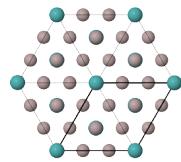
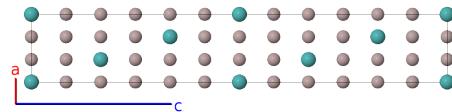
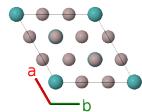
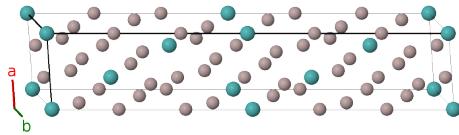
## A5B\_hR12\_167\_ce\_b-001

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<https://aflow.org/p/584Z>

[https://aflow.org/p/A5B\\_hR12\\_167\\_ce\\_b-001](https://aflow.org/p/A5B_hR12_167_ce_b-001)

Al  
Mo



**Prototype** Al<sub>5</sub>Mo

**AFLOW prototype label** A5B\_hR12\_167\_ce\_b-001

**ICSD** 105520

**Pearson symbol** hR12

**Space group number** 167

**Space group symbol**  $R\bar{3}c$

**AFLOW prototype command** `aflow --proto=A5B_hR12_167_ce_b-001 --params=a, c/a, x2, x3`

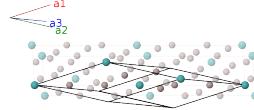
- Al<sub>5</sub>Mo is known to have three phases (Schuster, 1991):

- Below 650K it is in a rhombohedral structure, Al<sub>5</sub>Mo(r) (this structure).
- Between 650K and 750-800K it is in a trigonal structure, Al<sub>5</sub>Mo(h').
- Above 750-800K up to 846K it is in the Al<sub>5</sub>W structure.

- Hexagonal settings of this structure can be obtained with the option `--hex`.

## Rhombohedral primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} + \frac{1}{3}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{\sqrt{3}}a\hat{\mathbf{y}} + \frac{1}{3}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= -\frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} + \frac{1}{3}c\hat{\mathbf{z}}\end{aligned}$$



## Basis vectors

	Lattice coordinates	=	Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	0	=	0	(2b)	Mo I
$\mathbf{B}_2$	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{2}c\hat{\mathbf{z}}$	(2b)	Mo I
$\mathbf{B}_3$	$x_2\mathbf{a}_1 + x_2\mathbf{a}_2 + x_2\mathbf{a}_3$	=	$cx_2\hat{\mathbf{z}}$	(4c)	Al I
$\mathbf{B}_4$	$-(x_2 - \frac{1}{2})\mathbf{a}_1 - (x_2 - \frac{1}{2})\mathbf{a}_2 - (x_2 - \frac{1}{2})\mathbf{a}_3$	=	$-c(x_2 - \frac{1}{2})\hat{\mathbf{z}}$	(4c)	Al I
$\mathbf{B}_5$	$-x_2\mathbf{a}_1 - x_2\mathbf{a}_2 - x_2\mathbf{a}_3$	=	$-cx_2\hat{\mathbf{z}}$	(4c)	Al I
$\mathbf{B}_6$	$(x_2 + \frac{1}{2})\mathbf{a}_1 + (x_2 + \frac{1}{2})\mathbf{a}_2 + (x_2 + \frac{1}{2})\mathbf{a}_3$	=	$c(x_2 + \frac{1}{2})\hat{\mathbf{z}}$	(4c)	Al I
$\mathbf{B}_7$	$x_3\mathbf{a}_1 - (x_3 - \frac{1}{2})\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$	=	$\frac{1}{8}a(4x_3 - 1)\hat{\mathbf{x}} - \frac{\sqrt{3}}{8}a(4x_3 - 1)\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(6e)	Al II
$\mathbf{B}_8$	$\frac{1}{4}\mathbf{a}_1 + x_3\mathbf{a}_2 - (x_3 - \frac{1}{2})\mathbf{a}_3$	=	$\frac{1}{8}a(4x_3 - 1)\hat{\mathbf{x}} + \frac{\sqrt{3}}{8}a(4x_3 - 1)\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(6e)	Al II
$\mathbf{B}_9$	$-(x_3 - \frac{1}{2})\mathbf{a}_1 + \frac{1}{4}\mathbf{a}_2 + x_3\mathbf{a}_3$	=	$-a(x_3 - \frac{1}{4})\hat{\mathbf{x}} + \frac{1}{4}c\hat{\mathbf{z}}$	(6e)	Al II
$\mathbf{B}_{10}$	$-x_3\mathbf{a}_1 + (x_3 + \frac{1}{2})\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$	=	$-\frac{1}{8}a(4x_3 + 3)\hat{\mathbf{x}} + \frac{\sqrt{3}}{24}a(12x_3 + 1)\hat{\mathbf{y}} + \frac{5}{12}c\hat{\mathbf{z}}$	(6e)	Al II
$\mathbf{B}_{11}$	$\frac{3}{4}\mathbf{a}_1 - x_3\mathbf{a}_2 + (x_3 + \frac{1}{2})\mathbf{a}_3$	=	$-\frac{1}{8}a(4x_3 - 1)\hat{\mathbf{x}} - \frac{\sqrt{3}}{24}a(12x_3 + 5)\hat{\mathbf{y}} + \frac{5}{12}c\hat{\mathbf{z}}$	(6e)	Al II
$\mathbf{B}_{12}$	$(x_3 + \frac{1}{2})\mathbf{a}_1 + \frac{3}{4}\mathbf{a}_2 - x_3\mathbf{a}_3$	=	$a(x_3 + \frac{1}{4})\hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} + \frac{5}{12}c\hat{\mathbf{z}}$	(6e)	Al II

## References

- [1] J. C. Schuster and H. Ipser, *The Al-Al<sub>8</sub>Mo<sub>3</sub> section of the binary system aluminum-molybdenum*, Metall. Trans. A **22**, 1729–1736 (1991), doi:10.1007/BF02646496.