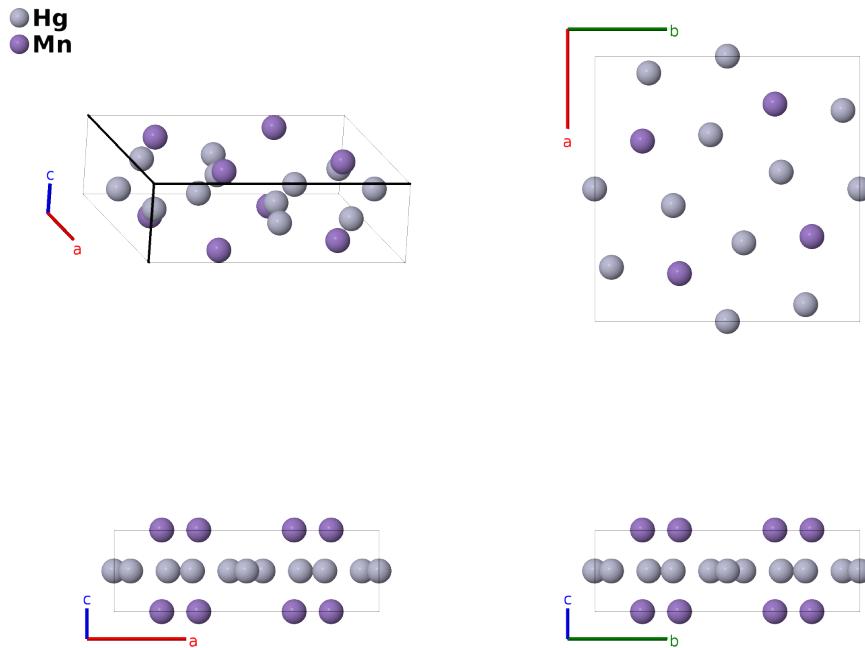


Mn₂Hg₅ Structure: A5B2_tP14_127_cj_g-001

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<https://aflow.org/p/BAHM>

https://aflow.org/p/A5B2_tP14_127_cj_g-001



Prototype	Hg ₅ Mn ₂
AFLOW prototype label	A5B2_tP14_127_cj_g-001
ICSD	104324
Pearson symbol	tP14
Space group number	127
Space group symbol	<i>P</i> 4/ <i>mbm</i>
AFLOW prototype command	<code>aflow --proto=A5B2_tP14_127_cj_g-001 --params=a, c/a, x₂, x₃, y₃</code>

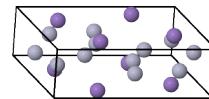
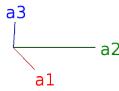
Other compounds with this structure

Ag₂Hg₅, Hf₂In₅, Li₂Sn₅, Mn₂Ga₅, Pd₂Hg₅, Ti₂In₅, V₂Ga₅, W₂Ga₅, Ti₃In₄

- We shifted the origin of the *c*-axis by *c*/2 from that used by (de Wet, 1961).

Simple Tetragonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= a \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates	=	Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$\frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$\frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(2c)	Hg I
\mathbf{B}_2	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	=	$\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(2c)	Hg I
\mathbf{B}_3	$x_2 \mathbf{a}_1 + (x_2 + \frac{1}{2}) \mathbf{a}_2$	=	$ax_2 \hat{\mathbf{x}} + a(x_2 + \frac{1}{2}) \hat{\mathbf{y}}$	(4g)	Mn I
\mathbf{B}_4	$-x_2 \mathbf{a}_1 - (x_2 - \frac{1}{2}) \mathbf{a}_2$	=	$-ax_2 \hat{\mathbf{x}} - a(x_2 - \frac{1}{2}) \hat{\mathbf{y}}$	(4g)	Mn I
\mathbf{B}_5	$-(x_2 - \frac{1}{2}) \mathbf{a}_1 + x_2 \mathbf{a}_2$	=	$-a(x_2 - \frac{1}{2}) \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}}$	(4g)	Mn I
\mathbf{B}_6	$(x_2 + \frac{1}{2}) \mathbf{a}_1 - x_2 \mathbf{a}_2$	=	$a(x_2 + \frac{1}{2}) \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}}$	(4g)	Mn I
\mathbf{B}_7	$x_3 \mathbf{a}_1 + y_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$ax_3 \hat{\mathbf{x}} + ay_3 \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8j)	Hg II
\mathbf{B}_8	$-x_3 \mathbf{a}_1 - y_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$-ax_3 \hat{\mathbf{x}} - ay_3 \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8j)	Hg II
\mathbf{B}_9	$-y_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$-ay_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8j)	Hg II
\mathbf{B}_{10}	$y_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$ay_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8j)	Hg II
\mathbf{B}_{11}	$-(x_3 - \frac{1}{2}) \mathbf{a}_1 + (y_3 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$-a(x_3 - \frac{1}{2}) \hat{\mathbf{x}} + a(y_3 + \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8j)	Hg II
\mathbf{B}_{12}	$(x_3 + \frac{1}{2}) \mathbf{a}_1 - (y_3 - \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$a(x_3 + \frac{1}{2}) \hat{\mathbf{x}} - a(y_3 - \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8j)	Hg II
\mathbf{B}_{13}	$(y_3 + \frac{1}{2}) \mathbf{a}_1 + (x_3 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$a(y_3 + \frac{1}{2}) \hat{\mathbf{x}} + a(x_3 + \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8j)	Hg II
\mathbf{B}_{14}	$-(y_3 - \frac{1}{2}) \mathbf{a}_1 - (x_3 - \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$-a(y_3 - \frac{1}{2}) \hat{\mathbf{x}} - a(x_3 - \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8j)	Hg II

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