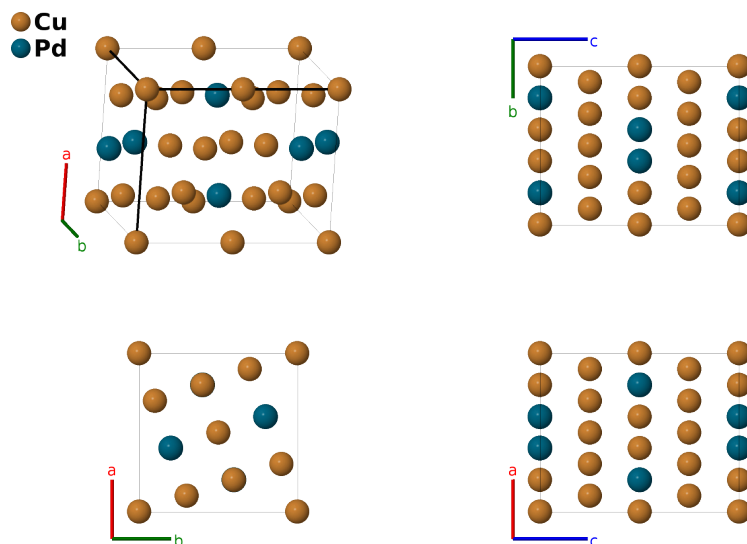


# Cu<sub>4</sub>Pd Structure: A4B\_tP20\_84\_afjk\_j-001

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<https://aflow.org/p/L3AR>

[https://aflow.org/p/A4B\\_tP20\\_84\\_afjk\\_j-001](https://aflow.org/p/A4B_tP20_84_afjk_j-001)

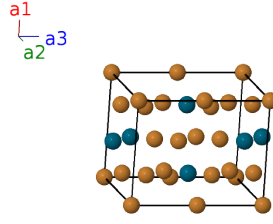


Prototype	Cu <sub>4</sub> Pd
AFLOW prototype label	A4B_tP20_84_afjk_j-001
ICSD	103087
Pearson symbol	tP20
Space group number	84
Space group symbol	$P4_2/m$
AFLOW prototype command	<pre>aflow --proto=A4B_tP20_84_afjk_j-001       --params=a, c/a, x<sub>3</sub>, y<sub>3</sub>, x<sub>4</sub>, y<sub>4</sub>, x<sub>5</sub>, y<sub>5</sub>, z<sub>5</sub></pre>

- Above 476°C Cu<sub>4</sub>Pd is completely disordered, with the atoms placed randomly on the sites of the face-centered cubic (A1) structure. Below that temperature it takes on this ordered tetragonal structure. (Geisler, 1954).
- The value of 0.25 for  $z_5$  is not given in (Geisler, 1954), but we infer it from the description of the cell as a decoration of the face-centered cubic lattice.

## Simple Tetragonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= a \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}}\end{aligned}$$



## Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$0$	$=$	$0$	(2a)	Cu I
$\mathbf{B}_2$	$\frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} c \hat{\mathbf{z}}$	(2a)	Cu I
$\mathbf{B}_3$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}}$	(2f)	Cu II
$\mathbf{B}_4$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{3}{4} c \hat{\mathbf{z}}$	(2f)	Cu II
$\mathbf{B}_5$	$x_3 \mathbf{a}_1 + y_3 \mathbf{a}_2$	$=$	$a x_3 \hat{\mathbf{x}} + a y_3 \hat{\mathbf{y}}$	(4j)	Cu III
$\mathbf{B}_6$	$-x_3 \mathbf{a}_1 - y_3 \mathbf{a}_2$	$=$	$-a x_3 \hat{\mathbf{x}} - a y_3 \hat{\mathbf{y}}$	(4j)	Cu III
$\mathbf{B}_7$	$-y_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-a y_3 \hat{\mathbf{x}} + a x_3 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4j)	Cu III
$\mathbf{B}_8$	$y_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$a y_3 \hat{\mathbf{x}} - a x_3 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4j)	Cu III
$\mathbf{B}_9$	$x_4 \mathbf{a}_1 + y_4 \mathbf{a}_2$	$=$	$a x_4 \hat{\mathbf{x}} + a y_4 \hat{\mathbf{y}}$	(4j)	Pd I
$\mathbf{B}_{10}$	$-x_4 \mathbf{a}_1 - y_4 \mathbf{a}_2$	$=$	$-a x_4 \hat{\mathbf{x}} - a y_4 \hat{\mathbf{y}}$	(4j)	Pd I
$\mathbf{B}_{11}$	$-y_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-a y_4 \hat{\mathbf{x}} + a x_4 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4j)	Pd I
$\mathbf{B}_{12}$	$y_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$a y_4 \hat{\mathbf{x}} - a x_4 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4j)	Pd I
$\mathbf{B}_{13}$	$x_5 \mathbf{a}_1 + y_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$a x_5 \hat{\mathbf{x}} + a y_5 \hat{\mathbf{y}} + c z_5 \hat{\mathbf{z}}$	(8k)	Cu IV
$\mathbf{B}_{14}$	$-x_5 \mathbf{a}_1 - y_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$-a x_5 \hat{\mathbf{x}} - a y_5 \hat{\mathbf{y}} + c z_5 \hat{\mathbf{z}}$	(8k)	Cu IV
$\mathbf{B}_{15}$	$-y_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + (z_5 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-a y_5 \hat{\mathbf{x}} + a x_5 \hat{\mathbf{y}} + c (z_5 + \frac{1}{2}) \hat{\mathbf{z}}$	(8k)	Cu IV
$\mathbf{B}_{16}$	$y_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + (z_5 + \frac{1}{2}) \mathbf{a}_3$	$=$	$a y_5 \hat{\mathbf{x}} - a x_5 \hat{\mathbf{y}} + c (z_5 + \frac{1}{2}) \hat{\mathbf{z}}$	(8k)	Cu IV
$\mathbf{B}_{17}$	$-x_5 \mathbf{a}_1 - y_5 \mathbf{a}_2 - z_5 \mathbf{a}_3$	$=$	$-a x_5 \hat{\mathbf{x}} - a y_5 \hat{\mathbf{y}} - c z_5 \hat{\mathbf{z}}$	(8k)	Cu IV
$\mathbf{B}_{18}$	$x_5 \mathbf{a}_1 + y_5 \mathbf{a}_2 - z_5 \mathbf{a}_3$	$=$	$a x_5 \hat{\mathbf{x}} + a y_5 \hat{\mathbf{y}} - c z_5 \hat{\mathbf{z}}$	(8k)	Cu IV
$\mathbf{B}_{19}$	$y_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - (z_5 - \frac{1}{2}) \mathbf{a}_3$	$=$	$a y_5 \hat{\mathbf{x}} - a x_5 \hat{\mathbf{y}} - c (z_5 - \frac{1}{2}) \hat{\mathbf{z}}$	(8k)	Cu IV
$\mathbf{B}_{20}$	$-y_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 - (z_5 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-a y_5 \hat{\mathbf{x}} + a x_5 \hat{\mathbf{y}} - c (z_5 - \frac{1}{2}) \hat{\mathbf{z}}$	(8k)	Cu IV

## References

- [1] A. H. Geisler and J. B. Newkirk, *Ordering Reaction of the Cu<sub>4</sub>Pd Alloy*, JOM **6**, 1076–1082 (1954), doi:10.1007/BF03398349.