

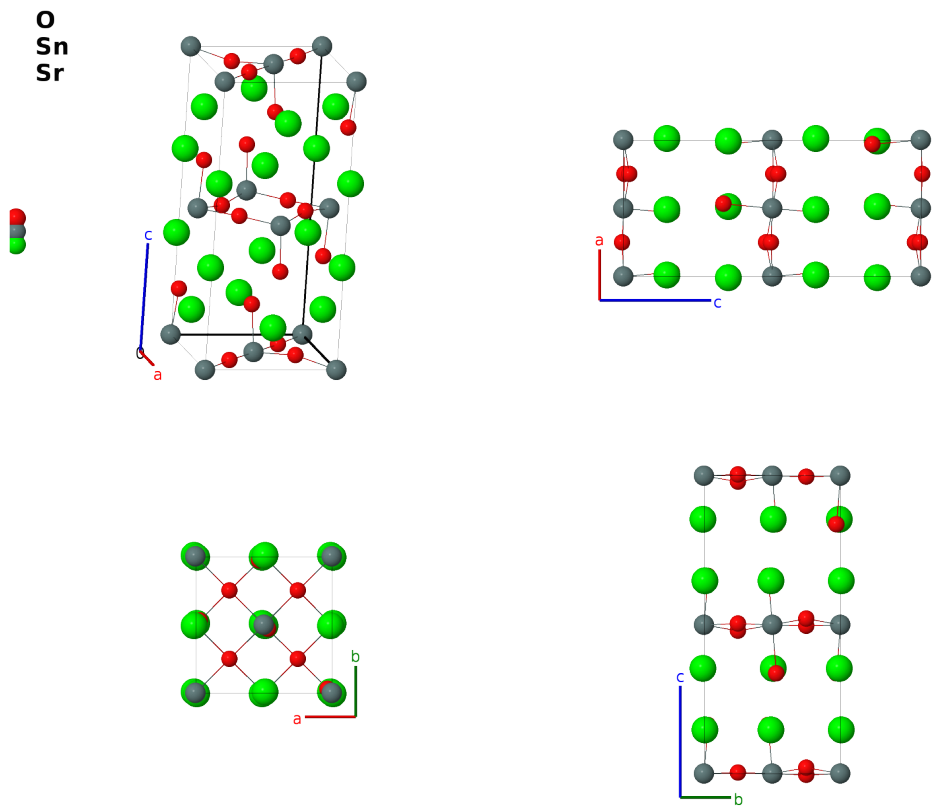
Low-temperature Sr_2SnO_4 Structure: A4BC2_oP28_56_cde_a_e-001

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<https://aflow.org/prototype-encyclopedia/TEMZ>

https://aflow.org/prototype-encyclopedia/A4BC2_oP28_56_cde_a_e-001

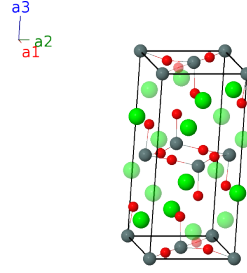


Prototype	O_4SnSr_2
AFLOW prototype label	A4BC2_oP28_56_cde_a_e-001
ICSD	59760
CCDC	1623556
Pearson symbol	oP28
Space group number	56
Space group symbol	$Pccn$
AFLOW prototype command	<code>aflow --proto=A4BC2_oP28_56_cde_a_e-001</code> <code>--params=a, b/a, c/a, z₂, z₃, x₄, y₄, z₄, x₅, y₅, z₅</code>

- We use the 4K data from (Fu, 2002).
- Many sources, including the ICSD, use La_2CuO_4 as the prototype for this structure, however (Yamada, 1988) find that that compound is better described as being in the La_2NiO_4 structure.
- All of these structures are distortions of the K_2NiF_4 Ruddlesden-Popper structure, a tetragonal perovskite phase.
- (Yun, 2022) describe the phase transitions of Sr_2SnO_4 with temperature:
 - At 4K it is in this low-temperature Sr_2SnO_4 , however note that (Fu, 2002) give crystallographic information for this structure up to 300K.
 - At 12K it is observed in the aforementioned La_2NiO_4 structure.
 - At 295K it is found in the orthorhombic La_2CuO_4 structure.
 - Finally, at 593K, it is in the K_2NiF_4 Ruddlesden-Popper structure.
- The exact experimental situation for these Ruddlesden-Popper derivatives is very uncertain, and we will update this page if and when more information is available.

Simple Orthorhombic primitive vectors

$$\begin{aligned} \mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= b \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}} \end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$=$	0	$=$	0	Sn I
$\mathbf{B}_2$	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} b \hat{\mathbf{y}}$	(4a) Sn I
$\mathbf{B}_3$	$=$	$\frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} b \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4a) Sn I
$\mathbf{B}_4$	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4a) Sn I
$\mathbf{B}_5$	$=$	$\frac{1}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + z_2 \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{x}} + \frac{1}{4} b \hat{\mathbf{y}} + c z_2 \hat{\mathbf{z}}$	(4c) O I
$\mathbf{B}_6$	$=$	$\frac{3}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - (z_2 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{3}{4} a \hat{\mathbf{x}} + \frac{3}{4} b \hat{\mathbf{y}} - c (z_2 - \frac{1}{2}) \hat{\mathbf{z}}$	(4c) O I
$\mathbf{B}_7$	$=$	$\frac{3}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - z_2 \mathbf{a}_3$	$=$	$\frac{3}{4} a \hat{\mathbf{x}} + \frac{3}{4} b \hat{\mathbf{y}} - c z_2 \hat{\mathbf{z}}$	(4c) O I
$\mathbf{B}_8$	$=$	$\frac{1}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + (z_2 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{x}} + \frac{1}{4} b \hat{\mathbf{y}} + c (z_2 + \frac{1}{2}) \hat{\mathbf{z}}$	(4c) O I
$\mathbf{B}_9$	$=$	$\frac{1}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{x}} + \frac{3}{4} b \hat{\mathbf{y}} + c z_3 \hat{\mathbf{z}}$	(4d) O II
$\mathbf{B}_{10}$	$=$	$\frac{3}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 - (z_3 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{3}{4} a \hat{\mathbf{x}} + \frac{1}{4} b \hat{\mathbf{y}} - c (z_3 - \frac{1}{2}) \hat{\mathbf{z}}$	(4d) O II
$\mathbf{B}_{11}$	$=$	$\frac{3}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 - z_3 \mathbf{a}_3$	$=$	$\frac{3}{4} a \hat{\mathbf{x}} + \frac{1}{4} b \hat{\mathbf{y}} - c z_3 \hat{\mathbf{z}}$	(4d) O II
$\mathbf{B}_{12}$	$=$	$\frac{1}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + (z_3 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{x}} + \frac{3}{4} b \hat{\mathbf{y}} + c (z_3 + \frac{1}{2}) \hat{\mathbf{z}}$	(4d) O II
$\mathbf{B}_{13}$	$=$	$x_4 \mathbf{a}_1 + y_4 \mathbf{a}_2 + z_4 \mathbf{a}_3$	$=$	$a x_4 \hat{\mathbf{x}} + b y_4 \hat{\mathbf{y}} + c z_4 \hat{\mathbf{z}}$	(8e) O III
$\mathbf{B}_{14}$	$=$	$-(x_4 - \frac{1}{2}) \mathbf{a}_1 - (y_4 - \frac{1}{2}) \mathbf{a}_2 + z_4 \mathbf{a}_3$	$=$	$-a (x_4 - \frac{1}{2}) \hat{\mathbf{x}} - b (y_4 - \frac{1}{2}) \hat{\mathbf{y}} + c z_4 \hat{\mathbf{z}}$	(8e) O III

$$\begin{aligned}
\mathbf{B}_{15} &= -x_4 \mathbf{a}_1 + \left(y_4 + \frac{1}{2}\right) \mathbf{a}_2 - \left(z_4 - \frac{1}{2}\right) \mathbf{a}_3 = -ax_4 \hat{\mathbf{x}} + b\left(y_4 + \frac{1}{2}\right) \hat{\mathbf{y}} - c\left(z_4 - \frac{1}{2}\right) \hat{\mathbf{z}} & (8e) & \text{O III} \\
\mathbf{B}_{16} &= \left(x_4 + \frac{1}{2}\right) \mathbf{a}_1 - y_4 \mathbf{a}_2 - \left(z_4 - \frac{1}{2}\right) \mathbf{a}_3 = a\left(x_4 + \frac{1}{2}\right) \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} - c\left(z_4 - \frac{1}{2}\right) \hat{\mathbf{z}} & (8e) & \text{O III} \\
\mathbf{B}_{17} &= -x_4 \mathbf{a}_1 - y_4 \mathbf{a}_2 - z_4 \mathbf{a}_3 = -ax_4 \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}} & (8e) & \text{O III} \\
\mathbf{B}_{18} &= \left(x_4 + \frac{1}{2}\right) \mathbf{a}_1 + \left(y_4 + \frac{1}{2}\right) \mathbf{a}_2 - z_4 \mathbf{a}_3 = a\left(x_4 + \frac{1}{2}\right) \hat{\mathbf{x}} + b\left(y_4 + \frac{1}{2}\right) \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}} & (8e) & \text{O III} \\
\mathbf{B}_{19} &= x_4 \mathbf{a}_1 - \left(y_4 - \frac{1}{2}\right) \mathbf{a}_2 + \left(z_4 + \frac{1}{2}\right) \mathbf{a}_3 = ax_4 \hat{\mathbf{x}} - b\left(y_4 - \frac{1}{2}\right) \hat{\mathbf{y}} + c\left(z_4 + \frac{1}{2}\right) \hat{\mathbf{z}} & (8e) & \text{O III} \\
\mathbf{B}_{20} &= -\left(x_4 - \frac{1}{2}\right) \mathbf{a}_1 + y_4 \mathbf{a}_2 + \left(z_4 + \frac{1}{2}\right) \mathbf{a}_3 = -a\left(x_4 - \frac{1}{2}\right) \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} + c\left(z_4 + \frac{1}{2}\right) \hat{\mathbf{z}} & (8e) & \text{O III} \\
\mathbf{B}_{21} &= x_5 \mathbf{a}_1 + y_5 \mathbf{a}_2 + z_5 \mathbf{a}_3 = ax_5 \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}} & (8e) & \text{Sr I} \\
\mathbf{B}_{22} &= -\left(x_5 - \frac{1}{2}\right) \mathbf{a}_1 - \left(y_5 - \frac{1}{2}\right) \mathbf{a}_2 + z_5 \mathbf{a}_3 = -a\left(x_5 - \frac{1}{2}\right) \hat{\mathbf{x}} - b\left(y_5 - \frac{1}{2}\right) \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}} & (8e) & \text{Sr I} \\
\mathbf{B}_{23} &= -x_5 \mathbf{a}_1 + \left(y_5 + \frac{1}{2}\right) \mathbf{a}_2 - \left(z_5 - \frac{1}{2}\right) \mathbf{a}_3 = -ax_5 \hat{\mathbf{x}} + b\left(y_5 + \frac{1}{2}\right) \hat{\mathbf{y}} - c\left(z_5 - \frac{1}{2}\right) \hat{\mathbf{z}} & (8e) & \text{Sr I} \\
\mathbf{B}_{24} &= \left(x_5 + \frac{1}{2}\right) \mathbf{a}_1 - y_5 \mathbf{a}_2 - \left(z_5 - \frac{1}{2}\right) \mathbf{a}_3 = a\left(x_5 + \frac{1}{2}\right) \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} - c\left(z_5 - \frac{1}{2}\right) \hat{\mathbf{z}} & (8e) & \text{Sr I} \\
\mathbf{B}_{25} &= -x_5 \mathbf{a}_1 - y_5 \mathbf{a}_2 - z_5 \mathbf{a}_3 = -ax_5 \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}} & (8e) & \text{Sr I} \\
\mathbf{B}_{26} &= \left(x_5 + \frac{1}{2}\right) \mathbf{a}_1 + \left(y_5 + \frac{1}{2}\right) \mathbf{a}_2 - z_5 \mathbf{a}_3 = a\left(x_5 + \frac{1}{2}\right) \hat{\mathbf{x}} + b\left(y_5 + \frac{1}{2}\right) \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}} & (8e) & \text{Sr I} \\
\mathbf{B}_{27} &= x_5 \mathbf{a}_1 - \left(y_5 - \frac{1}{2}\right) \mathbf{a}_2 + \left(z_5 + \frac{1}{2}\right) \mathbf{a}_3 = ax_5 \hat{\mathbf{x}} - b\left(y_5 - \frac{1}{2}\right) \hat{\mathbf{y}} + c\left(z_5 + \frac{1}{2}\right) \hat{\mathbf{z}} & (8e) & \text{Sr I} \\
\mathbf{B}_{28} &= -\left(x_5 - \frac{1}{2}\right) \mathbf{a}_1 + y_5 \mathbf{a}_2 + \left(z_5 + \frac{1}{2}\right) \mathbf{a}_3 = -a\left(x_5 - \frac{1}{2}\right) \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} + c\left(z_5 + \frac{1}{2}\right) \hat{\mathbf{z}} & (8e) & \text{Sr I}
\end{aligned}$$

References

- [1] W. T. Fu, D. Visser, and D. J. W. IJdo, *High-resolution neutron powder diffraction study on the structure of Sr_2SnO_4* , J. Solid State Chem. **169**, 208–213 (2002), doi:10.1016/S0022-4596(02)00067-1.
- [2] K. Yamada, E. Kudo, Y. Endoh, K. Tsuda, M. Tanaka, K. Kokusho, H. Asano, F. Izumi, M. Oda, Y. Hidaka, M. Suzuki, and T. Murakami, *Determination of Space Group and Refinement of Structure Parameters for $\text{La}_2\text{CuO}_{4-\delta}$ Crystals*, Jpn. J. Appl. Phys. **27**, 1132–1137 (1988). 10.1143/jjap.27.1132.

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