

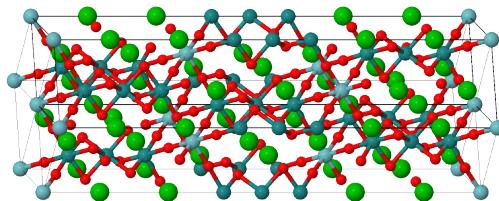
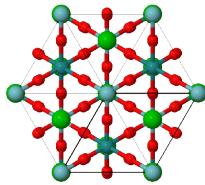
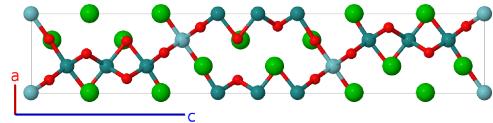
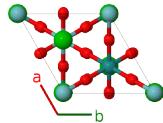
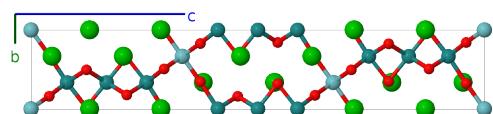
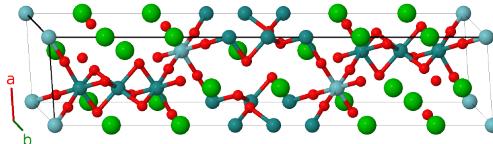
Ba₄NbRu₃O₁₂ Structure: A4BC12D3_hR20_166_2c_a_2h_bc-001

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<https://aflow.org/p/9CFG>

https://aflow.org/p/A4BC12D3_hR20_166_2c_a_2h_bc-001

● Ba
● Nb
● O
● Ru



Prototype Ba₄NbO₁₂Ru₃

AFLOW prototype label A4BC12D3_hR20_166_2c_a_2h_bc-001

ICSD none

Pearson symbol hR20

Space group number 166

Space group symbol $R\bar{3}m$

AFLOW prototype command `aflow --proto=A4BC12D3_hR20_166_2c_a_2h_bc-001
--params=a, c/a, x3, x4, x5, x6, z6, x7, z7`

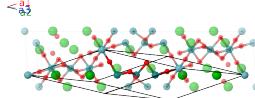
Other compounds with this structure

Ir₄NbRu₃O₁₂, Mn₄NbRu₃O₁₂, Rh₄NbRu₃O₁₂

- Hexagonal settings of this structure can be obtained with the option `--hex`.

Rhombohedral primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} + \frac{1}{3}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{\sqrt{3}}a\hat{\mathbf{y}} + \frac{1}{3}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= -\frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} + \frac{1}{3}c\hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates	Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	= 0	= 0	(1a)	Nb I
\mathbf{B}_2	= $\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	= $\frac{1}{2}c\hat{\mathbf{z}}$	(1b)	Ru I
\mathbf{B}_3	= $x_3\mathbf{a}_1 + x_3\mathbf{a}_2 + x_3\mathbf{a}_3$	= $cx_3\hat{\mathbf{z}}$	(2c)	Ba I
\mathbf{B}_4	= $-x_3\mathbf{a}_1 - x_3\mathbf{a}_2 - x_3\mathbf{a}_3$	= $-cx_3\hat{\mathbf{z}}$	(2c)	Ba I
\mathbf{B}_5	= $x_4\mathbf{a}_1 + x_4\mathbf{a}_2 + x_4\mathbf{a}_3$	= $cx_4\hat{\mathbf{z}}$	(2c)	Ba II
\mathbf{B}_6	= $-x_4\mathbf{a}_1 - x_4\mathbf{a}_2 - x_4\mathbf{a}_3$	= $-cx_4\hat{\mathbf{z}}$	(2c)	Ba II
\mathbf{B}_7	= $x_5\mathbf{a}_1 + x_5\mathbf{a}_2 + x_5\mathbf{a}_3$	= $cx_5\hat{\mathbf{z}}$	(2c)	Ru II
\mathbf{B}_8	= $-x_5\mathbf{a}_1 - x_5\mathbf{a}_2 - x_5\mathbf{a}_3$	= $-cx_5\hat{\mathbf{z}}$	(2c)	Ru II
\mathbf{B}_9	= $x_6\mathbf{a}_1 + x_6\mathbf{a}_2 + z_6\mathbf{a}_3$	= $\frac{1}{2}a(x_6 - z_6)\hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a(x_6 - z_6)\hat{\mathbf{y}} + \frac{1}{3}c(2x_6 + z_6)\hat{\mathbf{z}}$	(6h)	O I
\mathbf{B}_{10}	= $z_6\mathbf{a}_1 + x_6\mathbf{a}_2 + x_6\mathbf{a}_3$	= $-\frac{1}{2}a(x_6 - z_6)\hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a(x_6 - z_6)\hat{\mathbf{y}} + \frac{1}{3}c(2x_6 + z_6)\hat{\mathbf{z}}$	(6h)	O I
\mathbf{B}_{11}	= $x_6\mathbf{a}_1 + z_6\mathbf{a}_2 + x_6\mathbf{a}_3$	= $-\frac{1}{\sqrt{3}}a(x_6 - z_6)\hat{\mathbf{y}} + \frac{1}{3}c(2x_6 + z_6)\hat{\mathbf{z}}$	(6h)	O I
\mathbf{B}_{12}	= $-z_6\mathbf{a}_1 - x_6\mathbf{a}_2 - x_6\mathbf{a}_3$	= $\frac{1}{2}a(x_6 - z_6)\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a(x_6 - z_6)\hat{\mathbf{y}} - \frac{1}{3}c(2x_6 + z_6)\hat{\mathbf{z}}$	(6h)	O I
\mathbf{B}_{13}	= $-x_6\mathbf{a}_1 - x_6\mathbf{a}_2 - z_6\mathbf{a}_3$	= $-\frac{1}{2}a(x_6 - z_6)\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a(x_6 - z_6)\hat{\mathbf{y}} - \frac{1}{3}c(2x_6 + z_6)\hat{\mathbf{z}}$	(6h)	O I
\mathbf{B}_{14}	= $-x_6\mathbf{a}_1 - z_6\mathbf{a}_2 - x_6\mathbf{a}_3$	= $\frac{1}{\sqrt{3}}a(x_6 - z_6)\hat{\mathbf{y}} - \frac{1}{3}c(2x_6 + z_6)\hat{\mathbf{z}}$	(6h)	O I
\mathbf{B}_{15}	= $x_7\mathbf{a}_1 + x_7\mathbf{a}_2 + z_7\mathbf{a}_3$	= $\frac{1}{2}a(x_7 - z_7)\hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a(x_7 - z_7)\hat{\mathbf{y}} + \frac{1}{3}c(2x_7 + z_7)\hat{\mathbf{z}}$	(6h)	O II
\mathbf{B}_{16}	= $z_7\mathbf{a}_1 + x_7\mathbf{a}_2 + x_7\mathbf{a}_3$	= $-\frac{1}{2}a(x_7 - z_7)\hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a(x_7 - z_7)\hat{\mathbf{y}} + \frac{1}{3}c(2x_7 + z_7)\hat{\mathbf{z}}$	(6h)	O II
\mathbf{B}_{17}	= $x_7\mathbf{a}_1 + z_7\mathbf{a}_2 + x_7\mathbf{a}_3$	= $-\frac{1}{\sqrt{3}}a(x_7 - z_7)\hat{\mathbf{y}} + \frac{1}{3}c(2x_7 + z_7)\hat{\mathbf{z}}$	(6h)	O II
\mathbf{B}_{18}	= $-z_7\mathbf{a}_1 - x_7\mathbf{a}_2 - x_7\mathbf{a}_3$	= $\frac{1}{2}a(x_7 - z_7)\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a(x_7 - z_7)\hat{\mathbf{y}} - \frac{1}{3}c(2x_7 + z_7)\hat{\mathbf{z}}$	(6h)	O II
\mathbf{B}_{19}	= $-x_7\mathbf{a}_1 - x_7\mathbf{a}_2 - z_7\mathbf{a}_3$	= $-\frac{1}{2}a(x_7 - z_7)\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a(x_7 - z_7)\hat{\mathbf{y}} - \frac{1}{3}c(2x_7 + z_7)\hat{\mathbf{z}}$	(6h)	O II
\mathbf{B}_{20}	= $-x_7\mathbf{a}_1 - z_7\mathbf{a}_2 - x_7\mathbf{a}_3$	= $\frac{1}{\sqrt{3}}a(x_7 - z_7)\hat{\mathbf{y}} - \frac{1}{3}c(2x_7 + z_7)\hat{\mathbf{z}}$	(6h)	O II

References

- [1] L. T. Nguyen, T. Halloran, W. Xie, T. Kong, C. L. Broholm, and R. J. Cava, *Geometrically frustrated trimer-based Mott insulator*, Phys. Rev. Mater. **2**, 054414 (2018), doi:10.1103/PhysRevMaterials.2.054414.

Found in

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