

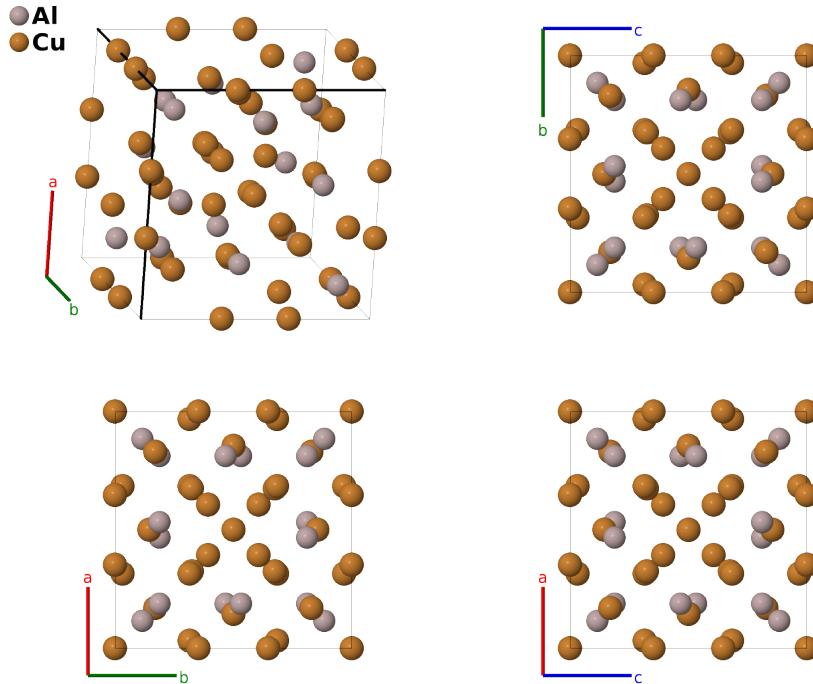
# $\gamma$ -brass ( $\text{Cu}_9\text{Al}_4$ , $D8_3$ ) Structure: A4B9\_cP52\_215\_ei\_3efgi-001

This structure originally had the label A4B9\_cP52\_215\_ei\_3efgi. Calls to that address will be redirected here.

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<https://aflow.org/p/TRNX>

[https://aflow.org/p/A4B9\\_cP52\\_215\\_ei\\_3efgi-001](https://aflow.org/p/A4B9_cP52_215_ei_3efgi-001)



<b>Prototype</b>	$\text{Al}_4\text{Cu}_9$
<b>AFLOW prototype label</b>	A4B9_cP52_215_ei_3efgi-001
<b>Strukturbericht designation</b>	$D8_3$
<b>Mineral name</b>	$\gamma$ -brass
<b>ICSD</b>	1625
<b>Pearson symbol</b>	cP52
<b>Space group number</b>	215
<b>Space group symbol</b>	$P\bar{4}3m$
<b>AFLOW prototype command</b>	<pre>aflow --proto=A4B9_cP52_215_ei_3efgi-001 --params=a,x1,x2,x3,x4,x5,x6,x7,z7,x8,z8</pre>

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**Other compounds with this structure**  
 $\text{Cu}_9\text{Ga}_4$ ,  $\text{InMn}_3$

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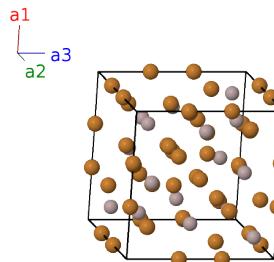
- (Arnberg, 1978) give the Wyckoff positions of the Cu-IV and Cu-V atoms as (6g) ( $x, 1/2, 1/2$ ), but give the coordinates in the form  $(x, 0, 0)$  corresponding to the (6f) site.
- (Stokhuyzen, 1974) used (6f) for both types of atoms in the isostructural system  $\text{Ga}_9\text{Al}_4$ .
- (Pearson, 1958) places the Cu-IV atoms on a (6f) site and Cu-V on (6g), but does not give explicit coordinates.
- Placing the Cu-V atoms on (6f) sites yields an interatomic distance of  $1.8\text{\AA}$ . This contradicts (Arnberg, 1978), who say that the minimum interatomic distance between the Cu-IV and Cu-V atoms is  $2.48\text{\AA}$ . Placing the Cu-V atoms on (6g) sites gives this distance, in agreement with (Pearson, 1958), so we make this choice for the crystal structure.
- This is a variety of  $\gamma$ -brass comparable to the  $D8_2$  structure. In fact, if we
  - Replace the Al and Cu-III atoms by Zn, while setting  $x_4 = x_1 + 1/2$ ,
  - Replace the Al II and Cu-VI atoms by Zn, with  $x_8 = x_7 + 1/2$  and  $z_8 = z_7 + 1/2$ ,
  - Set  $x_3 = x_2 + 1/2$  and
  - Set  $x_6 = x_5 + 1/2$ ,

then this structure is identical to  $D8_2$   $\gamma$ -brass.

- (Pearson, 1958), pp. 252, gives a list of compounds which can take on the  $D8_1$ ,  $D8_2$ , or  $D8_3$  structure, depending on the exact composition.
- (Mizutani, 2010) classifies this as a “P-cell”  $\gamma$ -brass.

### Simple Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= a \hat{\mathbf{y}} \\ \mathbf{a}_3 &= a \hat{\mathbf{z}}\end{aligned}$$



### Basis vectors

	Lattice coordinates	=	Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$x_1 \mathbf{a}_1 + x_1 \mathbf{a}_2 + x_1 \mathbf{a}_3$	=	$ax_1 \hat{\mathbf{x}} + ax_1 \hat{\mathbf{y}} + ax_1 \hat{\mathbf{z}}$	(4e)	Al I
$\mathbf{B}_2$	$-x_1 \mathbf{a}_1 - x_1 \mathbf{a}_2 + x_1 \mathbf{a}_3$	=	$-ax_1 \hat{\mathbf{x}} - ax_1 \hat{\mathbf{y}} + ax_1 \hat{\mathbf{z}}$	(4e)	Al I
$\mathbf{B}_3$	$-x_1 \mathbf{a}_1 + x_1 \mathbf{a}_2 - x_1 \mathbf{a}_3$	=	$-ax_1 \hat{\mathbf{x}} + ax_1 \hat{\mathbf{y}} - ax_1 \hat{\mathbf{z}}$	(4e)	Al I
$\mathbf{B}_4$	$x_1 \mathbf{a}_1 - x_1 \mathbf{a}_2 - x_1 \mathbf{a}_3$	=	$ax_1 \hat{\mathbf{x}} - ax_1 \hat{\mathbf{y}} - ax_1 \hat{\mathbf{z}}$	(4e)	Al I
$\mathbf{B}_5$	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	=	$ax_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$	(4e)	Cu I
$\mathbf{B}_6$	$-x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	=	$-ax_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$	(4e)	Cu I
$\mathbf{B}_7$	$-x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	=	$-ax_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$	(4e)	Cu I
$\mathbf{B}_8$	$x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	=	$ax_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$	(4e)	Cu I
$\mathbf{B}_9$	$x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	=	$ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(4e)	Cu II
$\mathbf{B}_{10}$	$-x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	=	$-ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(4e)	Cu II
$\mathbf{B}_{11}$	$-x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 - x_3 \mathbf{a}_3$	=	$-ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(4e)	Cu II
$\mathbf{B}_{12}$	$x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 - x_3 \mathbf{a}_3$	=	$ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(4e)	Cu II

$B_{13} =$	$x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + x_4 \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}}$	(4e)	Cu III
$B_{14} =$	$-x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 + x_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}}$	(4e)	Cu III
$B_{15} =$	$-x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 - x_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}}$	(4e)	Cu III
$B_{16} =$	$x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 - x_4 \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}}$	(4e)	Cu III
$B_{17} =$	$x_5 \mathbf{a}_1$	$=$	$ax_5 \hat{\mathbf{x}}$	(6f)	Cu IV
$B_{18} =$	$-x_5 \mathbf{a}_1$	$=$	$-ax_5 \hat{\mathbf{x}}$	(6f)	Cu IV
$B_{19} =$	$x_5 \mathbf{a}_2$	$=$	$ax_5 \hat{\mathbf{y}}$	(6f)	Cu IV
$B_{20} =$	$-x_5 \mathbf{a}_2$	$=$	$-ax_5 \hat{\mathbf{y}}$	(6f)	Cu IV
$B_{21} =$	$x_5 \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{z}}$	(6f)	Cu IV
$B_{22} =$	$-x_5 \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{z}}$	(6f)	Cu IV
$B_{23} =$	$x_6 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6g)	Cu V
$B_{24} =$	$-x_6 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-ax_6 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6g)	Cu V
$B_{25} =$	$\frac{1}{2} \mathbf{a}_1 + x_6 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6g)	Cu V
$B_{26} =$	$\frac{1}{2} \mathbf{a}_1 - x_6 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6g)	Cu V
$B_{27} =$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + x_6 \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + ax_6 \hat{\mathbf{z}}$	(6g)	Cu V
$B_{28} =$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 - x_6 \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} - ax_6 \hat{\mathbf{z}}$	(6g)	Cu V
$B_{29} =$	$x_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} + az_7 \hat{\mathbf{z}}$	(12i)	Al II
$B_{30} =$	$-x_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} + az_7 \hat{\mathbf{z}}$	(12i)	Al II
$B_{31} =$	$-x_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 - z_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} - az_7 \hat{\mathbf{z}}$	(12i)	Al II
$B_{32} =$	$x_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 - z_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} - az_7 \hat{\mathbf{z}}$	(12i)	Al II
$B_{33} =$	$z_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$az_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} + ax_7 \hat{\mathbf{z}}$	(12i)	Al II
$B_{34} =$	$z_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 - x_7 \mathbf{a}_3$	$=$	$az_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} - ax_7 \hat{\mathbf{z}}$	(12i)	Al II
$B_{35} =$	$-z_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$-az_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} + ax_7 \hat{\mathbf{z}}$	(12i)	Al II
$B_{36} =$	$-z_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 - x_7 \mathbf{a}_3$	$=$	$-az_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} - ax_7 \hat{\mathbf{z}}$	(12i)	Al II
$B_{37} =$	$x_7 \mathbf{a}_1 + z_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} + az_7 \hat{\mathbf{y}} + ax_7 \hat{\mathbf{z}}$	(12i)	Al II
$B_{38} =$	$-x_7 \mathbf{a}_1 + z_7 \mathbf{a}_2 - x_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} + az_7 \hat{\mathbf{y}} - ax_7 \hat{\mathbf{z}}$	(12i)	Al II
$B_{39} =$	$x_7 \mathbf{a}_1 - z_7 \mathbf{a}_2 - x_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} - az_7 \hat{\mathbf{y}} - ax_7 \hat{\mathbf{z}}$	(12i)	Al II
$B_{40} =$	$-x_7 \mathbf{a}_1 - z_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} - az_7 \hat{\mathbf{y}} + ax_7 \hat{\mathbf{z}}$	(12i)	Al II
$B_{41} =$	$x_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} + az_8 \hat{\mathbf{z}}$	(12i)	Cu VI
$B_{42} =$	$-x_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} + az_8 \hat{\mathbf{z}}$	(12i)	Cu VI
$B_{43} =$	$-x_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 - z_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} - az_8 \hat{\mathbf{z}}$	(12i)	Cu VI
$B_{44} =$	$x_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 - z_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} - az_8 \hat{\mathbf{z}}$	(12i)	Cu VI
$B_{45} =$	$z_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 + x_8 \mathbf{a}_3$	$=$	$az_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} + ax_8 \hat{\mathbf{z}}$	(12i)	Cu VI
$B_{46} =$	$z_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 - x_8 \mathbf{a}_3$	$=$	$az_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} - ax_8 \hat{\mathbf{z}}$	(12i)	Cu VI
$B_{47} =$	$-z_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 + x_8 \mathbf{a}_3$	$=$	$-az_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} + ax_8 \hat{\mathbf{z}}$	(12i)	Cu VI
$B_{48} =$	$-z_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 - x_8 \mathbf{a}_3$	$=$	$-az_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} - ax_8 \hat{\mathbf{z}}$	(12i)	Cu VI
$B_{49} =$	$x_8 \mathbf{a}_1 + z_8 \mathbf{a}_2 + x_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} + az_8 \hat{\mathbf{y}} + ax_8 \hat{\mathbf{z}}$	(12i)	Cu VI
$B_{50} =$	$-x_8 \mathbf{a}_1 + z_8 \mathbf{a}_2 - x_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} + az_8 \hat{\mathbf{y}} - ax_8 \hat{\mathbf{z}}$	(12i)	Cu VI
$B_{51} =$	$x_8 \mathbf{a}_1 - z_8 \mathbf{a}_2 - x_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} - az_8 \hat{\mathbf{y}} - ax_8 \hat{\mathbf{z}}$	(12i)	Cu VI
$B_{52} =$	$-x_8 \mathbf{a}_1 - z_8 \mathbf{a}_2 + x_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} - az_8 \hat{\mathbf{y}} + ax_8 \hat{\mathbf{z}}$	(12i)	Cu VI

## References

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