

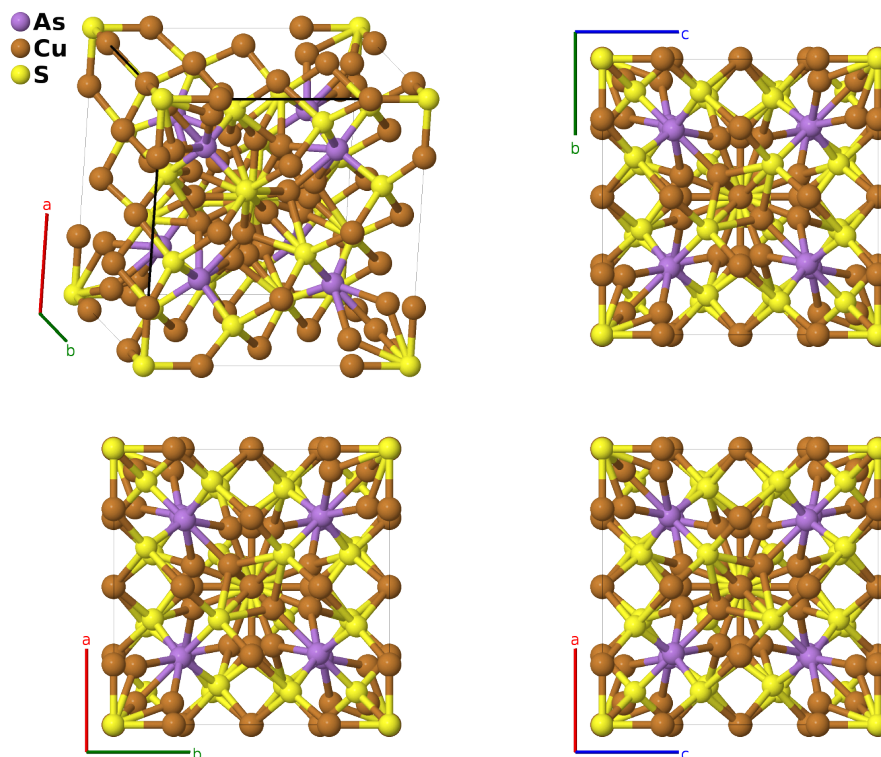
Tennantite ($\text{Cu}_{12}\text{As}_4\text{S}_{13}$) Structure: A4B24C13_cI82_217_c_deg_ag-001

This structure originally had the label A4B24C13_cI82_217_c_deg_ag. Calls to that address will be redirected here.

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<https://aflow.org/p/5PAV>

https://aflow.org/p/A4B24C13_cI82_217_c_deg_ag-001



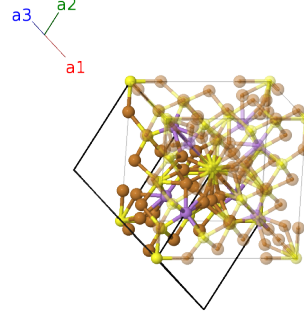
Prototype	$\text{AsCu}_{12}\text{S}_{13}$
AFLOW prototype label	A4B24C13_cI82_217_c_deg_ag-001
Mineral name	tennantite
ICSD	403458
Pearson symbol	cI82
Space group number	217
Space group symbol	$\bar{I}43m$
AFLOW prototype command	<code>aflow --proto=A4B24C13_cI82_217_c_deg_ag-001 --params=a, x2, x4, x5, z5, x6, z6</code>

Other compounds with this structure
 $\text{Cu}_{14}\text{Sb}_4\text{S}_{13}$ (tetrahedrite)

- The Cu-II (12e) site is only occupied 75.8% of the time, and the Cu-III site is occupied 12.1% of the time, so that these sites only contain twelve atoms between them.
- Searching (Downs, 2003) shows that natural samples often have antimony substituting for arsenic. The antimony structures (tetrahedrites) contain higher concentrations of copper.

Body-centered Cubic primitive vectors

$$\begin{aligned} \mathbf{a}_1 &= -\frac{1}{2}a\hat{x} + \frac{1}{2}a\hat{y} + \frac{1}{2}a\hat{z} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{x} - \frac{1}{2}a\hat{y} + \frac{1}{2}a\hat{z} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{x} + \frac{1}{2}a\hat{y} - \frac{1}{2}a\hat{z} \end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	0	$=$	0	(2a)	S I
\mathbf{B}_2	$2x_2 \mathbf{a}_1 + 2x_2 \mathbf{a}_2 + 2x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{x} + ax_2 \hat{y} + ax_2 \hat{z}$	(8c)	As I
\mathbf{B}_3	$-2x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{x} - ax_2 \hat{y} + ax_2 \hat{z}$	(8c)	As I
\mathbf{B}_4	$-2x_2 \mathbf{a}_2$	$=$	$-ax_2 \hat{x} + ax_2 \hat{y} - ax_2 \hat{z}$	(8c)	As I
\mathbf{B}_5	$-2x_2 \mathbf{a}_1$	$=$	$ax_2 \hat{x} - ax_2 \hat{y} - ax_2 \hat{z}$	(8c)	As I
\mathbf{B}_6	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{x} + \frac{1}{2}a\hat{y}$	(12d)	Cu I
\mathbf{B}_7	$\frac{1}{2} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{x} + \frac{1}{2}a\hat{z}$	(12d)	Cu I
\mathbf{B}_8	$\frac{3}{4} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{y} + \frac{1}{2}a\hat{z}$	(12d)	Cu I
\mathbf{B}_9	$\frac{1}{4} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{x} + \frac{1}{4}a\hat{y}$	(12d)	Cu I
\mathbf{B}_{10}	$\frac{1}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{x} + \frac{1}{4}a\hat{z}$	(12d)	Cu I
\mathbf{B}_{11}	$\frac{3}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{y} + \frac{1}{4}a\hat{z}$	(12d)	Cu I
\mathbf{B}_{12}	$x_4 \mathbf{a}_2 + x_4 \mathbf{a}_3$	$=$	$ax_4 \hat{x}$	(12e)	Cu II
\mathbf{B}_{13}	$-x_4 \mathbf{a}_2 - x_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{x}$	(12e)	Cu II
\mathbf{B}_{14}	$x_4 \mathbf{a}_1 + x_4 \mathbf{a}_3$	$=$	$ax_4 \hat{y}$	(12e)	Cu II
\mathbf{B}_{15}	$-x_4 \mathbf{a}_1 - x_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{y}$	(12e)	Cu II
\mathbf{B}_{16}	$x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2$	$=$	$ax_4 \hat{z}$	(12e)	Cu II
\mathbf{B}_{17}	$-x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2$	$=$	$-ax_4 \hat{z}$	(12e)	Cu II
\mathbf{B}_{18}	$(x_5 + z_5) \mathbf{a}_1 + (x_5 + z_5) \mathbf{a}_2 + 2x_5 \mathbf{a}_3$	$=$	$ax_5 \hat{x} + ax_5 \hat{y} + az_5 \hat{z}$	(24g)	Cu III
\mathbf{B}_{19}	$-(x_5 - z_5) \mathbf{a}_1 - (x_5 - z_5) \mathbf{a}_2 - 2x_5 \mathbf{a}_3$	$=$	$-ax_5 \hat{x} - ax_5 \hat{y} + az_5 \hat{z}$	(24g)	Cu III
\mathbf{B}_{20}	$(x_5 - z_5) \mathbf{a}_1 - (x_5 + z_5) \mathbf{a}_2$	$=$	$-ax_5 \hat{x} + ax_5 \hat{y} - az_5 \hat{z}$	(24g)	Cu III
\mathbf{B}_{21}	$-(x_5 + z_5) \mathbf{a}_1 + (x_5 - z_5) \mathbf{a}_2$	$=$	$ax_5 \hat{x} - ax_5 \hat{y} - az_5 \hat{z}$	(24g)	Cu III
\mathbf{B}_{22}	$2x_5 \mathbf{a}_1 + (x_5 + z_5) \mathbf{a}_2 + (x_5 + z_5) \mathbf{a}_3$	$=$	$az_5 \hat{x} + ax_5 \hat{y} + ax_5 \hat{z}$	(24g)	Cu III

$$\begin{aligned}
\mathbf{B}_{23} &= -2x_5 \mathbf{a}_1 - (x_5 - z_5) \mathbf{a}_2 - (x_5 - z_5) \mathbf{a}_3 &= & az_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}} & (24g) & \text{Cu III} \\
\mathbf{B}_{24} &= (x_5 - z_5) \mathbf{a}_2 - (x_5 + z_5) \mathbf{a}_3 &= & -az_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}} & (24g) & \text{Cu III} \\
\mathbf{B}_{25} &= -(x_5 + z_5) \mathbf{a}_2 + (x_5 - z_5) \mathbf{a}_3 &= & -az_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}} & (24g) & \text{Cu III} \\
\mathbf{B}_{26} &= (x_5 + z_5) \mathbf{a}_1 + 2x_5 \mathbf{a}_2 + (x_5 + z_5) \mathbf{a}_3 &= & ax_5 \hat{\mathbf{x}} + az_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}} & (24g) & \text{Cu III} \\
\mathbf{B}_{27} &= -(x_5 - z_5) \mathbf{a}_1 - 2x_5 \mathbf{a}_2 - (x_5 - z_5) \mathbf{a}_3 &= & -ax_5 \hat{\mathbf{x}} + az_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}} & (24g) & \text{Cu III} \\
\mathbf{B}_{28} &= -(x_5 + z_5) \mathbf{a}_1 + (x_5 - z_5) \mathbf{a}_3 &= & ax_5 \hat{\mathbf{x}} - az_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}} & (24g) & \text{Cu III} \\
\mathbf{B}_{29} &= (x_5 - z_5) \mathbf{a}_1 - (x_5 + z_5) \mathbf{a}_3 &= & -ax_5 \hat{\mathbf{x}} - az_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}} & (24g) & \text{Cu III} \\
\mathbf{B}_{30} &= (x_6 + z_6) \mathbf{a}_1 + (x_6 + z_6) \mathbf{a}_2 + 2x_6 \mathbf{a}_3 &= & ax_6 \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} + az_6 \hat{\mathbf{z}} & (24g) & \text{S II} \\
\mathbf{B}_{31} &= -(x_6 - z_6) \mathbf{a}_1 - (x_6 - z_6) \mathbf{a}_2 - 2x_6 \mathbf{a}_3 &= & -ax_6 \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} + az_6 \hat{\mathbf{z}} & (24g) & \text{S II} \\
\mathbf{B}_{32} &= (x_6 - z_6) \mathbf{a}_1 - (x_6 + z_6) \mathbf{a}_2 &= & -ax_6 \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} - az_6 \hat{\mathbf{z}} & (24g) & \text{S II} \\
\mathbf{B}_{33} &= -(x_6 + z_6) \mathbf{a}_1 + (x_6 - z_6) \mathbf{a}_2 &= & ax_6 \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} - az_6 \hat{\mathbf{z}} & (24g) & \text{S II} \\
\mathbf{B}_{34} &= 2x_6 \mathbf{a}_1 + (x_6 + z_6) \mathbf{a}_2 + (x_6 + z_6) \mathbf{a}_3 &= & az_6 \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} + ax_6 \hat{\mathbf{z}} & (24g) & \text{S II} \\
\mathbf{B}_{35} &= -2x_6 \mathbf{a}_1 - (x_6 - z_6) \mathbf{a}_2 - (x_6 - z_6) \mathbf{a}_3 &= & az_6 \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} - ax_6 \hat{\mathbf{z}} & (24g) & \text{S II} \\
\mathbf{B}_{36} &= (x_6 - z_6) \mathbf{a}_2 - (x_6 + z_6) \mathbf{a}_3 &= & -az_6 \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} + ax_6 \hat{\mathbf{z}} & (24g) & \text{S II} \\
\mathbf{B}_{37} &= -(x_6 + z_6) \mathbf{a}_2 + (x_6 - z_6) \mathbf{a}_3 &= & -az_6 \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} - ax_6 \hat{\mathbf{z}} & (24g) & \text{S II} \\
\mathbf{B}_{38} &= (x_6 + z_6) \mathbf{a}_1 + 2x_6 \mathbf{a}_2 + (x_6 + z_6) \mathbf{a}_3 &= & ax_6 \hat{\mathbf{x}} + az_6 \hat{\mathbf{y}} + ax_6 \hat{\mathbf{z}} & (24g) & \text{S II} \\
\mathbf{B}_{39} &= -(x_6 - z_6) \mathbf{a}_1 - 2x_6 \mathbf{a}_2 - (x_6 - z_6) \mathbf{a}_3 &= & -ax_6 \hat{\mathbf{x}} + az_6 \hat{\mathbf{y}} - ax_6 \hat{\mathbf{z}} & (24g) & \text{S II} \\
\mathbf{B}_{40} &= -(x_6 + z_6) \mathbf{a}_1 + (x_6 - z_6) \mathbf{a}_3 &= & ax_6 \hat{\mathbf{x}} - az_6 \hat{\mathbf{y}} - ax_6 \hat{\mathbf{z}} & (24g) & \text{S II} \\
\mathbf{B}_{41} &= (x_6 - z_6) \mathbf{a}_1 - (x_6 + z_6) \mathbf{a}_3 &= & -ax_6 \hat{\mathbf{x}} - az_6 \hat{\mathbf{y}} + ax_6 \hat{\mathbf{z}} & (24g) & \text{S II}
\end{aligned}$$

References

- [1] A. A. Yaroslavzev, A. V. Mironov, A. N. Kuznetsov, A. P. Dudka, and O. N. Khrykina, *Tennantite: multi-temperature crystal structure, phase transition and electronic structure of synthetic $\text{Cu}_{12}\text{As}_4\text{S}_{13}$* , Acta Crystallogr. Sect. B **75**, 634–642 (2019), doi:10.1107/S2052520619007595.
- [2] R. T. Downs and M. Hall-Wallace, *The American Mineralogist Crystal Structure Database*, Am. Mineral. **88**, 247–250 (2003).